

# Overview of Non-Solenoidal Startup Studies in the Pegasus ST

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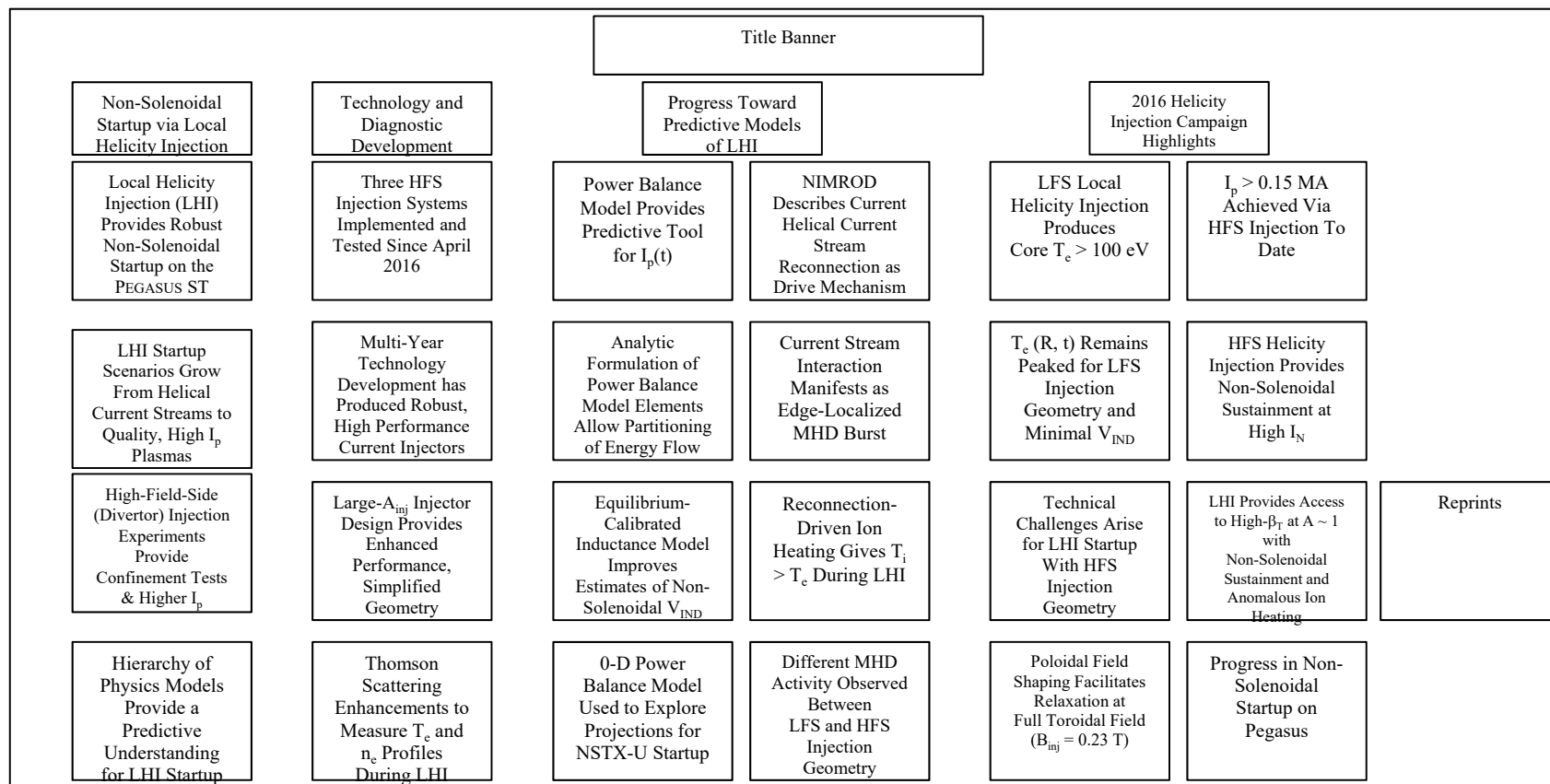
PEGASUS  
Toroidal Experiment



# Layout

8.5" x 11"

8' W x 4' H





# Non-Solenoidal Startup via Local Helicity Injection



# Technology and Diagnostic Development



# Progress Toward Predictive Models of LHI



# 2016 Helicity Injection Campaign Highlights



# Local Helicity Injection (LHI) Provides Robust Non-Solenoidal Startup on the PEGASUS ST

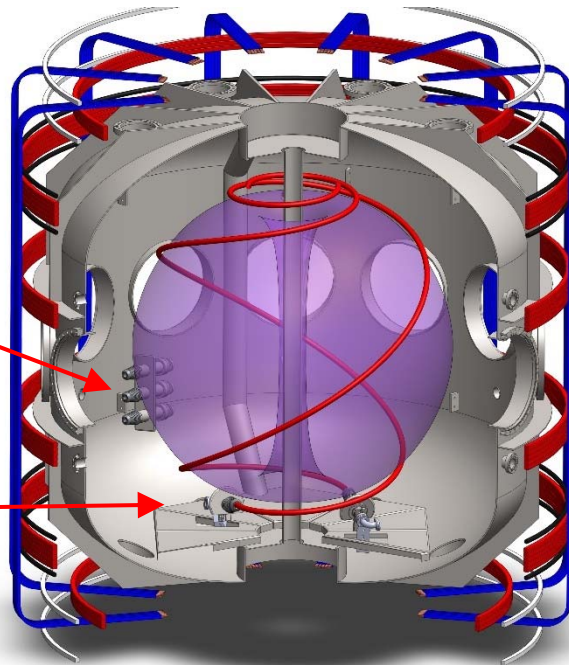


LFS System

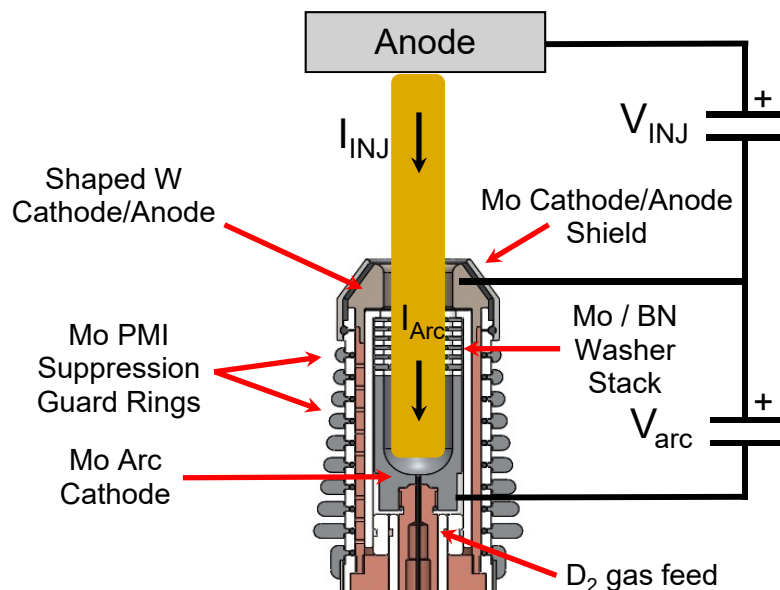
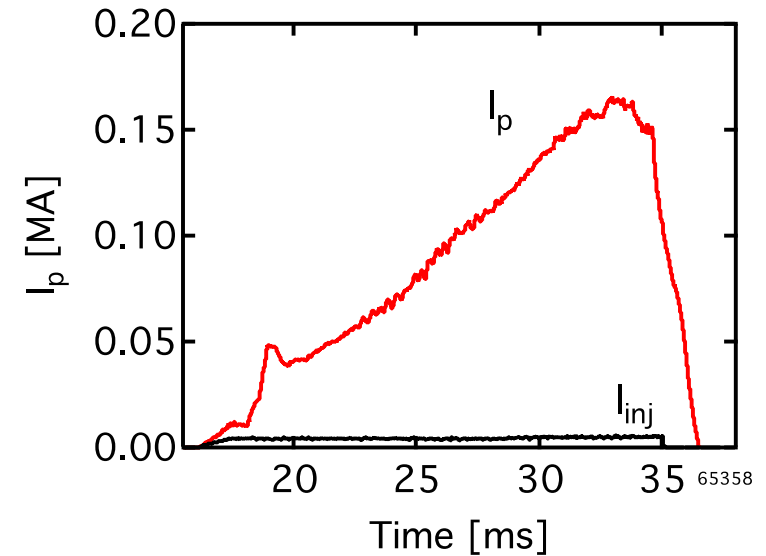
HFS System



Helicity Injectors



$I_p \leq 0.18$  MA via LHI ( $I_{inj} = 5$  kA)



## Plasma Parameters

$I_p$	$\leq 0.23$ MA
$\tau_{shot}$	$\leq 0.025$ s
$B_T$	0.15 T
$A$	1.15–1.3
$R$	0.2–0.45 m
$a$	$\leq 0.4$ m
$\kappa$	1.4–3.7

## Injector Parameters

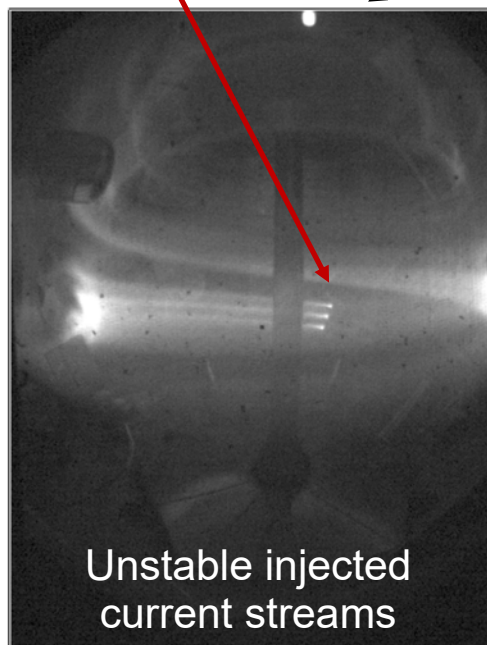
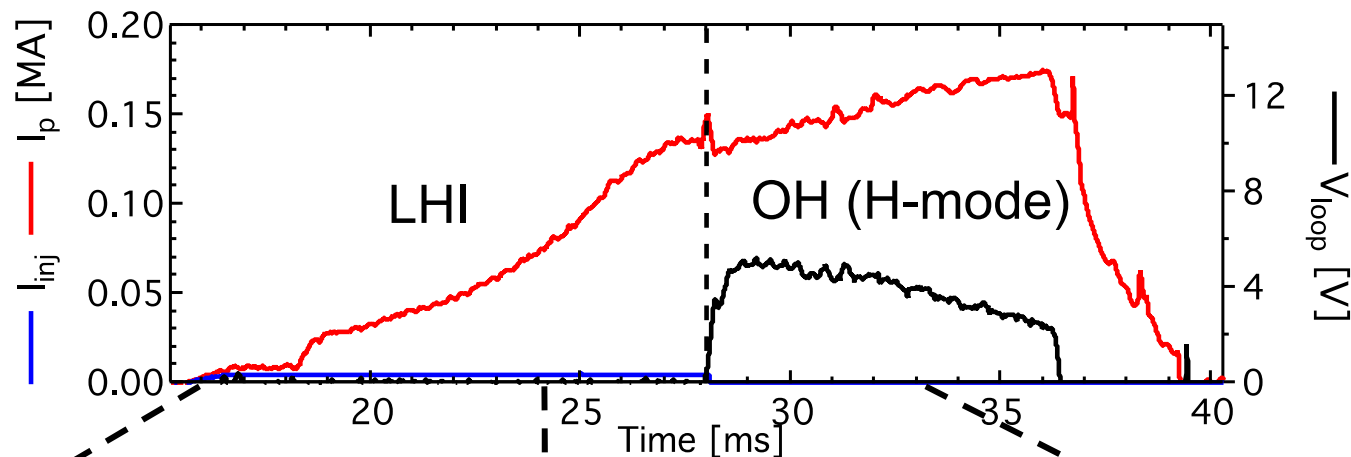
$\Sigma I_{inj}$	$\leq 14$ kA
$I_{inj}$	$\leq 4$ kA
$V_{inj}$	$\leq 2.5$ kV
$N_{inj}$	$\leq 4$
$A_{inj}$	$= 2-4$ cm <sup>2</sup>
$I_{arc}$	$\leq 4$ kA
$V_{arc}$	$\leq 0.5$ kV



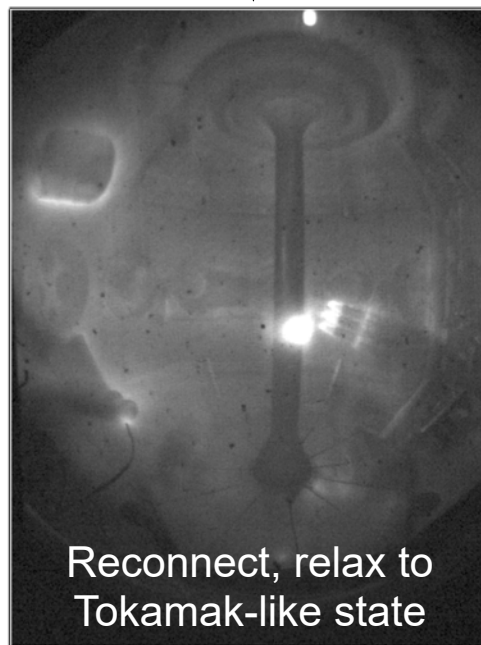


# LHI Startup Scenarios Grow From Helical Current Streams to Quality, High $I_p$ Plasmas

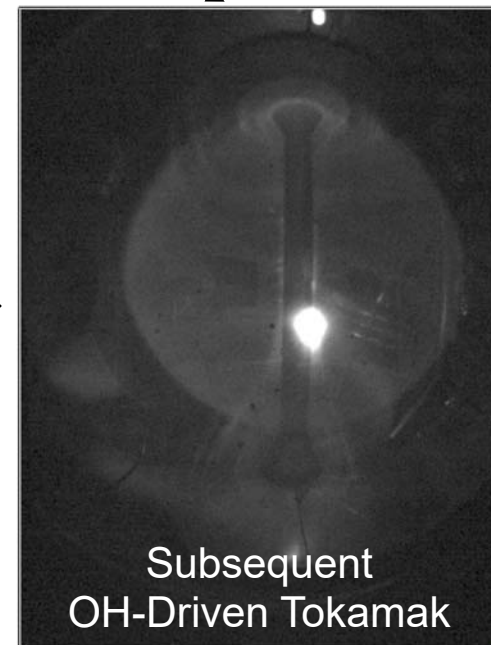
Three-Injector Array



Null Formation  
Relaxation



Injector Shutoff



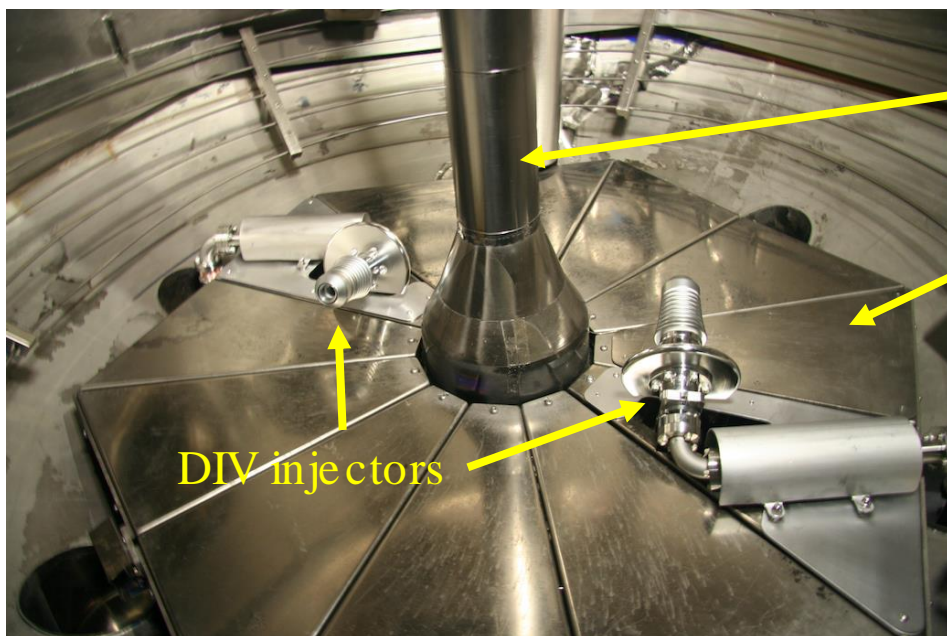
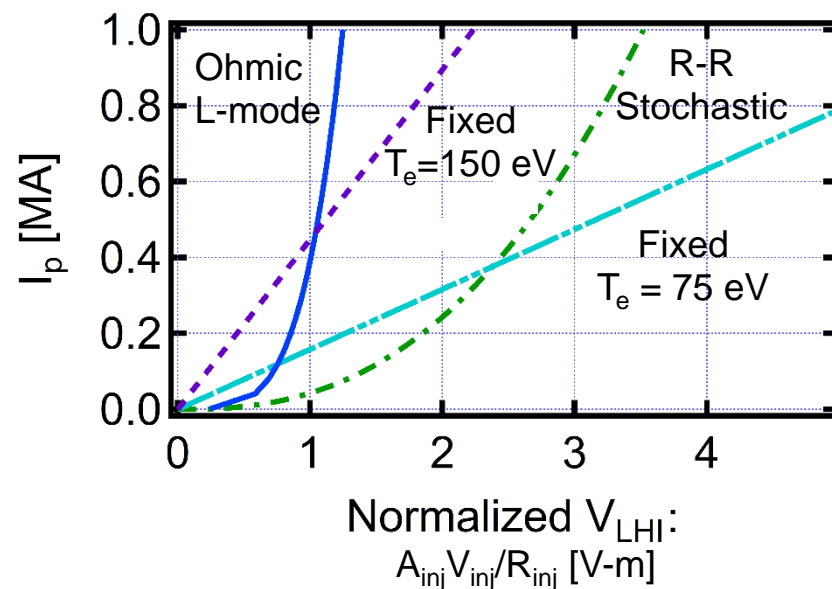




# High-Field-Side (Divertor) Injection Experiments Provide Confinement Tests & Higher $I_p$

- Initial HFS injector campaign in progress
  - Development to minimize PMI as  $B_{TF}$  increases
- Configuration minimizes  $V_{IND}$
- 3-4x increase in HI drive:  $V_{eff} \sim A_{inj} V_{inj} / R_{inj}$
- Test reconnection mechanisms at higher  $I_p$ ,  $B_{TF}$
- Injectors at longer pulse, high- $B_{TF}$

NSTX-U Projected Performance



Centerstack

Lower DIV  
Strike Plate

DIV injectors





# Hierarchy of Physics Models Provide a Predictive Understanding for LHI Startup

1. Taylor relaxation, helicity conservation
  - Steady-state maximum  $I_p$  limits

Taylor Relaxation

$$I_p \leq I_{TL} \sim \sqrt{\frac{I_{TF} I_{inj}}{w}}$$

Helicity Conservation

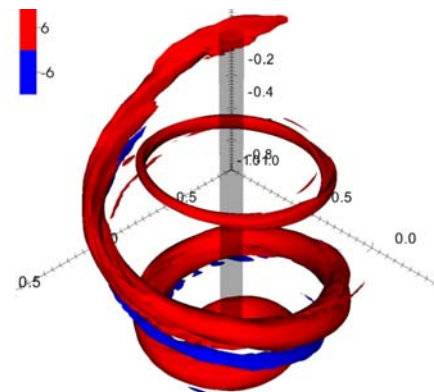
$$V_{LHI} \approx \frac{A_{inj} B_{\phi, inj}}{\Psi} V_{inj}$$

2. 0-D power-balance  $I_p(t)$ 
  - $V_{LHI}$  for effective LHI current drive

$$I_p [V_{LHI} + V_{IR} + V_{IND}] = 0; I_p \leq I_{TL}$$

3. 3D Resistive MHD (NIMROD)
  - Physics of LHI current drive mechanism

Reconnecting LHI Current Stream





# Three HFS Injection Systems Implemented and Tested Since April 2016

- Two injectors at toroidally opposite positions in lower divertor region
- Design point leverages high  $A_{inj}$ 
  - 3–4 $\times$  increase in  $V_{LHI}$  over prior systems
  - $A_{inj} = 8 \text{ cm}^2$  total
  - $V_{inj} \leq 1.2 \text{ kV}$
  - $I_{inj} \geq 8 \text{ kA}$  total
- Systems vary  $R_{inj}$ ,  $Z_{inj}$ , local limiter geometry
  - Latest design incorporates floating, electropolished divertor shield plates

*Configuration 1*



*Configuration 2*



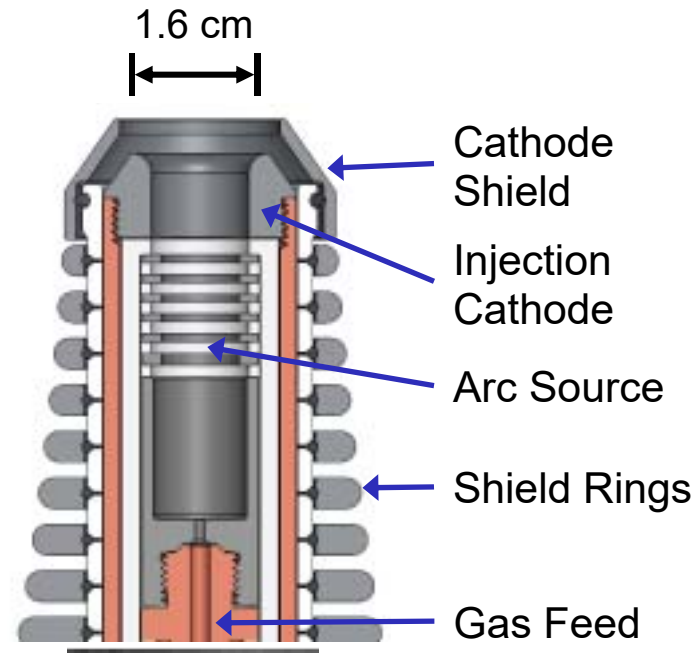
*Configuration 3*





# Multi-Year Technology Development has Produced Robust, High Performance Current Injectors

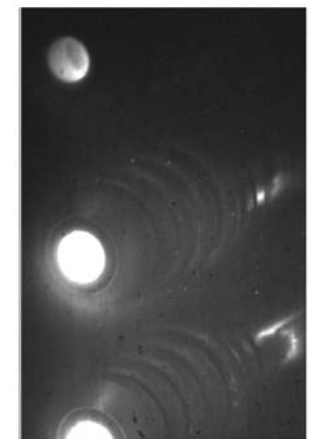
- Washer-stack arc source:
  - $J_{inj} \sim 1 \text{ kA/cm}^2$
- High-voltage in SOL:  $V_{inj} > 1 \text{ kV}$ 
  - Frustum cathode
  - Floating cathode shield
- PMI control: 1-2 cm from LCFS
  - Cascaded shield rings
  - Local limiter
  - Mo, W PFCs



Three-Injector Array



Clean, High- $V_{inj}$  Operation

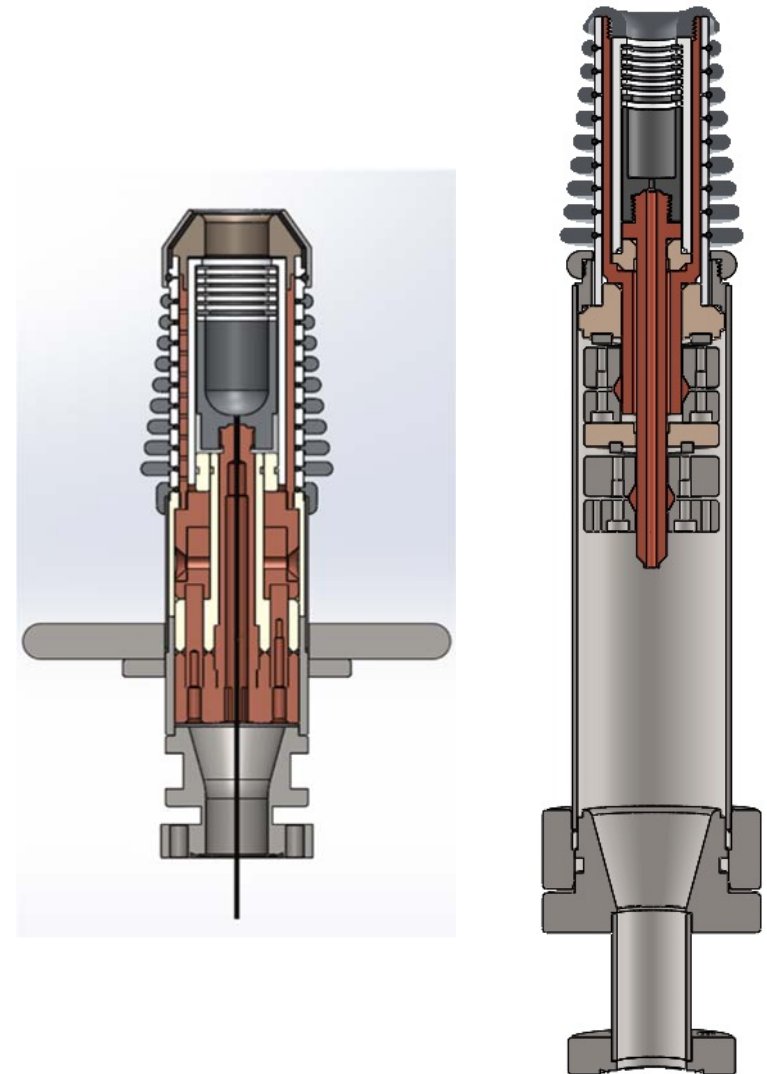






# Large- $A_{inj}$ Injector Design Provides Enhanced Performance, Simplified Geometry

- New injectors designed for HFS system
  - Doubled  $A_{inj}$  ( $2 \text{ cm}^2 \rightarrow 4 \text{ cm}^2$ )
  - Compact design for lower divertor region
- Modular internal assembly
  - Permits in-vessel maintenance/repositioning
  - Exterior PFC components rapidly adjusted about common arc chamber / fueling system
    - Changes to  $A_{inj}$ , shield structures
  - Integrated hypodermic gas feed alleviates field sensitivity from previous
- Refractory materials for resilience to harsh environment
  - W for high- $V_{inj}$  cathode/anode
  - Mo for external shield assemblies



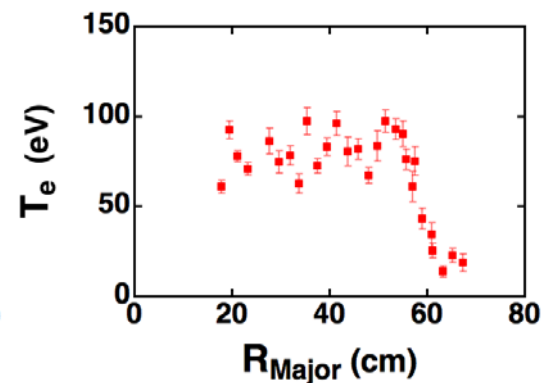
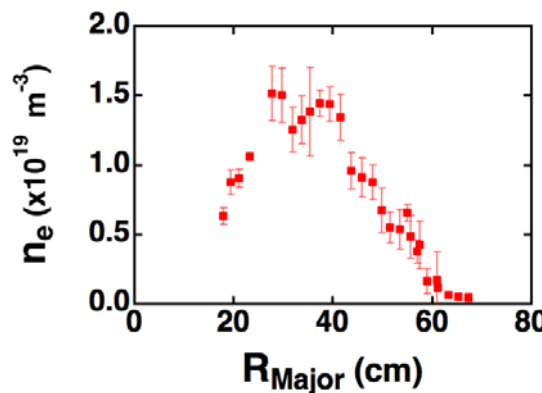
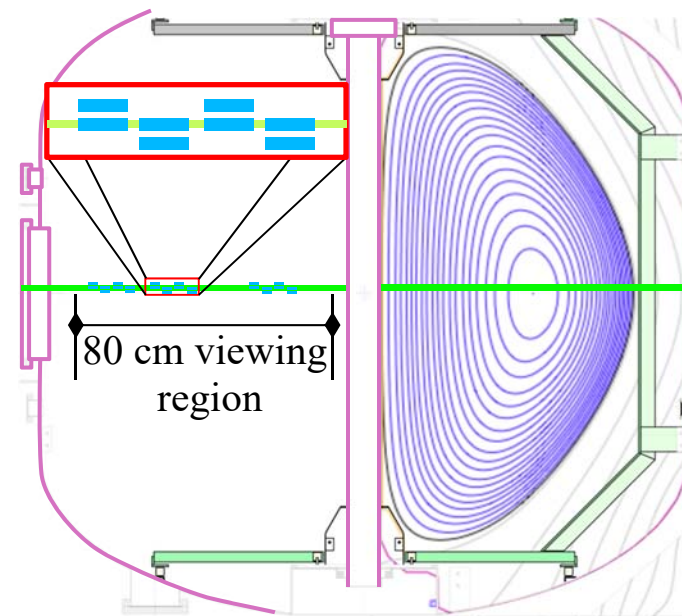
New:  $4 \text{ cm}^2$  Old:  $2 \text{ cm}^2$



# Thomson Scattering Enhancements to Measure $T_e$ and $n_e$ Profiles During LHI

- Improved timing / synchronization
  - Higher realized laser power
  - Lowered beam scrape-off losses
- System automation
  - Intra-shot beam alignment
  - Data acquisition
- Stray light mitigation
  - Baffling, electronic gating
- Background signal reduction
  - Wire grid polarizers
  - High speed shutters

## *Thomson Viewing Locations and $A \sim 1$ Plasma*

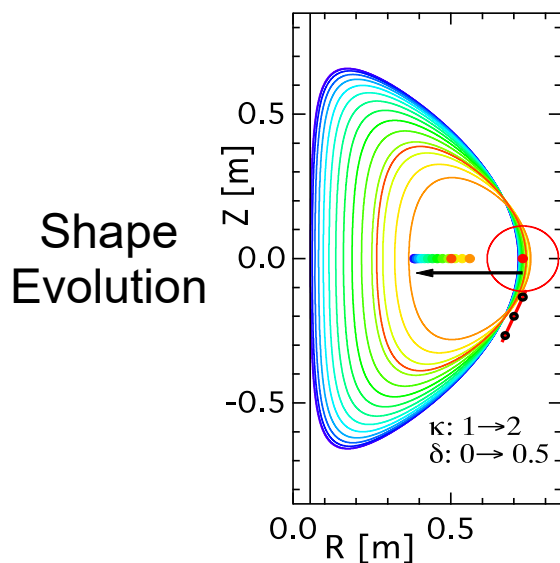




# Power Balance Model Provides Predictive Tool for $I_p(t)$

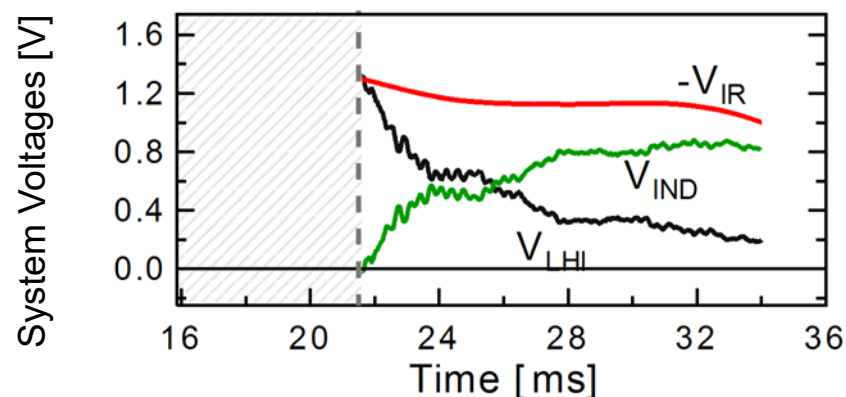
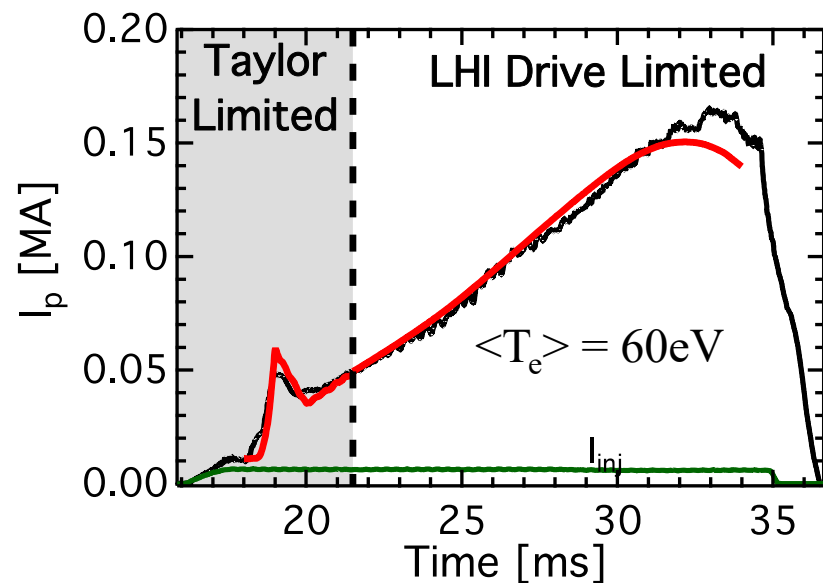
$$I_p [V_{LHI} + V_{IR} + V_{IND}] = 0$$

- $V_{LHI}$ : effective drive
- $V_{IR}$ : resistive dissipation
- $V_{IND}$ : analytic, from shape(t)
- Taylor relaxation limit:  $I_p \leq I_{TL}$



- $V_{IND}$  dominates current drive with LFS mid-plane injection

- Model reasonably recreates  $I_p(t)$







# Analytic Formulation of Power Balance Model Elements Allow Partitioning of Energy Flow

$$I_p \left[ \underbrace{V_{PF} + V_{geo} - V_{W_m}}_{V_{IND}} - V_{IR} + V_{LHI} \right] = 0$$

- Recent Improvements
  - Revised  $L_p$ ,  $B_Z$  models\*
  - Moving plasma boundary
  - Neoclassical resistivity

*Inductive Drive from Poloidal Fields*

$$V_{PF} = - \sum_{coils} \frac{d}{dt} [\psi_{PF}] \approx - \frac{\partial}{\partial t} \left[ M_V \pi R_0^2 B_V |_{R_0} \right]$$

$$B_V = - \frac{\mu_0 I_p}{4 \pi R_0} \left\{ \frac{1}{\mu_0} \frac{\partial L_e}{\partial R} + \frac{\ell_i}{2} + \beta_p - \frac{1}{2} \right\}$$

$$M_V(\varepsilon, \kappa) = \frac{(1-\varepsilon)^2}{(1-\varepsilon)^2 c(\varepsilon) + d(\varepsilon) \sqrt{\kappa}} \quad \begin{aligned} c(\varepsilon) &= 1 + 0.98\varepsilon^2 + 0.49\varepsilon^4 + 1.47\varepsilon^6 \\ d(\varepsilon) &= 0.25\varepsilon(1 + 0.84\varepsilon - 1.44\varepsilon^2) \end{aligned}$$

*LHI Drive*

$$V_{LHI} = \frac{A_{inj} B_{\varphi, inj}}{\Psi} V_{inj}$$

*Resistive Dissipation*

$$V_{IR} = I_p R_p = I_p \left( \frac{\langle \eta \rangle 2 \pi R_0}{A_p} \right)$$

*Inductive Drive from Shape(t)*

$$V_{geo} = - \frac{d}{dt} [L_e I_p] = -L_e \frac{dI_p}{dt} - I_p \frac{dL_e}{dt}$$

$$L_e = \mu_0 R_0 \frac{a(\varepsilon)(1-\varepsilon)}{1-\varepsilon + \kappa b(\varepsilon)}$$

$$\begin{aligned} a(\varepsilon) &= \left( 1 + 1.81\sqrt{\varepsilon} + 2.05\varepsilon \right) \ln \left( \frac{8}{\varepsilon} \right) \\ &\quad - \left( 2.0 + 9.25\sqrt{\varepsilon} + 1.21\varepsilon \right) \\ b(\varepsilon) &= 0.73\sqrt{\varepsilon} (1 + 2\varepsilon^4 - 6\varepsilon^5 + 3.7\varepsilon^6) \end{aligned}$$

*Plasma Magnetic Energy Change*

$$V_{W_m} \approx - \frac{1}{I_p} \frac{d}{dt} \left( \frac{1}{2} L_i I_p^2 \right)$$

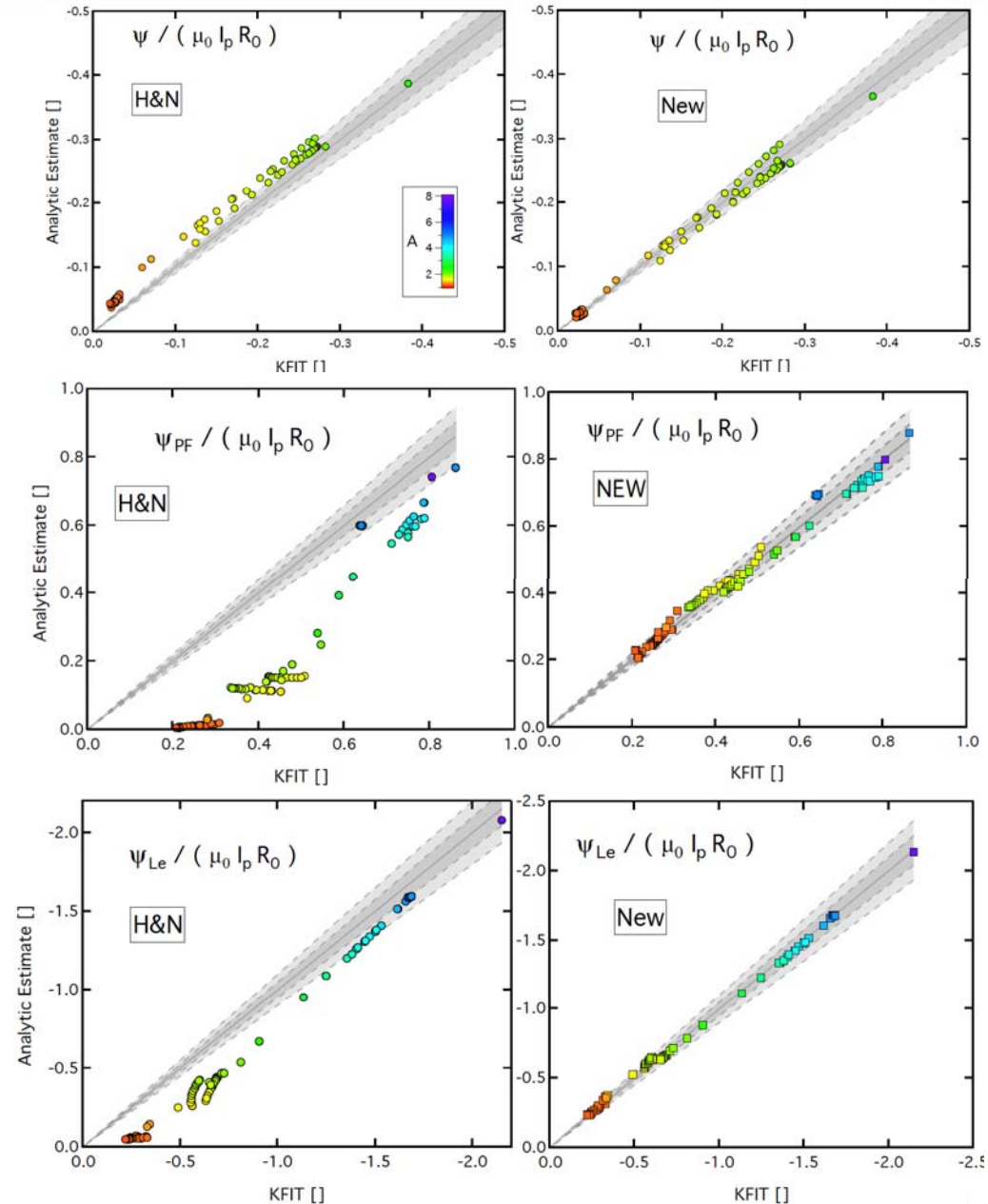
$$\ell_i = \frac{C_p^2}{\mu_0 V_p} L_i$$





# Equilibrium-Calibrated Inductance Model Improves Estimates of Non-Solenoidal $V_{IND}$

- Maintaining radial force balance provides  $V_{IND}$ 
  - Originally calculated via H-N formulae
- Important to quantify contributions from shape, PF drive in LHI system design
- Model equilibrium database generated to test analytic formulae in realistic magnetic geometries
  - $N = 331$ ;  $1.15 < A < 8$ ;  $1 < \kappa < 3$
  - $0 < \beta_p < 1$ ;  $0.2 < \ell_i < 0.75$
- Poor partitioning of  $V_{IND}$  between shape,  $V_{PF}$  components found
  - However, total flux estimates in better agreement
- Revised  $V_{IND}$  model developed
  - Derived new coefficients in H-N formalism via fit to equilibrium database
  - Weak dependence on  $\beta_p$ ,  $\ell_i$  introduced

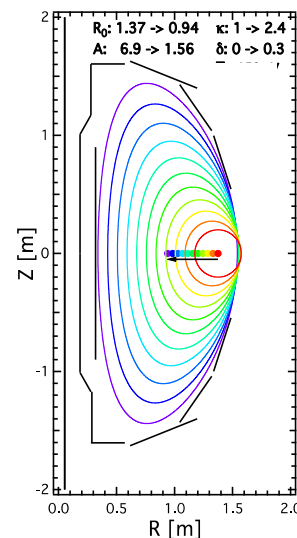




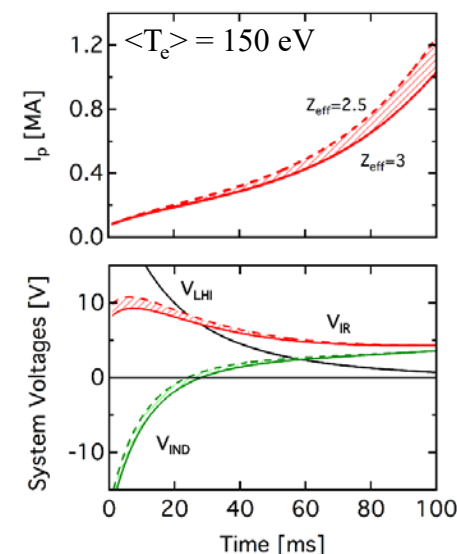
# 0-D Power Balance Model Used to Explore Projections for NSTX-U Startup

- Helicity dissipation ( $V_{IR}$ ) dependent on  $T_e$ , realized electron confinement
- Importance of  $V_{LHI}$ ,  $V_{IND}$  depends on injector geometry, plasma growth scenario
  - Final plasma depends strongly on full time evolution
- Injector geometry emphasizes different drive terms
  - LFS injection:  $V_{LHI}$  early,  $V_{IND}$  late
  - HFS: injection mainly  $V_{LHI}$
- Need to explore plasma evolution with different dominant drive terms
  - Informs predictive model
  - Future: High  $I_p$  tests in both geometries

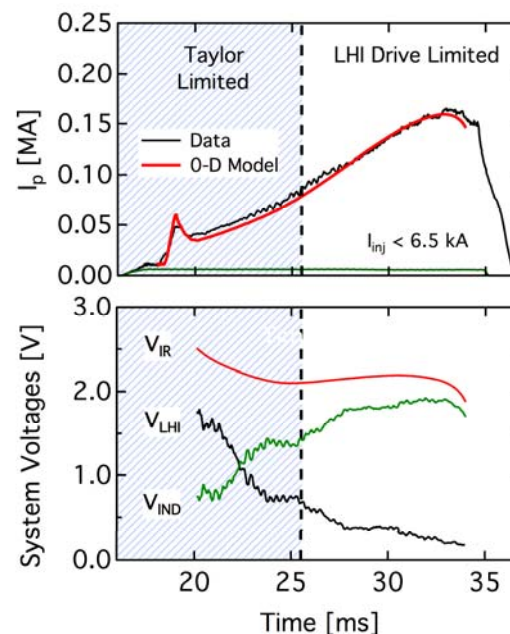
## Shape evolution for LFS LHI on NSTX-U



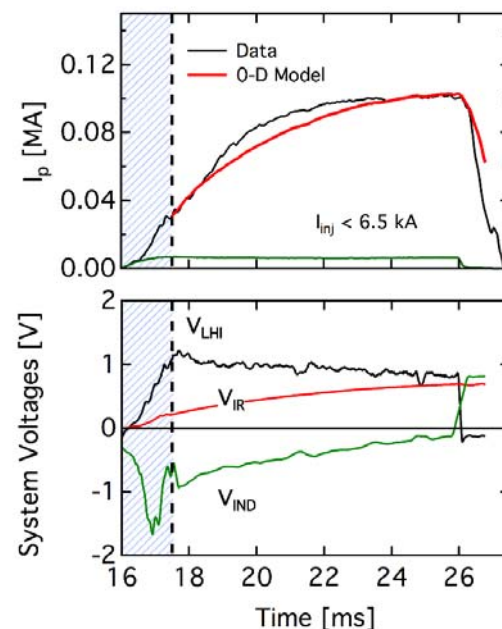
## NSTX-U: Projected



## LFS PEGASUS



## HFS PEGASUS

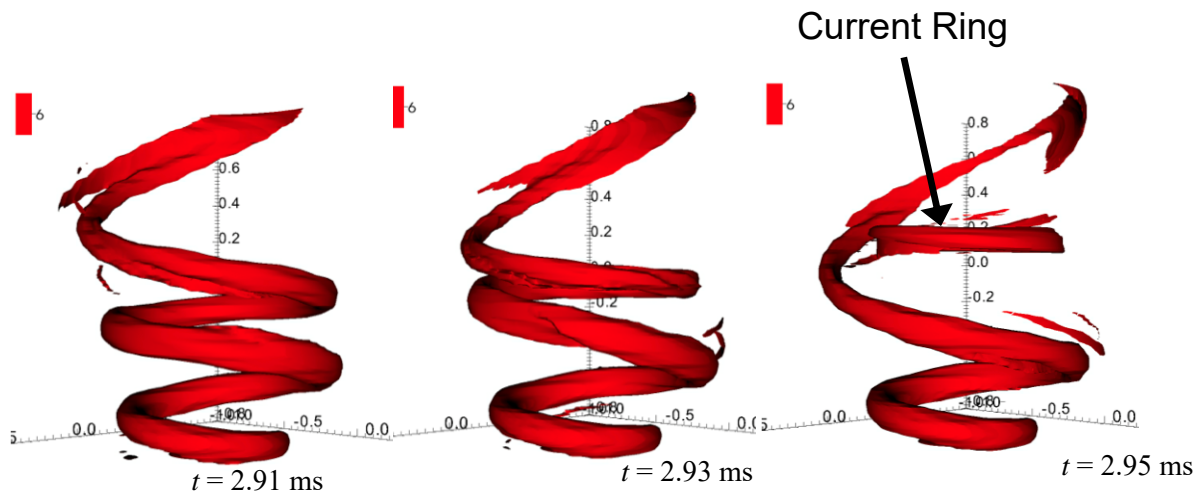




# NIMROD Describes Helical Current Stream Reconnection as Drive Mechanism

- Divertor injection → minimal inductive drive

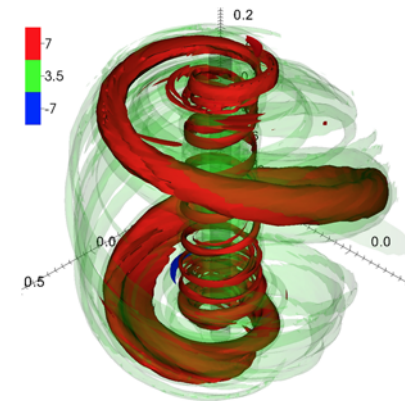
*Divertor LHI Startup Shows suggestive commonality between experiment and NIMROD modeling*



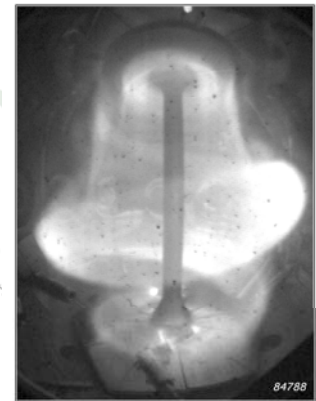
1. Streams follow field lines

2. Adjacent passes attract

3. Reconnection pinches off current rings



NIMROD Simulation  
[O'Bryan PhD 2014]



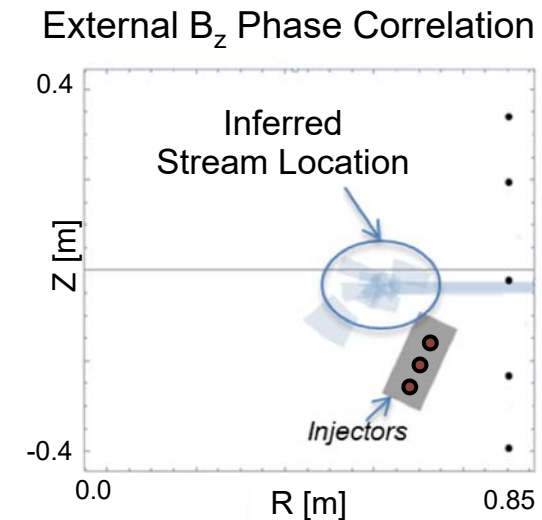
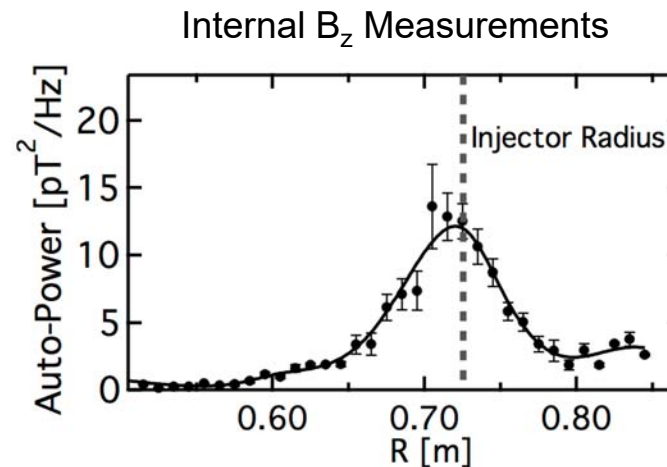
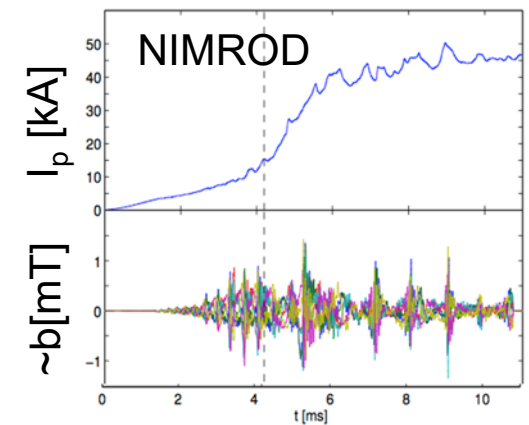
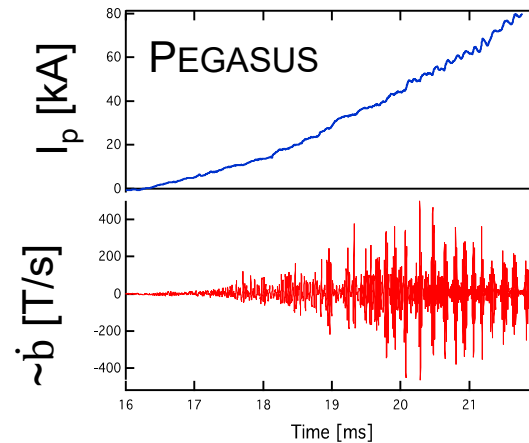
May 2016 PEGASUS  
High-speed Imaging





# Current Stream Interaction Manifests as Edge-Localized MHD Burst

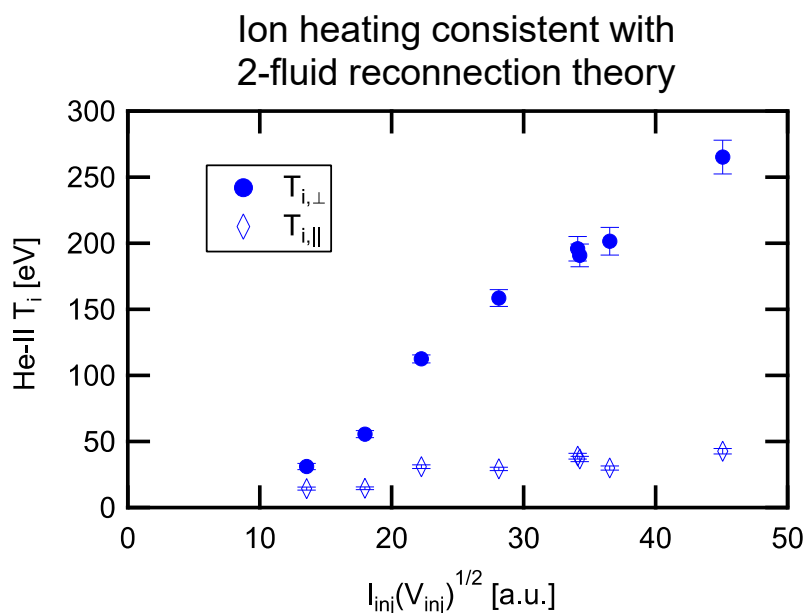
- Magnetics localize coherent streams in edge
  - Infers NIMROD streams in edge
- Reconnection-drive edge ion heating
- Any stochastic reconnection region may be localized to edge



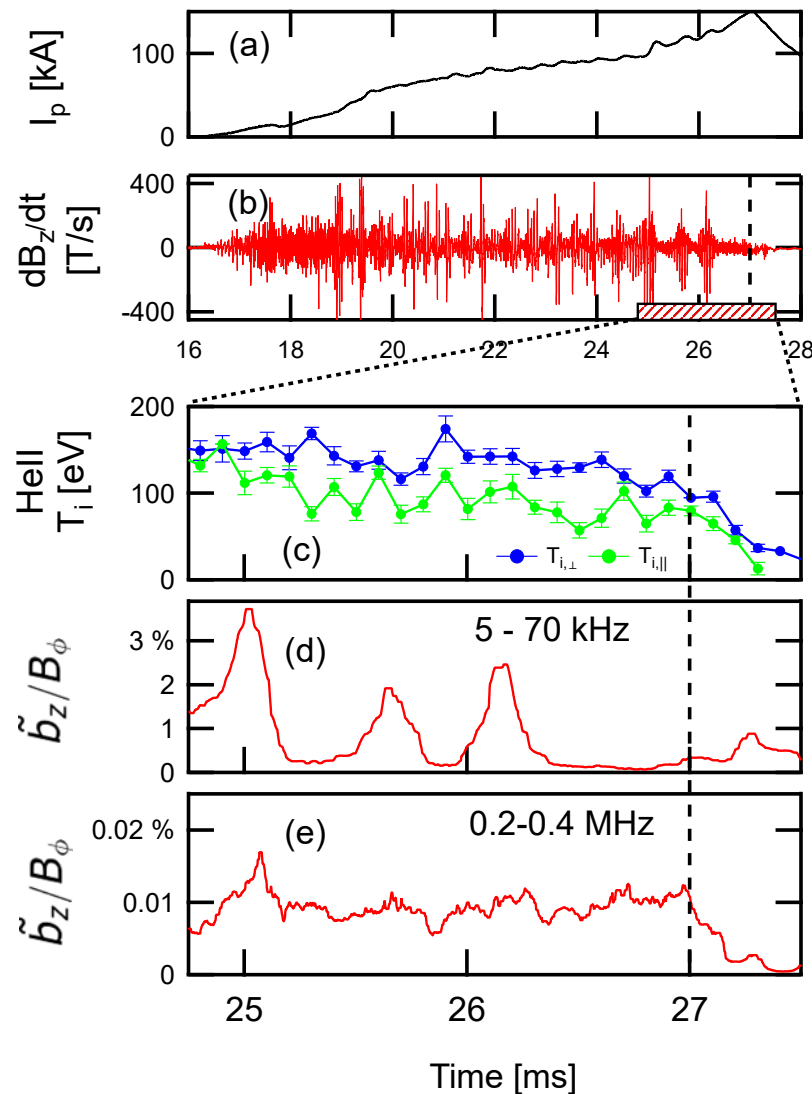


# Reconnection-Driven Ion Heating Gives $T_i > T_e$ During LHI

- Impurity  $T_i(0) \sim 100 - 500 \text{ eV} > T_e$  routinely observed during LHI
- Continuous ion heating from reconnection between collinear current streams
  - No effect on current drive efficiency
  - Significant ion heating ( $\sim \text{few } 0.1 \text{ MW}$ )



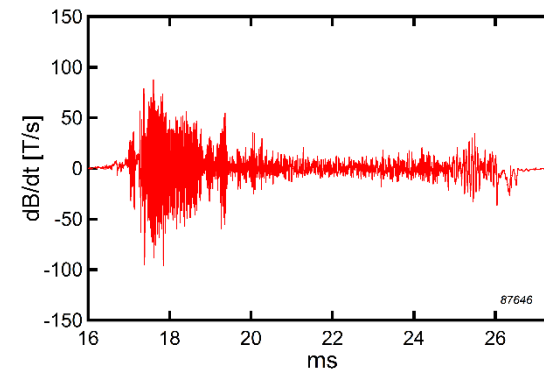
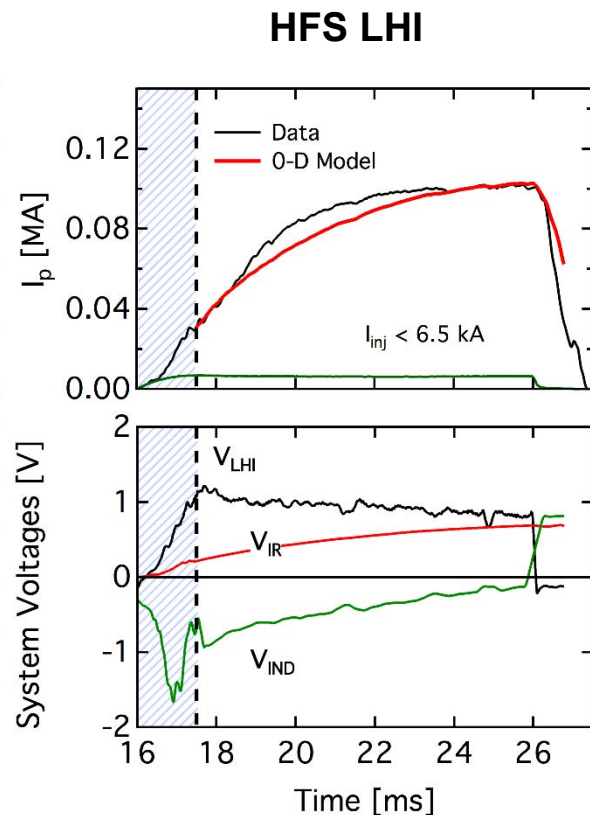
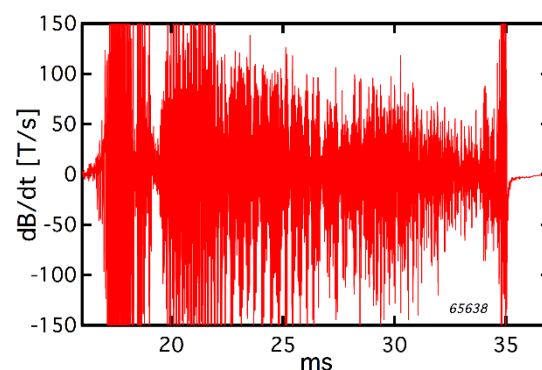
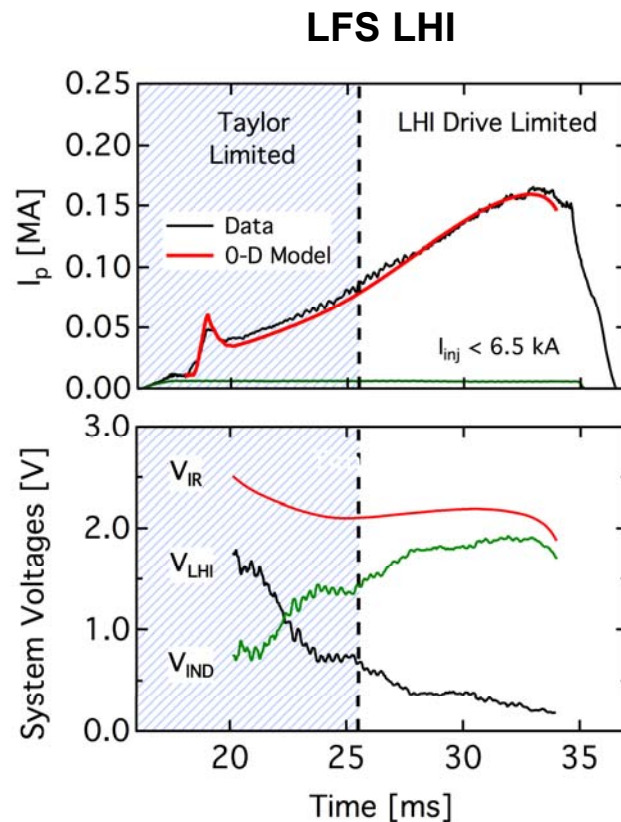
Ion heating correlated with high frequency MHD fluctuations, not with discrete reconnection between helical streams





# Different MHD Activity Observed Between LFS and HFS Injection Geometry

- LFS (outboard) injection:
  - MHD initially continuous, large amplitude,  $n = 1$
  - Transitions to intermittent bursts later in the discharge
  - Burst spacing increase with  $I_p$
  - Similar to NIMROD simulation
- HFS (inboard) injection:
  - Continuous, large-amplitude  $n = 1$  activity early on
  - Abrupt cut-off in large amplitude activity
  - Reduced  $n = 1$  magnitude for remainder of discharge
- Differences suggest multiple current drive mechanisms present

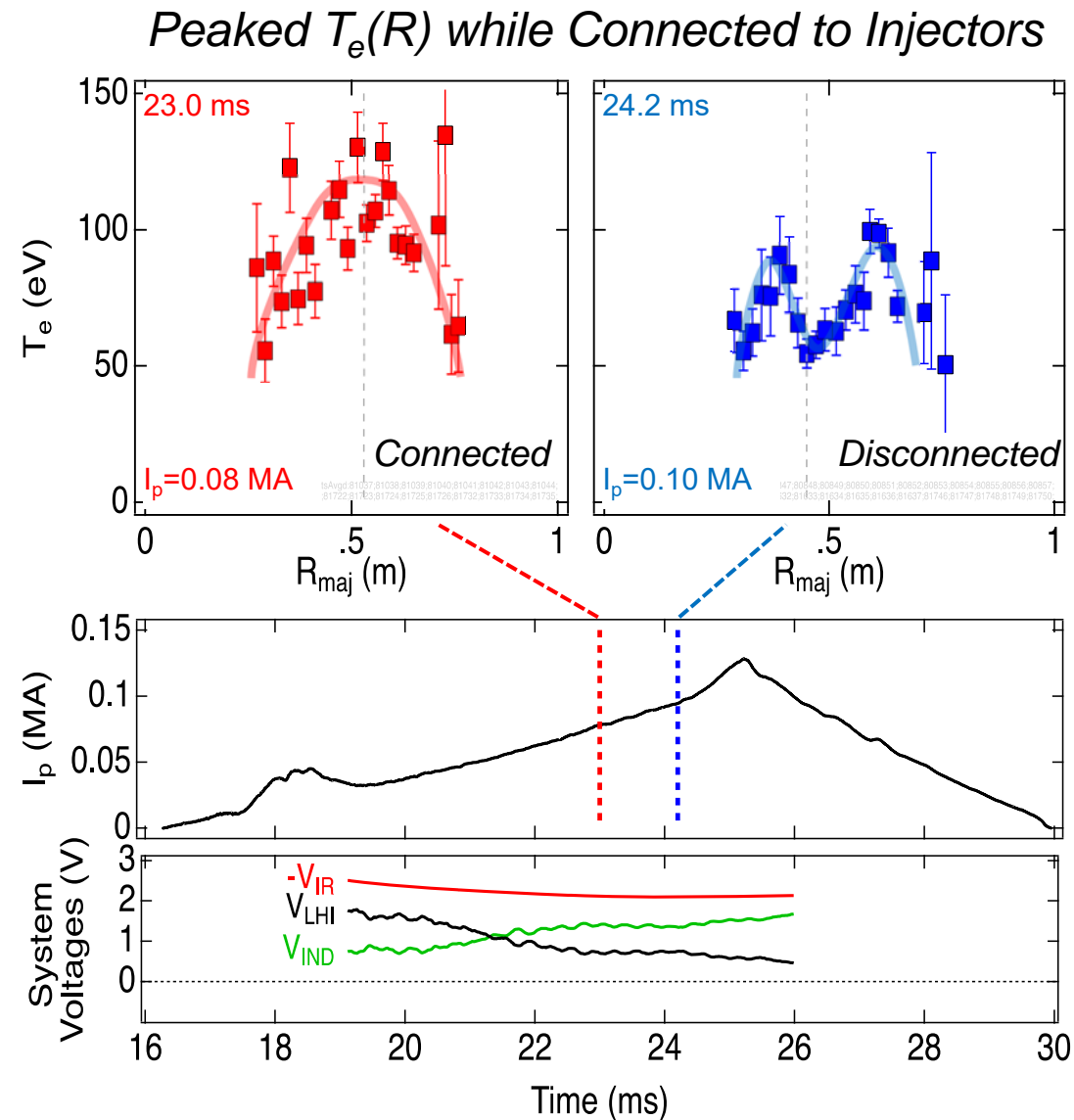






# LFS Local Helicity Injection Produces Core $T_e > 100$ eV

- Plasma shape grows inward from LFS injectors
  - Shape evolution generates  $V_{\text{IND}}$
  - $V_{\text{IND}} > V_{\text{LHI}}$  during high- $I_p$  phase
- Peaked  $T_e(R)$  during drive phase (connected)
  - Not strongly stochastic
  - After disconnect radial compression drives skin current
- Core  $n_e > 10^{19} \text{ m}^{-3}$ ,  
 $T_e \geq 100$  eV provides target for subsequent CD

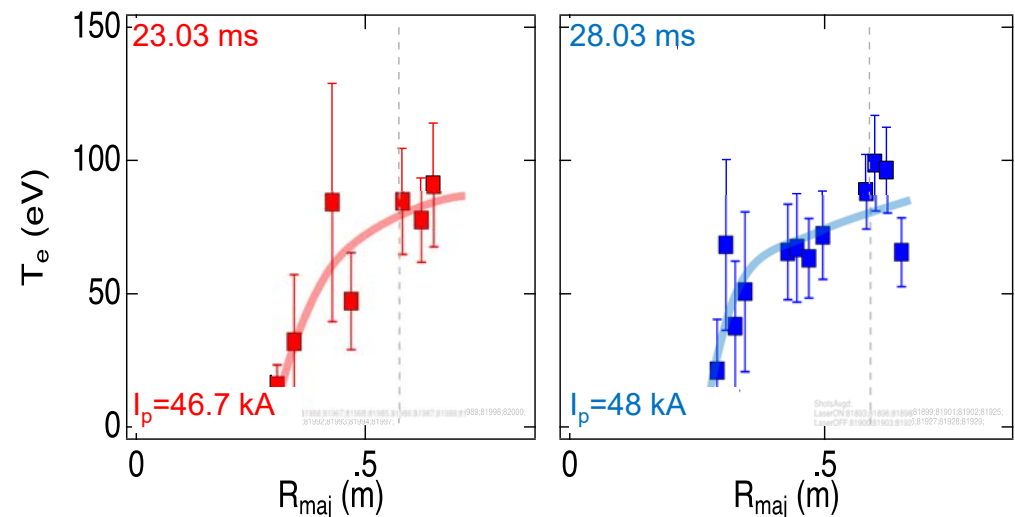




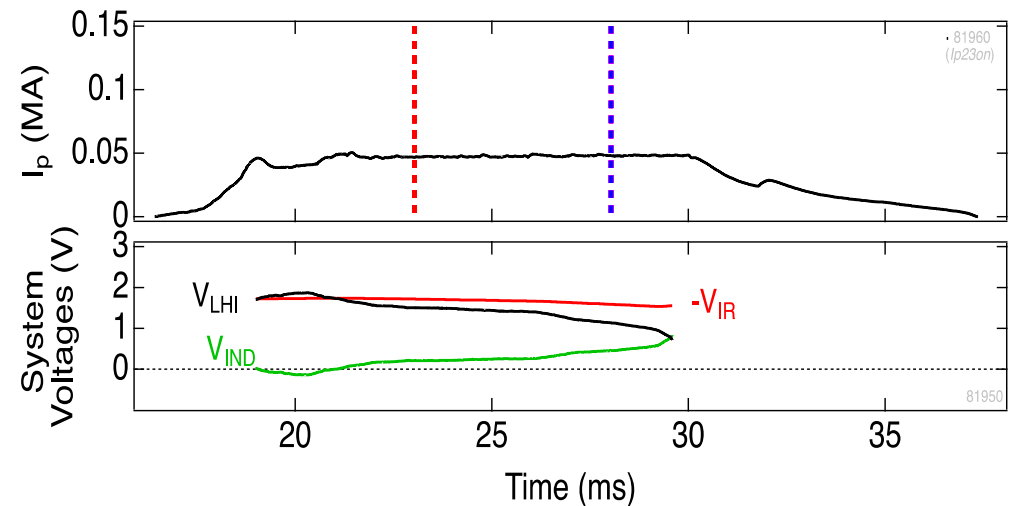
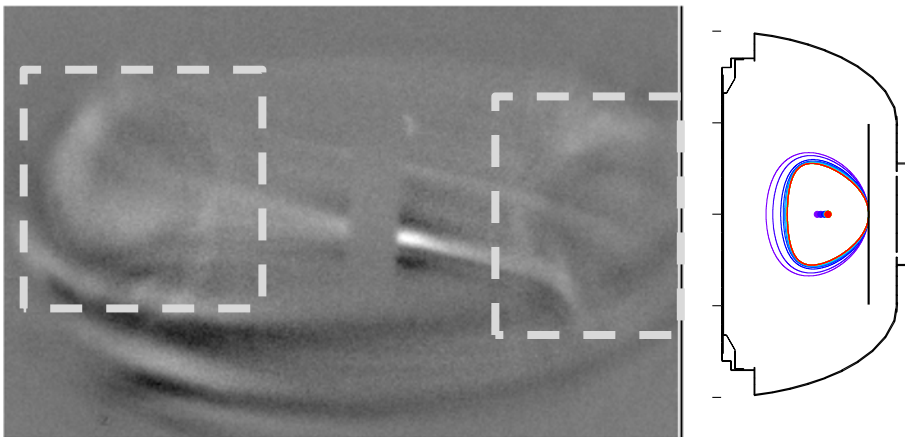
# $T_e(R, t)$ Remains Peaked for LFS Injection Geometry and Minimal $V_{IND}$

- Plasmas with same LFS LHI system and static geometry evolution
  - Lower performance due to shape constraint
    - High  $R_0$ , reduced  $A_{\text{plasma}}$
  - $V_{IND} \sim 0 < V_{LHI}$ ;  $T_e(0) \sim 80$  eV
- $T_e(R)$  peaked while driven by outboard LHI

$T_e(R) > 85$  eV with majority LFS LHI-drive



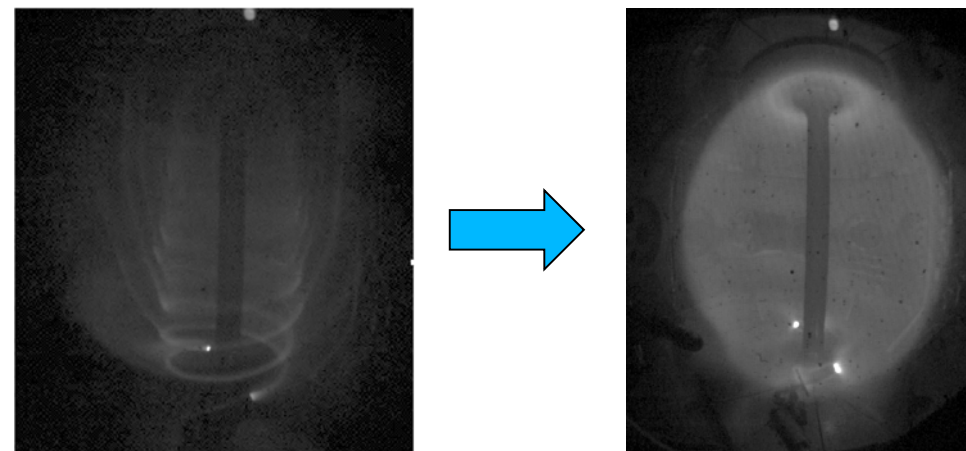
*Contrast-enhanced high-speed image and fast boundary reconstructions*





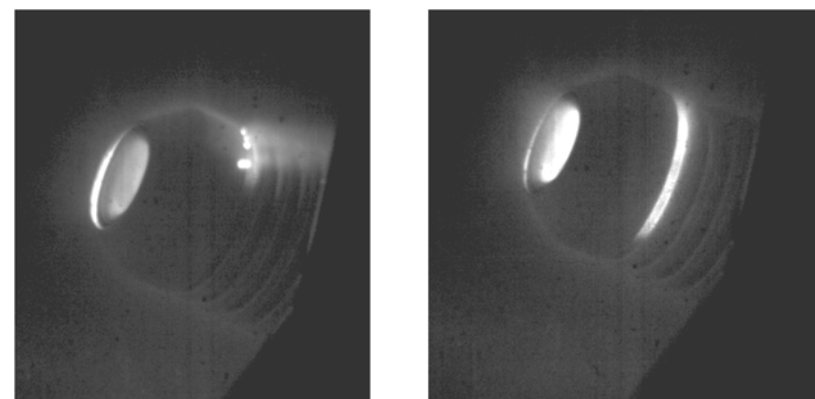
# Technical Challenges Arise for LHI Startup With HFS Injection Geometry

- Initial relaxation to tokamak state
  - More difficult for low  $R_{inj}$ , high  $B_{inj}$
  - Magnetic geometry constrained by injector clearance requirements
- Current source behavior at increased  $B_{inj}$
- Plasma-material interactions
  - PMI on injector surfaces
    - inhibits  $V_{inj}$
    - can damage injectors
  - PMI on machine surfaces
    - Impedes reproducibility
    - More severe for HFS injection



*Above: LHI plasma before and after relaxation*

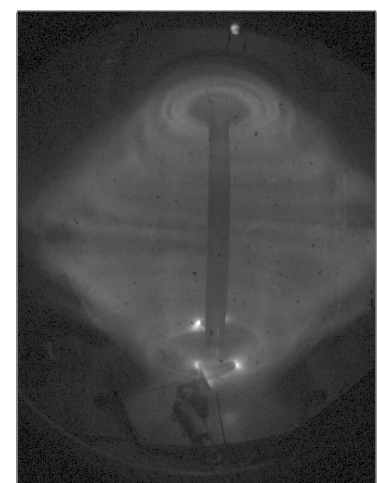
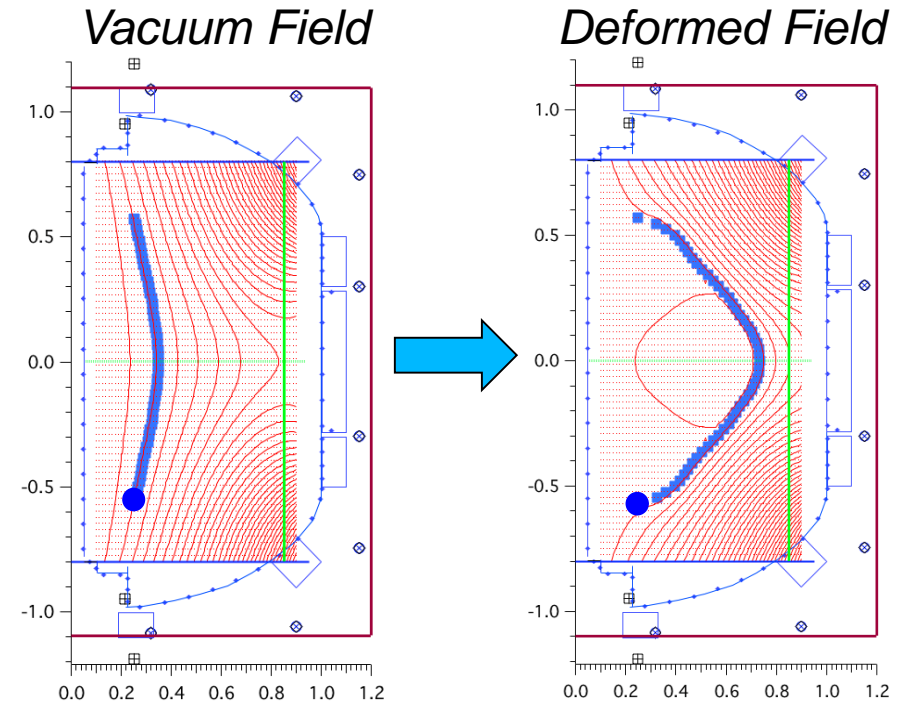
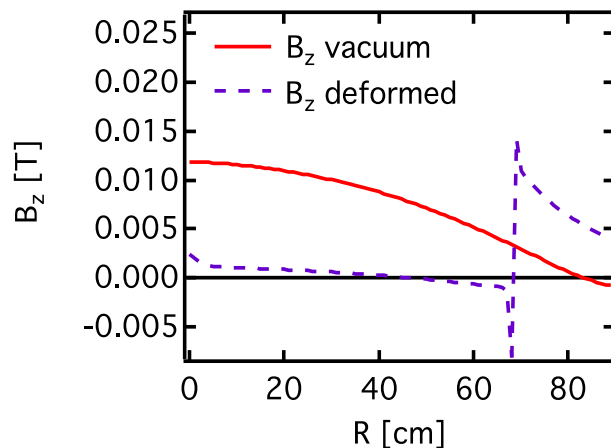
*Below: example of PMI on injector (left),  
eventually leading to insulator failure (right)*





# Poloidal Field Shaping Facilitates Relaxation at Full Toroidal Field ( $B_{inj} = 0.23$ T)

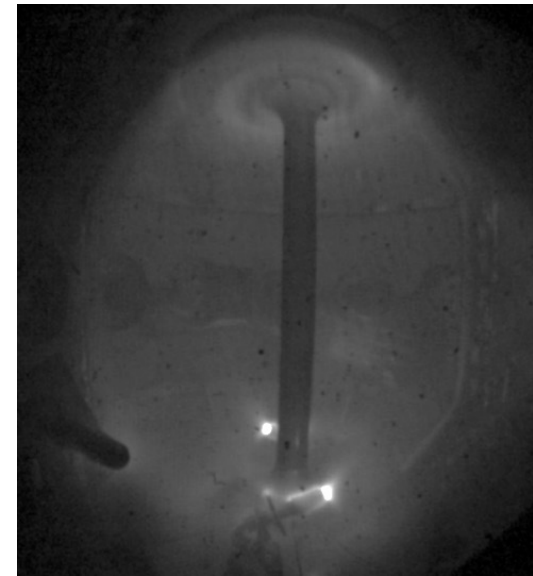
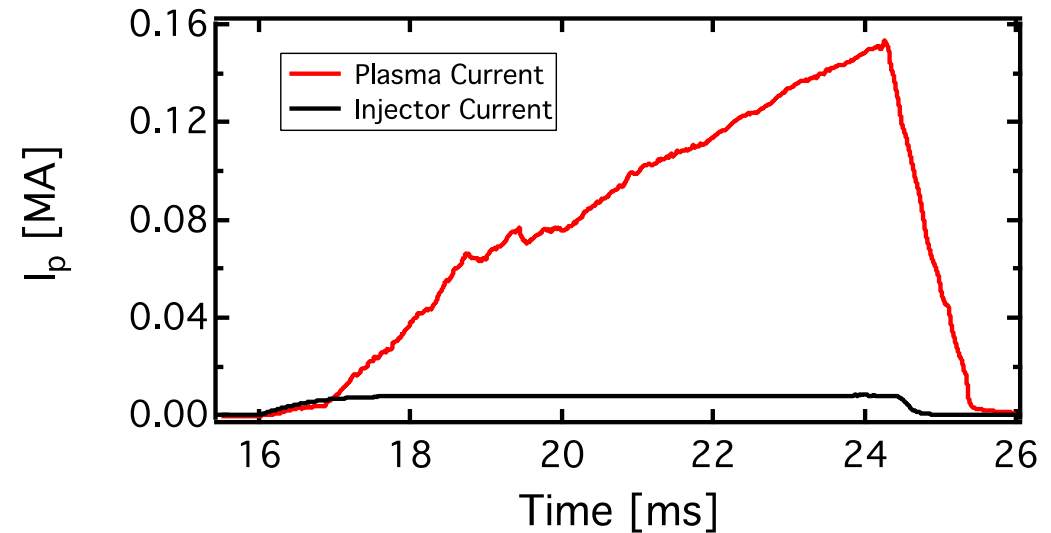
- Milestone for HFS LHI system achieved
- Technical challenge with HFS injectors:
  - Lower  $R_{inj} \rightarrow$  higher  $B_{TF}$  with respect to LFS system
    - $\rightarrow$  more  $B_z$  for injector clearance ( $\sim B_z/B_{TF}$ )
  - $B_{TF}$  increased  $\sim 10\times$  over previous experiments
    - $\rightarrow$  Relaxation at constant  $I_{inj}$  more difficult
- Poloidal field shaping key to full-field relaxation
  - Reduces midplane  $|B|$  and maintains injector clearance
  - Limited by  $I_{inj}$ -deformed streams contacting vessel





# $I_p > 0.15$ MA Achieved Via HFS Injection To Date

- $V_{LHI} \sim 1$  kV increased 2× over previous HFS LHI experiments
- Most operations at low field:
  - $B_{inj} = 0.046\text{--}0.092$  T
    - (20-40% of Pegasus maximum)
  - Reduced PMI, easier relaxation
- Full  $B_{TF}$  scenarios developed
  - $B_{inj} = 0.23$  T,  $I_{TF} = 0.288$  MA
  - $I_p \approx 0.1$  MA
  - PMI more prevalent at high  $B_{TF}$
- Injector geometry variants addressing observed PMI
  - Improvements found in each iteration

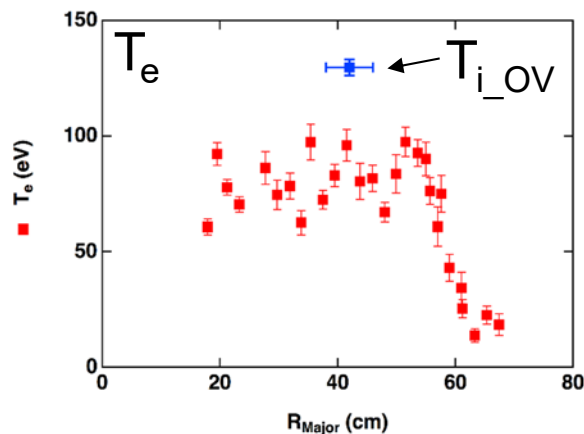
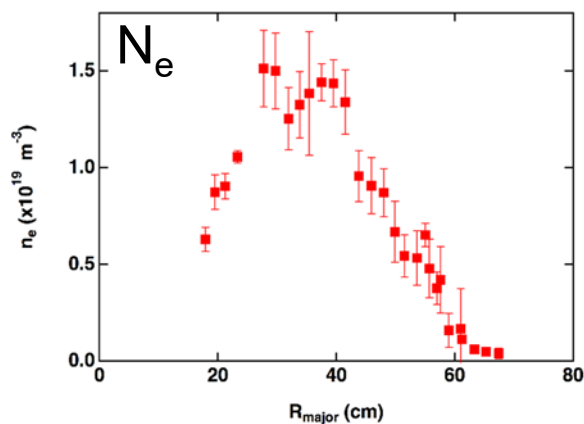




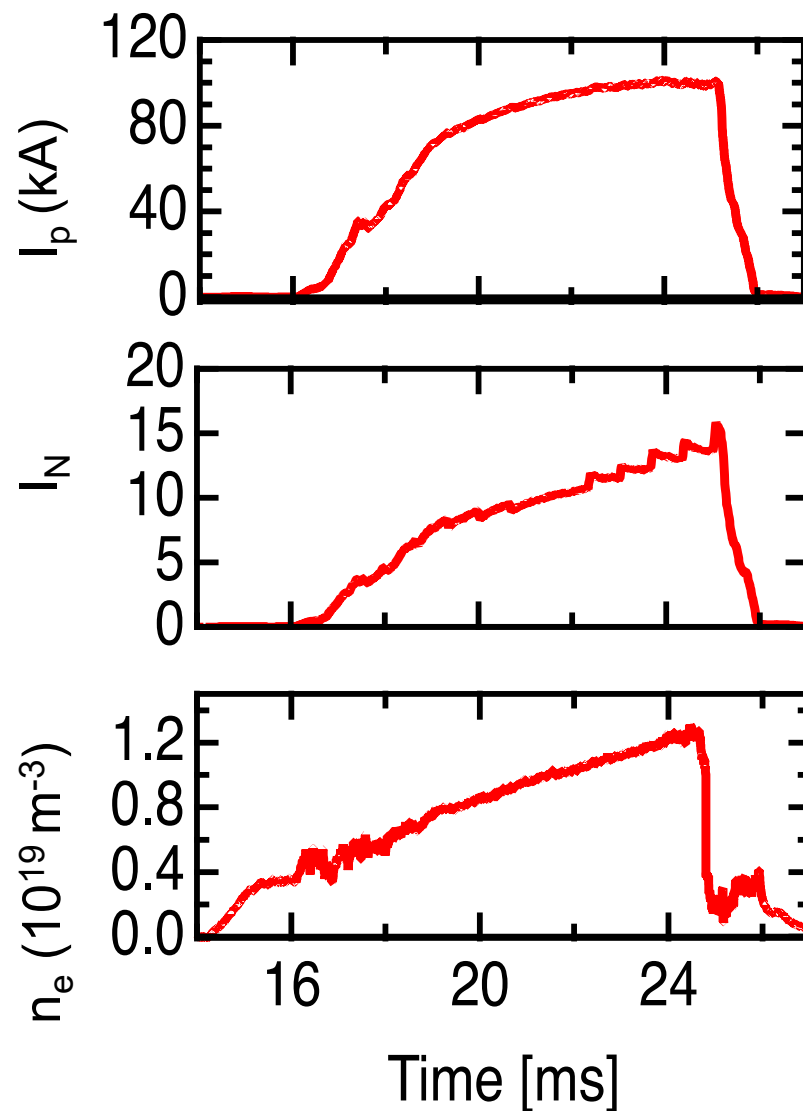


# HFS Helicity Injection Provides Non-Solenoidal Sustainment at High $I_N$

- Constant geometry: minimal  $V_{IND}$
- Low  $I_{TF} \sim 0.6 I_p$
- $I_N > 10$  accessible
  - Constant or ramped-down  $B_{TF}$
- Potential for high  $\beta_T$ 
  - Aided by anomalous ion heating



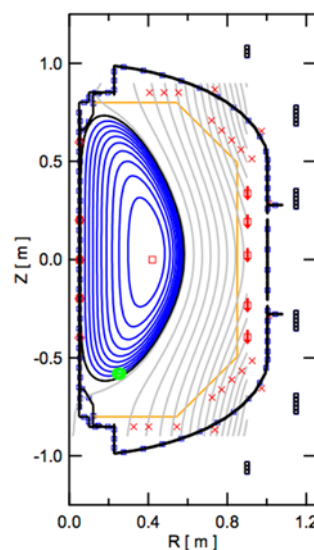
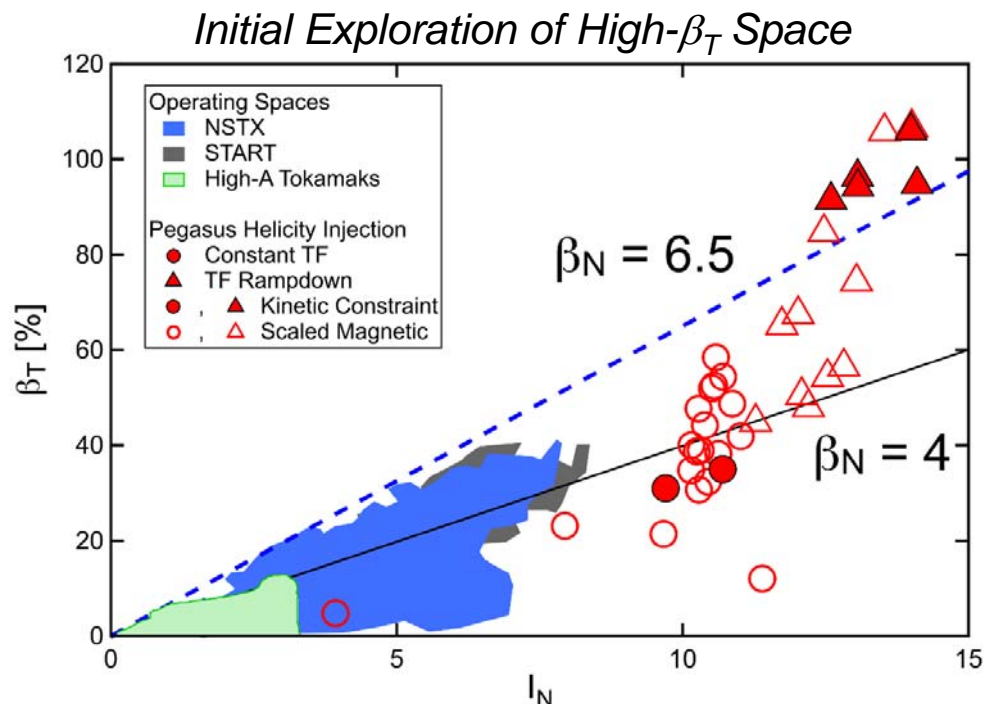
Access to  $I_N > 14$ ,  $n_e \sim 1 \times 10^{19} \text{ m}^{-3}$  with HFS Injection,  $B_{TF}$  Rampdown





# LHI Provides Access to High- $\beta_T$ at $A \sim 1$ with Non-Solenoidal Sustainment and Anomalous Ion Heating

- Equilibrium reconstructions with kinetic constraints used to determine  $\beta_T \equiv 2\mu_0 \langle p \rangle / B_{T0}^2$ 
  - Matches external magnetics,  $p_{\text{tot}}(0)$ , and edge in  $T_e(R)$
  - Includes anomalous  $T_i(0)$
  - Some caveats for these initial results
    - Assumes closed flux surfaces inboard of injectors
    - Role of SOL edge current
    - Magnetics-only reconstructions scaled via comparison to those with kinetic constraints
    - Need full kinetic profiles in future
- High  $\beta_T$  plasmas often terminated by disruption
  - $n = 1$ , low- $m$  precursors
- Expands accessible high  $I_N$ ,  $\beta_T$  space for tokamak stability studies at extreme toroidicity
  - Campaign underway to document, extend to higher  $I_p$
  - Improving LHI injector hardware to increase  $I_p$ ,  $B_{TF}$  access



Equilibrium Parameters  
Shot 87332, 24.50 ms, Undo 72

$I_p$	102 kA	$R_0$	0.317 m
$\beta_t$	0.95	$a$	0.263 m
$\ell_i$	0.22	$A$	1.21
$\beta_p$	0.45	$\kappa$	2.6
$W$	545 J	$\delta$	0.54
$B_{T0}$	0.0249 T	$q_{95}$	7.24





# Progress in Non-Solenoidal Startup on Pegasus

- LHI provides high  $I_p$ , non-solenoidal tokamak startup
  - Flexible injection geometry balances  $V_{LHI}$  and  $V_{IND}$  drive, engineering constraints
  - Improved power balance model suggests technique is scalable to larger devices
  - Questions remain on confinement and reconnection dynamics
    - Thomson scattering: Peaked  $T_e$ ,  $n_e$  suggest favorable realized confinement
- New high-field-side injector systems exploring strong  $V_{LHI}$  limit
  - Injector operation and relaxation to tokamak demonstrated at full TF ( $B_{inj} \sim 0.25$  T)
  - Completely  $V_{LHI}$  driven startup and sustainment realized
  - Non-solenoidal  $I_p(t)$  via LHI enables access to stability tests at extreme toroidicity
    - Sustained operation at high  $I_N$ , high  $\beta_T$
- Present campaign:
  - Optimize HFS injector implementation to mitigate PMI at high  $B_{TF}$
  - Develop high  $I_p$  scenarios to test scalings in LFS, HFS geometries
  - Design CHI system for comparison studies (with PPPL, U. Wash)



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