

# Instrumentation Development for a Novel Local Electric Field Fluctuation Diagnostic

M.R. Bakken, M.G. Burke, R.J. Fonck, D.J. Fuerstenberg,  
B.T. Lewicki, M.M. Liben, A.T. Rhodes, and G.R. Winz



University of  
Wisconsin-Madison

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# Introduction



# Measurements of Electric Field Fluctuations are Desired for Validating Tokamak Core Turbulence and Transport Models

- $\tilde{E} = k_{\perp} \tilde{\phi}$  measurements are underdiagnosed in tokamaks and integral to turbulent plasma physics
  - Provides:
    - $\tilde{v}_r$ : cross-field transport
    - $\tilde{v}_{\theta}$ : transport barrier
- A novel high-speed, high-throughput spectrometer is being developed to measure local  $\tilde{E}$  up to 500 kHz
  - $U \cong 0.1 \text{ cm}^2\text{-ster}$
  - Spectral resolution  $\cong 0.5 \text{ \AA}$
- A low-divergence, 80keV diagnostic neutral beam from PPPL is being refurbished to support the  $\tilde{E}$  diagnostic
- A magnetized test chamber with  $B_T > 0.5 \text{ T}$  and tokamak-like density planned for diagnostic testing



# $\tilde{E}$ Levels Projected by Tokamak Fluctuation Scaling

- Estimate of drift wave fluctuations can be obtained from scaling relations of density and electrostatic potential fluctuations<sup>1</sup>:

$$\frac{\tilde{n}}{n} \sim \frac{e\tilde{\phi}}{T_e}$$

- Turbulence peaks at perpendicular wavenumbers of order unity inverse ion gyroradius at the local  $T_e$

$$k_{\perp} \rho_s \sim \alpha$$

- Various tokamaks have found  $\alpha$  ranging from 0.1 – 1

- Taking  $\tilde{E} \sim k_{\perp} \tilde{\phi}$ :

$$\tilde{E} \approx \frac{\tilde{n}}{n} \frac{T_e}{e \rho_s} \alpha \approx \frac{T_e}{e a}$$

- Where  $a$  is the plasma radius

<sup>1</sup> Wesson, J. Tokamaks. Oxford, UK: Clarendon Press, 2004.



# Measuring $\tilde{E}$ is Challenging, but Possible Against Background Motional Stark Effect

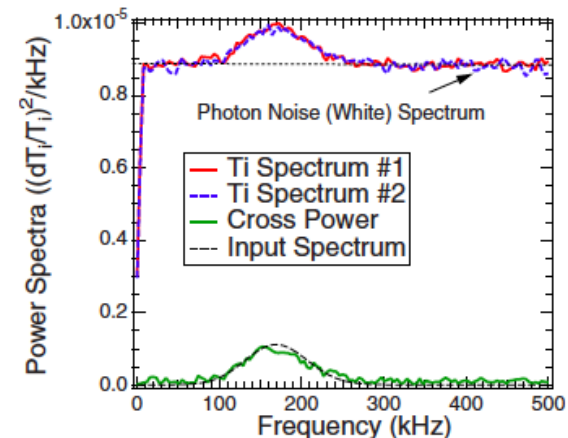
Experiment	$T_e(\text{eV})$	$B(\text{T})$	$a \text{ (m)}$	$\tilde{E}/E_{\text{MSE}}$
Pegasus - 1	100	0.15	0.3	$1 \times 10^{-3}$
Pegasus - 2	300	0.3	0.35	$1.4 \times 10^{-3}$
NSTX-U	$\sim 2000$	1	0.6	$\sim 2.6 \times 10^{-3}$
DIII-D	2000	2	0.7	$0.7 \times 10^{-3}$

- Across devices  $\tilde{E}/E_{\text{MSE}} \sim 0.1\%$



# Two-point correlation can extract $\tilde{E}$ , similar to present Turbulence Diagnostics

- $\tilde{T}_i$  and  $\tilde{n}$  are known to be small:
    - $\tilde{T}_i/T_i \sim 10^{-2}$  (HF/UF-CHERS)<sup>1</sup>
    - $\tilde{n}/n \sim 10^{-2}$  (BES)<sup>2</sup>
  - Anticipated  $\tilde{E}/E_{\text{MSE}} \approx 10^{-3}$ 
    - Comparable to photon noise floor  $\sim 10^{-3}$
  - To extract  $E$ ,
    - cross correlate with BES signal
      - Similar to UF-CHERS
- $$\langle \tilde{E}_T \tilde{n}_T \rangle = \langle (\tilde{E}_p + \tilde{E}_\gamma)(\tilde{n}_p + \tilde{n}_\gamma) \rangle$$
- $$\approx \langle E_p n_p \rangle$$
- Two-point cross-correlation of overlapping  $E$  signal
 
$$\langle E_{T_1} E_{T_2} \rangle \approx \langle E_{p_1} E_{p_2} \rangle$$



<sup>1</sup> H.T. Evensen et al., Rev. Sci. Instrum. **66**, 845 (1995)

<sup>2</sup> R.J. Fonck et al., Phys. Rev. Letts **70**, 3736 (1993)

<sup>3</sup> G.R. McKee et al., Rev. Sci. Instrum. **79**, 10F528 (2008)





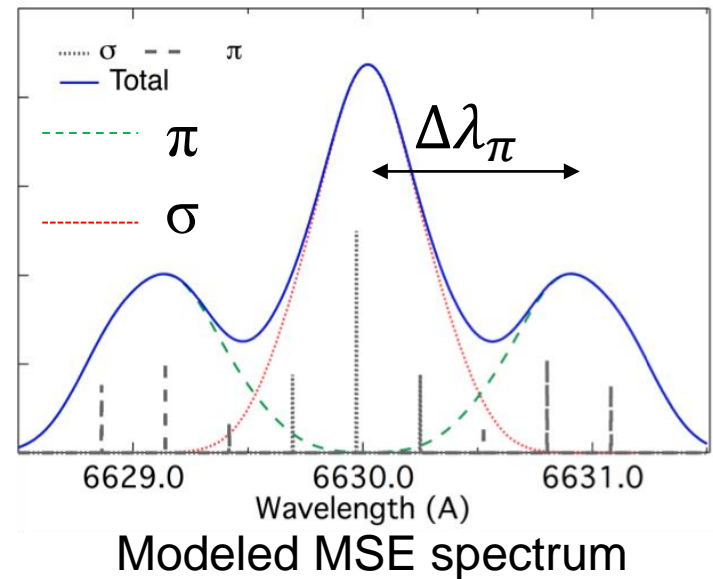
# Measurement Technique

# Local $\tilde{E}$ Results in Fluctuations in the Stark Manifold

- The measured field is

$$\mathbf{E}_{\text{tot}} = \mathbf{E}_{\text{plasma}} + \mathbf{v}_{\text{beam}} \times \mathbf{B}$$

- For 80 keV beam,  $B_T = 0.3\text{T}$
- $E_{\mathbf{v} \times \mathbf{B}} \approx 1\text{ MV/m}$
- Two measurement methods:
  - $\frac{\pi}{\sigma}$  line ratio
  - $\Delta\lambda_{\pi}$ : separation of  $\pi$  lines



1 H. A. Bethe & E. E. Salpeter. *Quantum Mechanics of One- and Two-Electron Atoms*. New York: Dover Publications, Inc., 1957.  
 2 H. Y-H. Yuh, PhD Thesis, MIT (1995).



$$\tilde{\vec{E}}_{plasma}(t)$$

- Midplane beam, sightline: linewidth changes

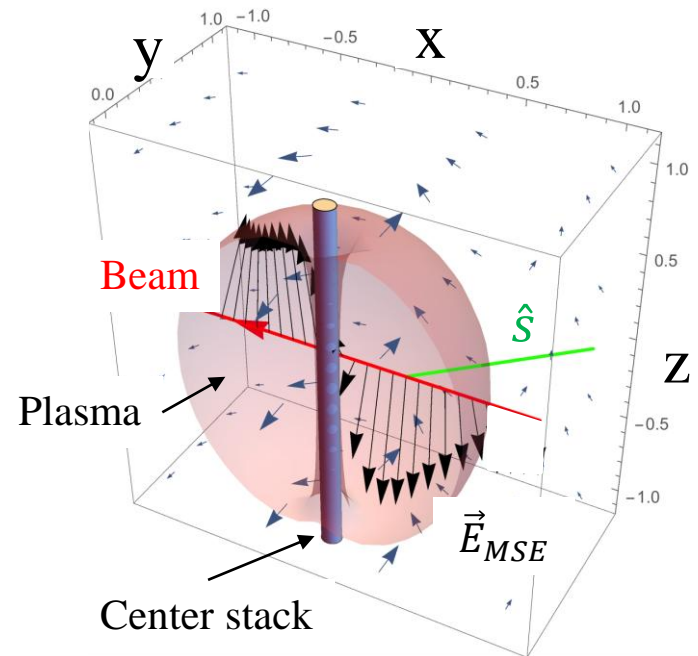
$$\widetilde{\Delta\lambda}_{Stark} \propto \tilde{E}_z$$

- Midplane beam, off-midplane sightline: Intensity ratio change

$$R = \frac{\sum I_{\pi}}{\sum I_{\sigma}} \propto \tilde{E}_R F(\tilde{n})$$

- First emphasis on line width measurement: insensitive to density fluctuations

Example: ST Geometry





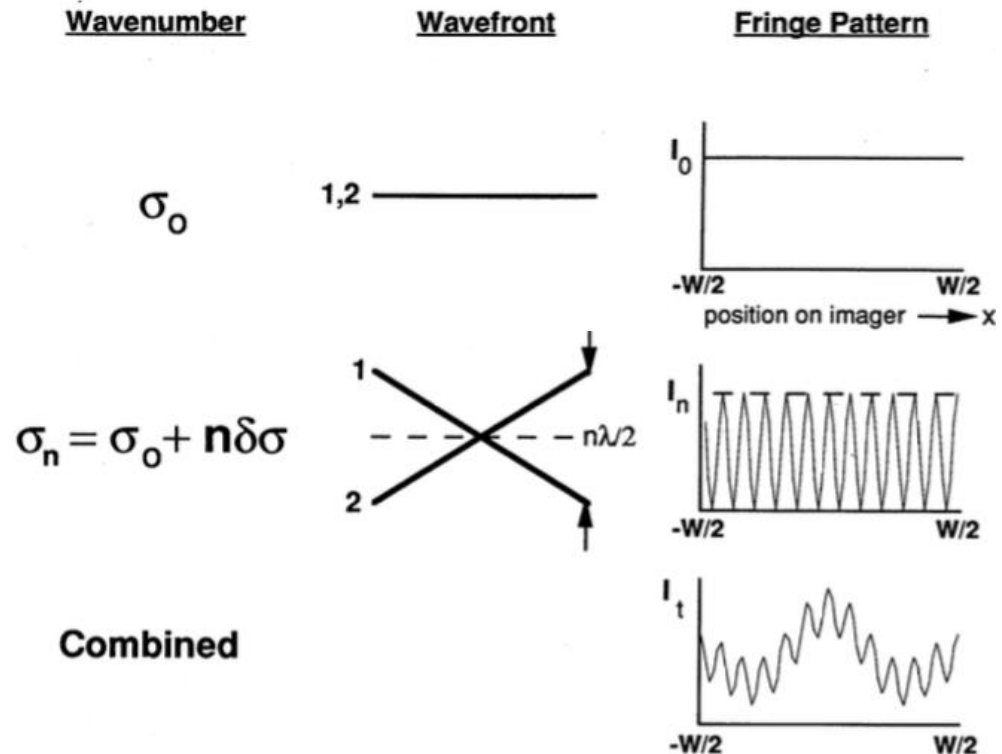
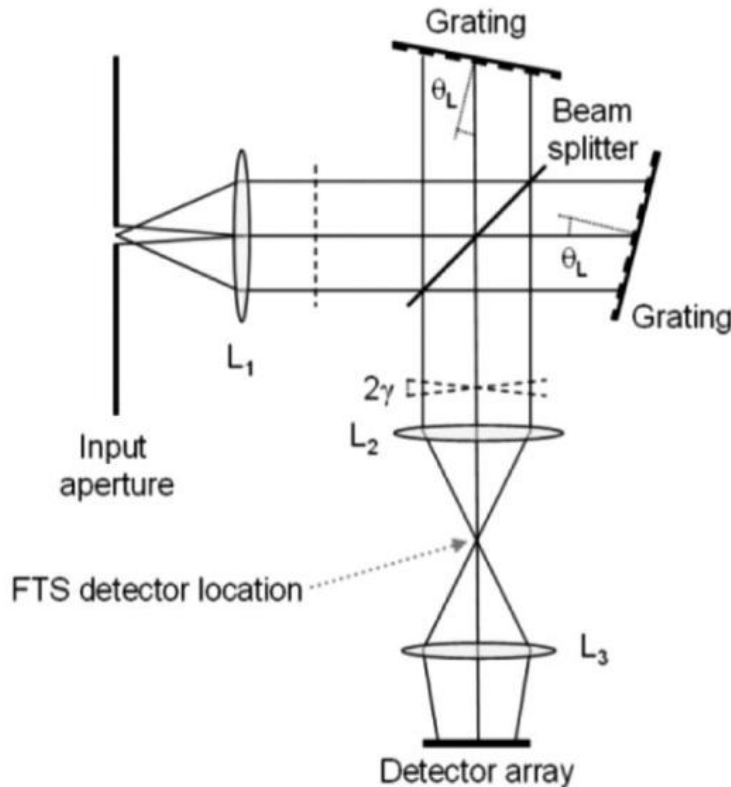
# Spectrometer Requirements are Formidable for $\Delta\lambda_\pi$ Measurement

- Resolution:
  - Need  $\sim 8$  spectral elements to resolve 2 gaussian  $\pi$  components
  - $\Delta\lambda_\pi \sim 4 \text{ \AA}$  giving a spectral resolution of  $0.5 \text{ \AA}$ 
    - $R = \frac{\lambda}{\delta\lambda} \sim 1.3 \times 10^4$
- Etendue (optical throughput):
  - Matched to port availability and collection optics
  - $U = 0.1 \text{ cm}^2\text{-ster}$
  - 2 spatial points
- Compatible Detector System:
  - $\sim 250\text{kHz}$  time response
- Mitigation of sightline-DNB broadening, low beam divergence, very good beam stability, high species fraction

*H. Evensen, PhD Thesis, UW-Madison (1996)*

# Spatial Heterodyne Spectroscopy + New High-Speed 2D Detectors → Powerful Spectrometer Concept

- Self scanned, 2 beam interferometer

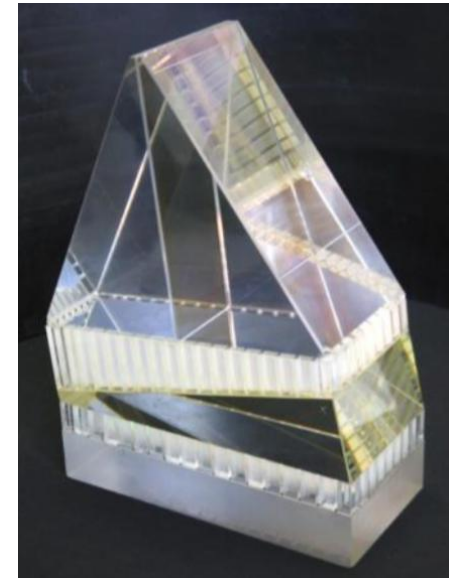


$$I(x) = \int_0^{\sigma} B(\sigma) (1 + \cos[2\pi(4|\sigma - \sigma_0|x \tan \theta_L)]) d\sigma$$

# Spatial Heterodyne Spectroscopy Achieves High Resolution and Throughput

- SHS theoretical resolving power:
  - $R = \sigma / \delta\sigma \approx 2W/d$
  - For  $\tilde{E}$ : Need  $R \sim 1 \times 10^4$
  - For  $W = 50$  mm only requires  $d = 1/100$  lines/mm
  - Resolution readily achievable with simple coarse gratings, compact size
- SHS throughput comparable to field widened Fourier Transform spectrometer
  - For  $\tilde{E}$ : need throughput of  $0.05$ - $0.1$   $\text{cm}^2\text{str}$
  - $U = 2\pi\epsilon A/R = \eta * 0.015$  ;  $\eta \sim 1$  (no field widening) –  $100$  (field widening)
- Required throughput readily achievable in SHS

## DASH Interferometer



$R \approx 5 \times 10^4$ ,  $U \approx 0.15$   $\text{cm}^2\text{str}$

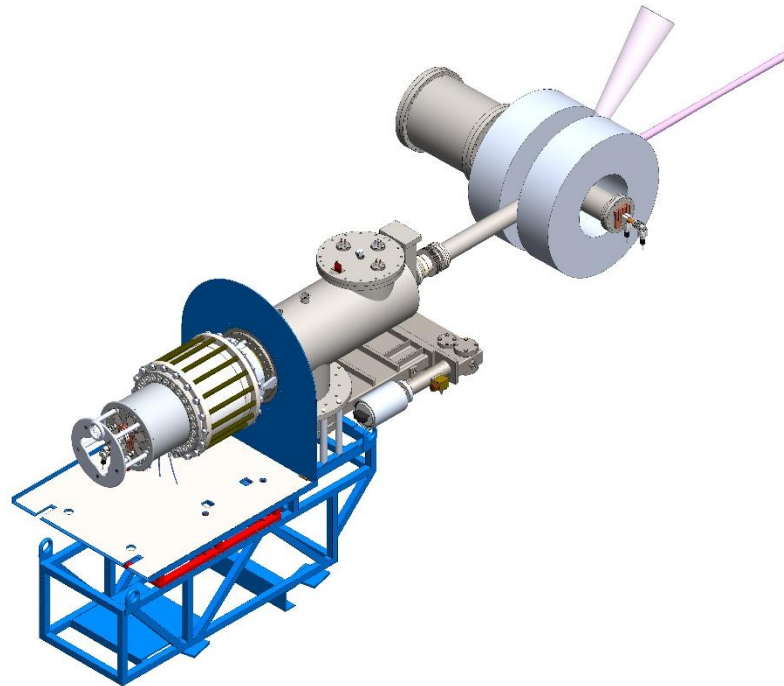
J. M. Harlander, C. R. Englert, D. D. Babcock, and F. L. Roesler, Opt. Express, OE, **18**, 2010.



# Diagnostic Beam and Target Chamber

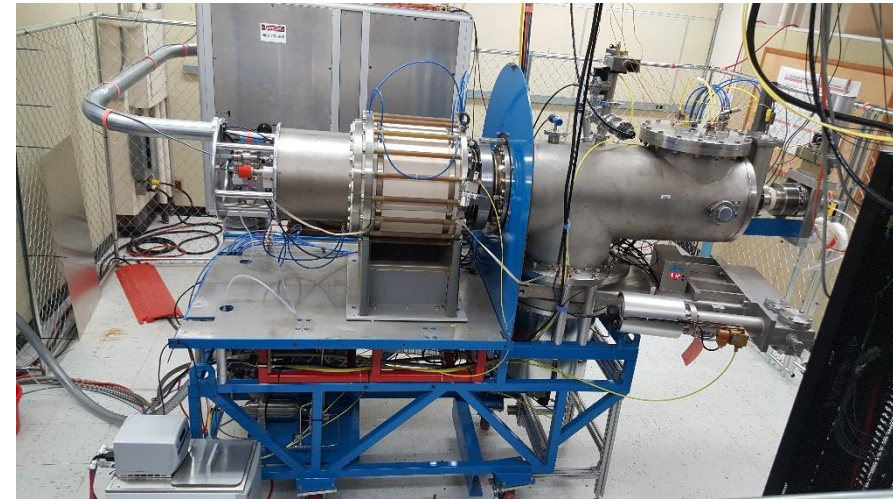
# High Performance Beam Eases $\tilde{E}$ Measurement

- Beam produced by Culham for PPPL meets beam requirements necessary for E-field fluctuation measurements
  - Low divergence
  - High energy
  - High species fraction (new active arc source)
- Initial deployment will be on a magnetized target chamber



# Diagnostic Requires High Energy, Low Divergence Beam

- Using DNB on loan from PPPL
  - $H^0$
  - Extracted Ion Current: 2-3 A
  - Full-energy  $J$  at focus: 3-6 mA/cm<sup>2</sup>
  - Diameter ~ 9cm
  - Pulse Length ~ 100ms
- Favorable features
  - Low divergence:  $\leq 0.47^\circ$ 
    - Mitigates divergence line broadening
  - High  $E_b \sim 60 - 80$  keV
    - Maximizes MSE broadening
  - 90-95% ionization at full beam energy
    - New plasma arc source
    - Optimize signal at full energy component



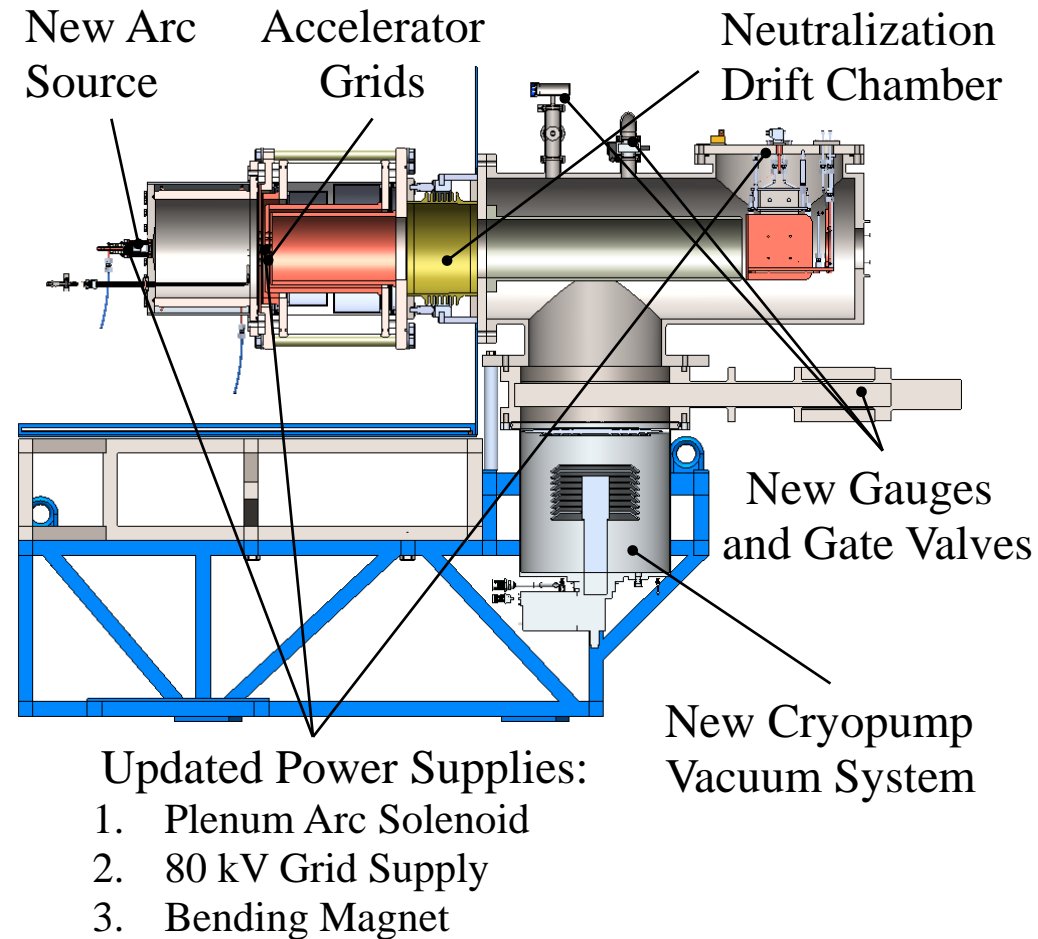
J.R. Coupland et al, *Rev. of Sci. Instrum.* **61**, 472 (1990)  
 I.L.S. Gray et al, *IEEE* **1**, 149 (1989)

M. R. Bakken, HTPD 2016



# DNB Significantly Refurbished for $\tilde{E}$ Diagnostic Development

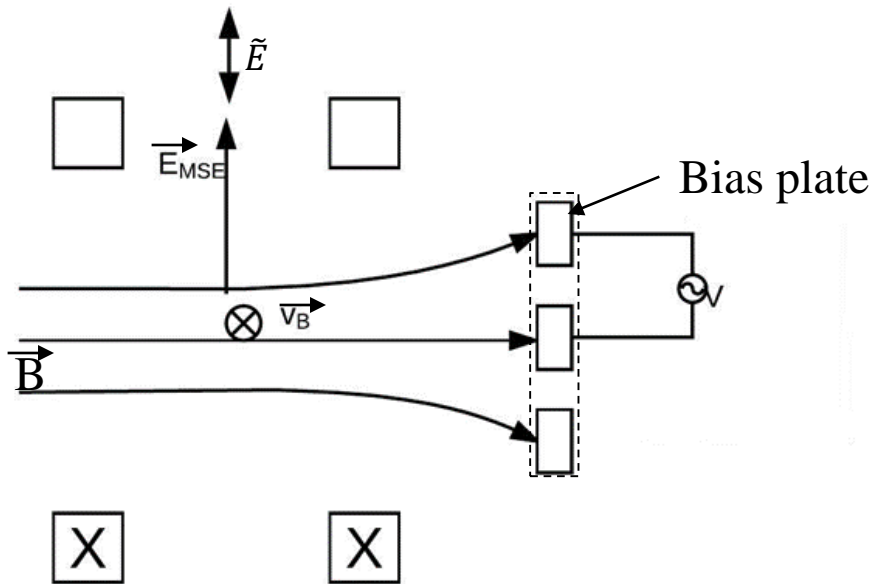
- New Active Arc Source
  - High full energy species fraction
- Vacuum System
  - All new seals and pump
- New Power Systems
  - Low ripple, 80kV power supply
  - Arc source power supply
- New Control Systems
  - NI FPGA and DAQ controlled with LabView



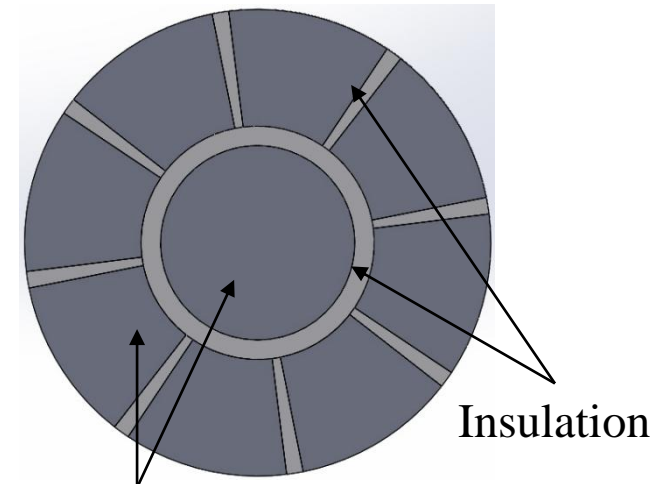


# Target Chamber Designed to Induce Local $\tilde{E}$

- Bias plate at target chamber end used to induce fluctuations
  - Potential oscillations between conducting surfaces induces  $\tilde{E} || E_{MSE}$
  - Oscillating the right/left sides induces  $\tilde{E} \perp E_{MSE}$



**Segmented plate allows parallel and perpendicular fluctuations**



Conducting surface



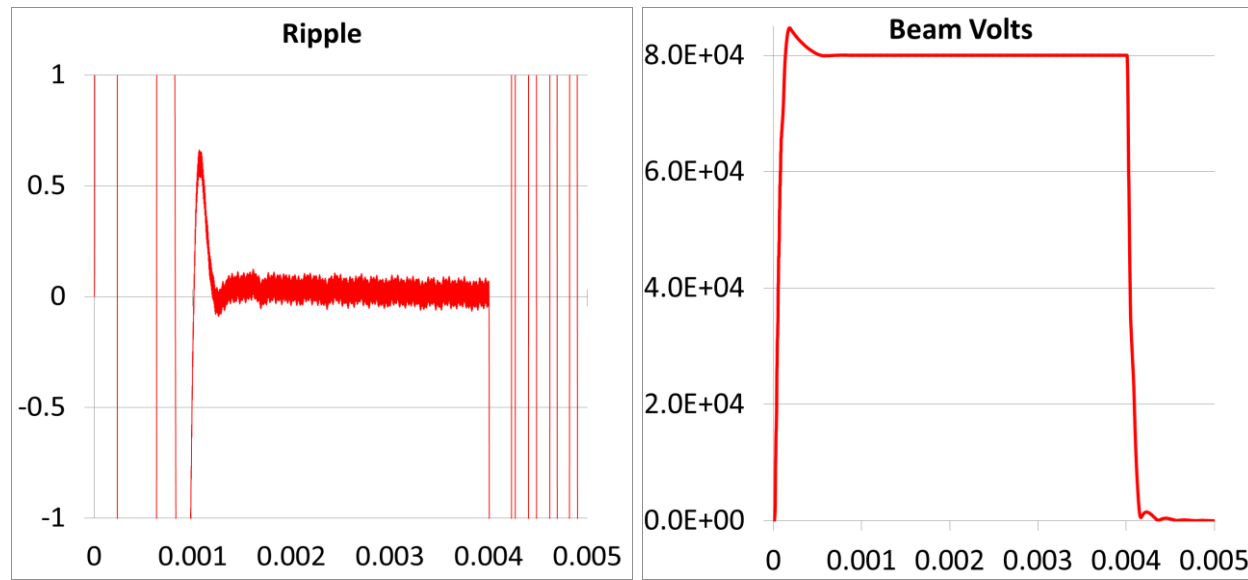
# Novel Power Supply



# Low Ripple, 80keV High Voltage Power Supply Designed and Fabricated

- New power system required for diagnostic development
- High energy, flat voltage power supply
- Resonant converter topology for low voltage ripple

## Simulated Performance with PLECS



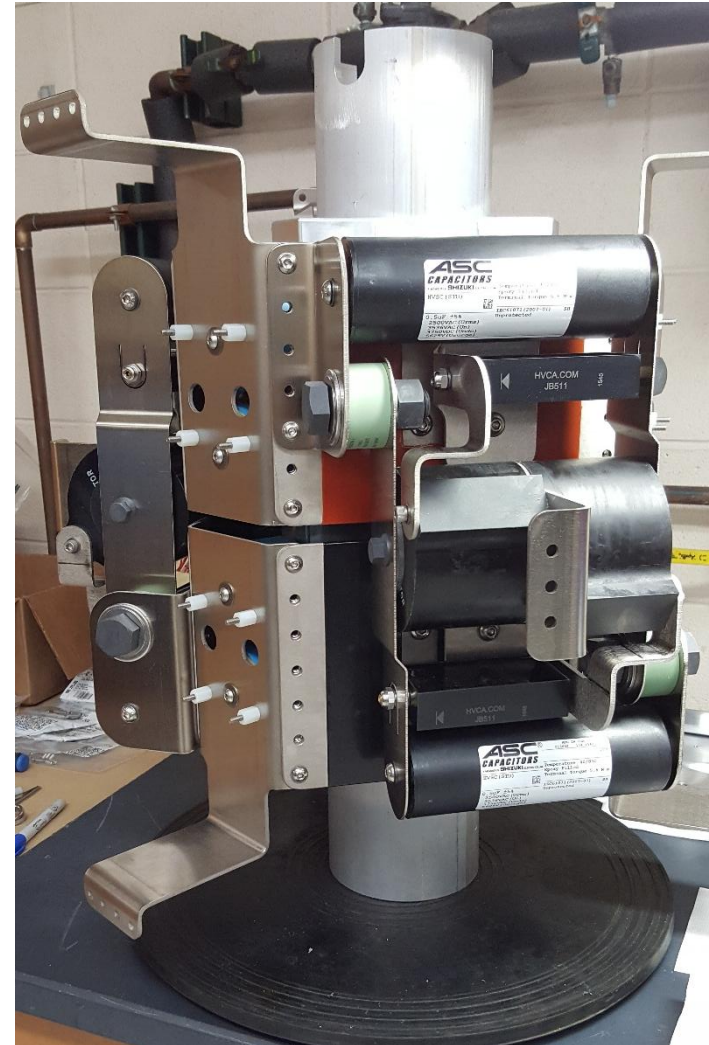
## Assembled Power Supply



# 80kV / 400kW Resonant Converter Implemented with IGBT Switches

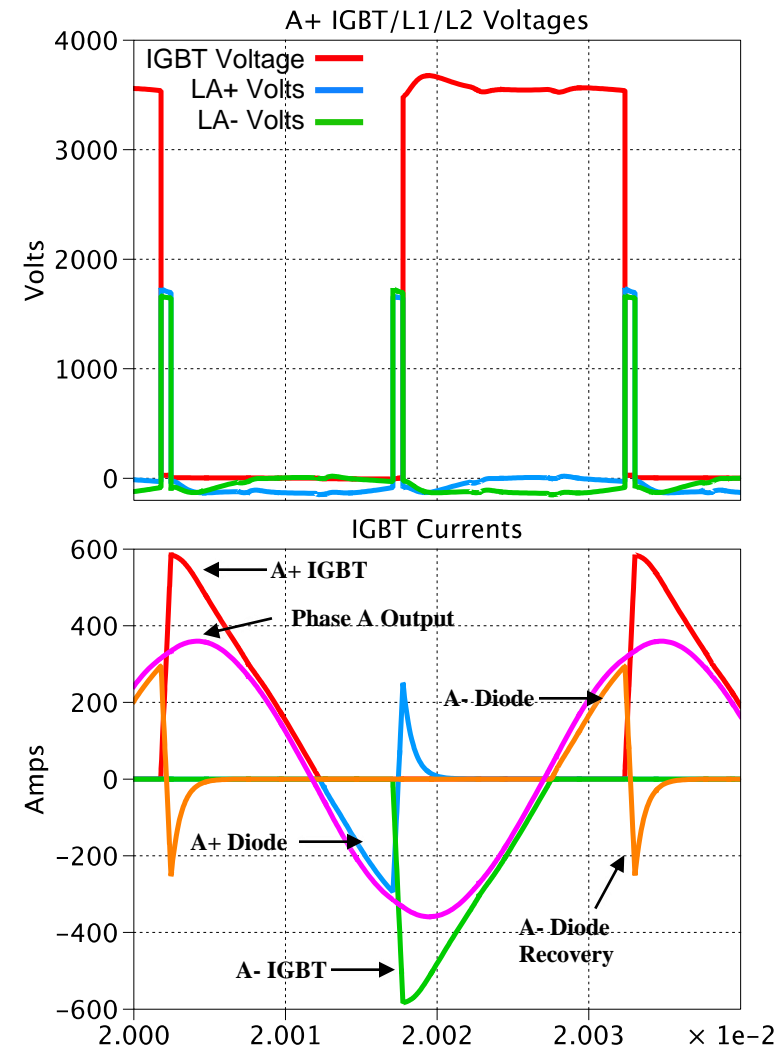
- Resonant Converter
  - 35 kHz Base Switching Frequency
  - 3 single phase transformers
  - Fast Rise/Fall time ( $< 200\mu\text{sec}$ )
  - Low filter energy (1J)
  - Low voltage ripple ( $\pm 0.00025\%$ )
  - Low energy per cycle (2J)
  - Low primary stored energy (120kJ)
  - Gain is load dependent
  - Excellent fault behavior
- FPGA Control
  - 40 MHz Base Frequency
  - Digital Control

400kW / 3600V 3-Phase Primary Bridge



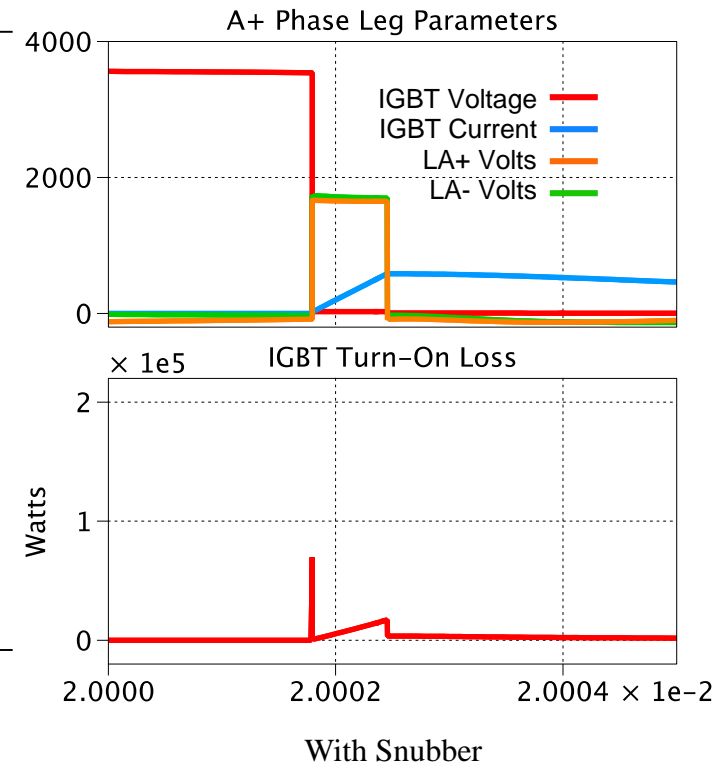
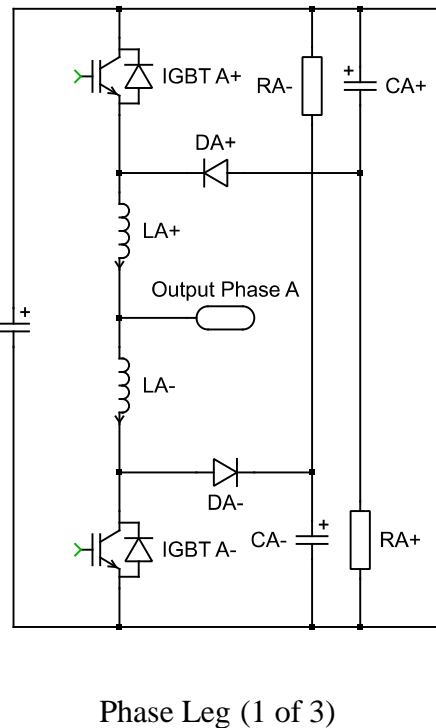
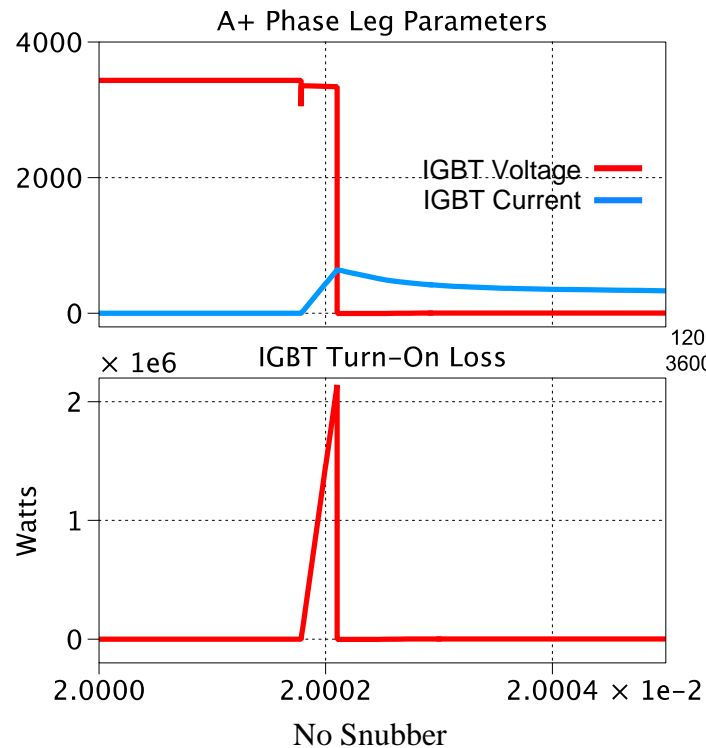
# Zero Voltage/Zero Current Switching Provides Minimal System Losses

- What is ZVC/ZCS
  - Passive commutation
  - IGBT turn-off losses are zero
  - Diode commutation at zero voltage (with snubber)
  - Lower system losses allows higher frequency operation
  - Higher frequency allows for higher power density (lower energy per cycle)
- What's not to like?
  - Lowest loss only at resonance
  - Turn-On losses can still be significant
  - Impedance imbalances cause trouble
  - Control difficult because of dynamic gain



# Multi-pole Bridge Snubber Minimizes Switching Losses

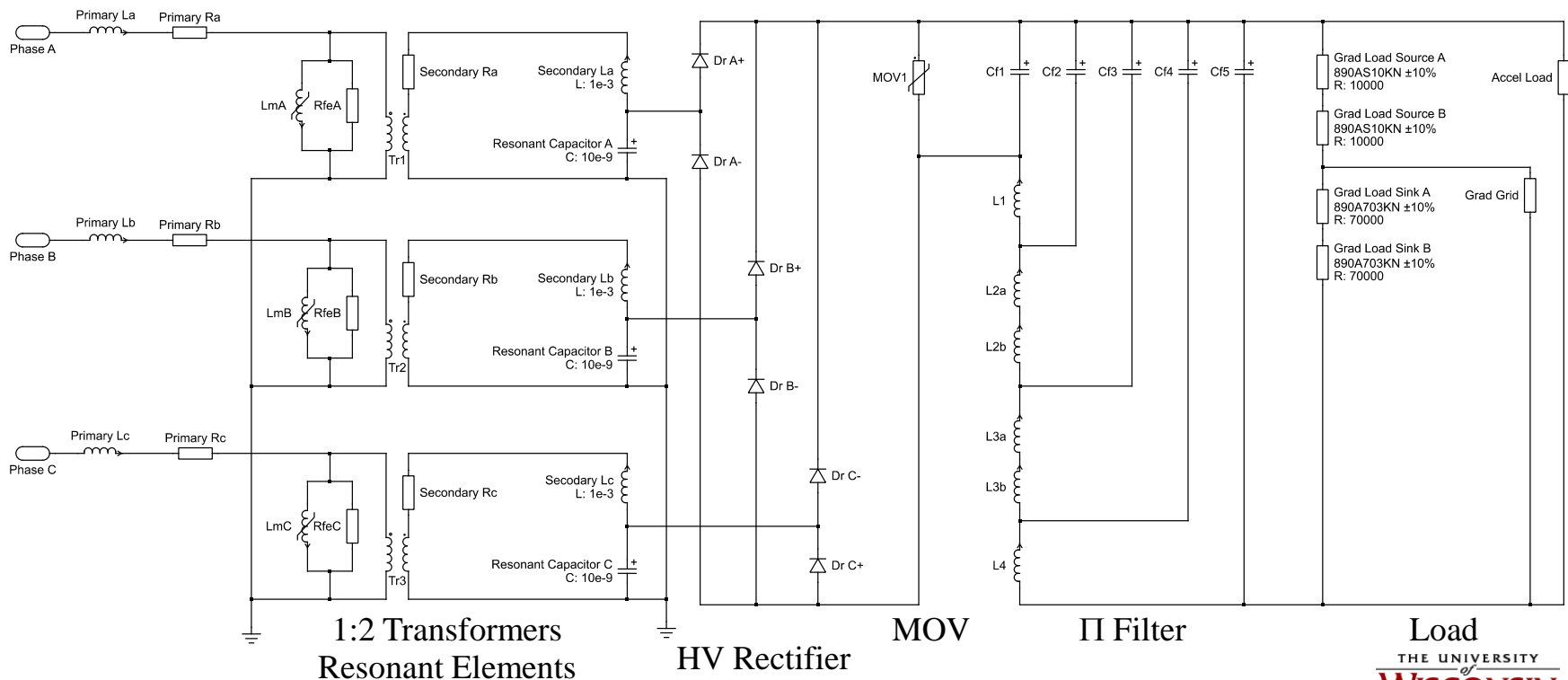
- Clamps device for  $\sim 400\text{nsec}$
- Allows turn-on of IGBT at zero voltage
- Loss reduction enables access to higher switching frequencies



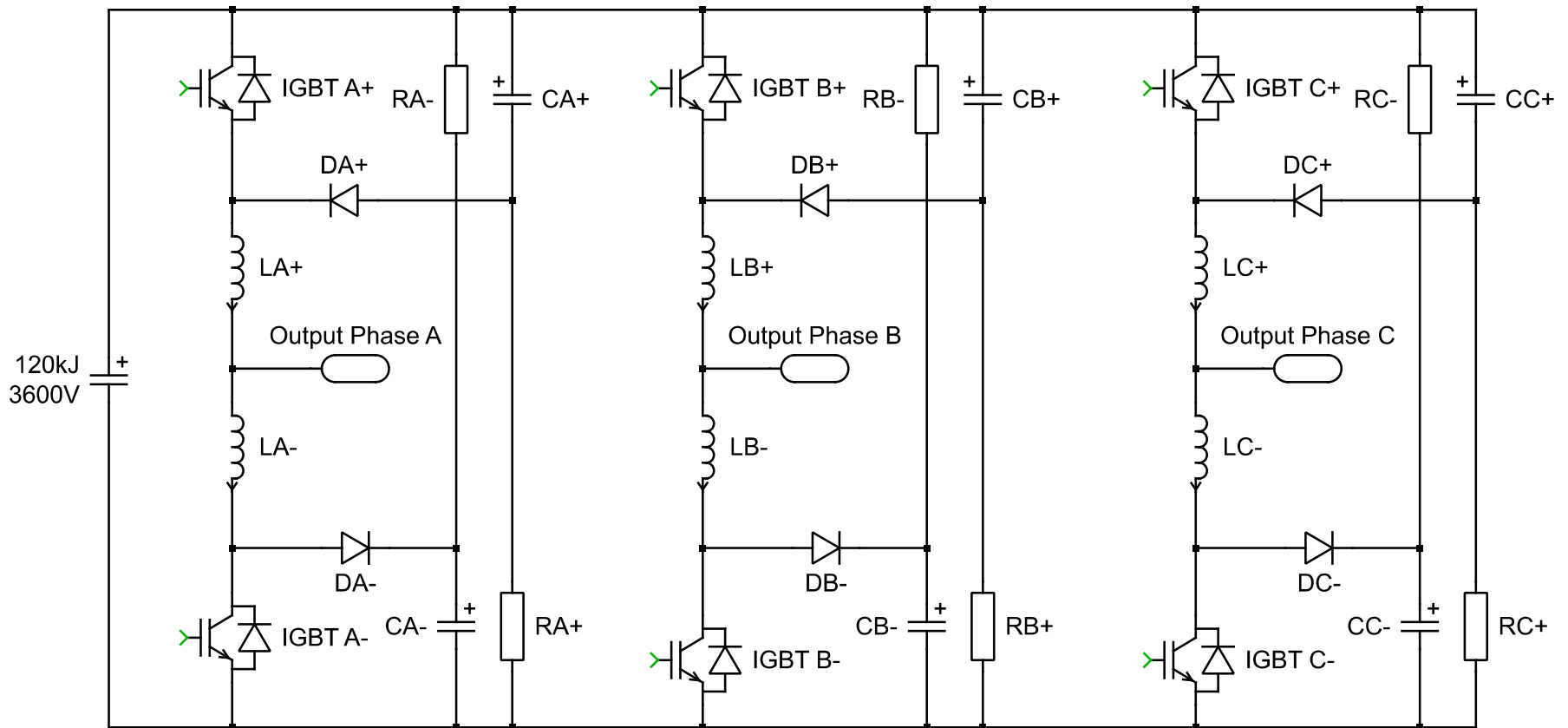
# > 20x gain achievable in HV Section

## • Resonant Converter High Voltage Section

- 80kV at 5A with 1J of 80kV filter energy
- Transformer leakage inductance ( $L_a/L_b/L_c$ ) utilized for resonant circuit
- Very fast ramp times  $< 200\mu s$  to 80kV and no crowbar
- Very low ripple  $\pm 0.2V$  or  $\pm 0.00025\%$



# 3600V Primary with Multi-Pole Snubber





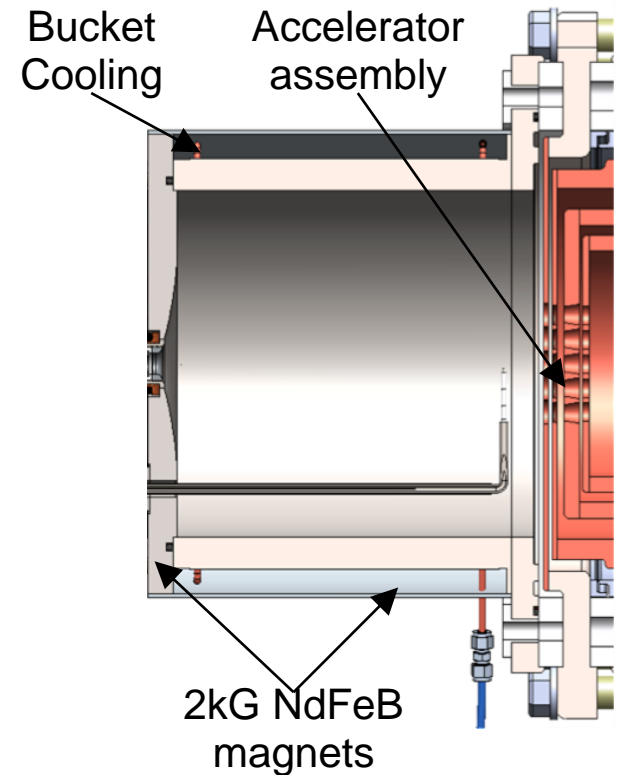
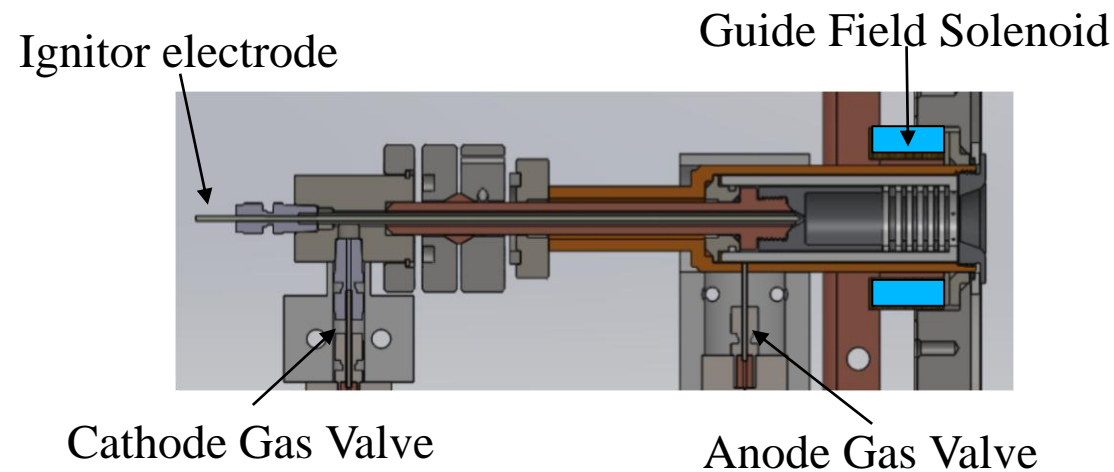


# Source Plasma Characterization

# New High Density Plasma Arc Source Provides Optimal Species Mix

- Hot filament source replaced with washer stack arc source
  - New arc parameters:
    - $T_e \sim 10 \text{ eV}$
    - $n_e \sim 10^{22} \text{ m}^{-3}$
- Arc plasma provides high ionization fraction
  - 80-90% at full energy achieved with other arc source beams<sup>1-3</sup>

- Plasma expands into a bucket with multipole cusp fields



<sup>1</sup> Deichuli et al, Rev. Sci. Instrum. **79**, 02C106 (2008)

<sup>2</sup> Abdrashitov, et al, Rev. Sci. Instrum. **72**, 594 (2001)

<sup>3</sup> Korepanov, et al, Rev. Sci. Instrum. **75**, 1829 (2004)

# Operational Space Mapped to Match Grid Perveance Requirements

- Beam Extraction Requirements

- Extracted Current: 1-3 A
- Grid Extraction area: 19 x 1.52 cm<sup>2</sup>

$$\rightarrow j_{\text{ext}} = 35 - 100 \text{ mA/cm}^2$$

- At the grids:

$$j_{\text{plasma}} = n_e e v_B \rightarrow j_{\text{ext}} = I_{\text{ext}} / A_{\text{ext}}$$

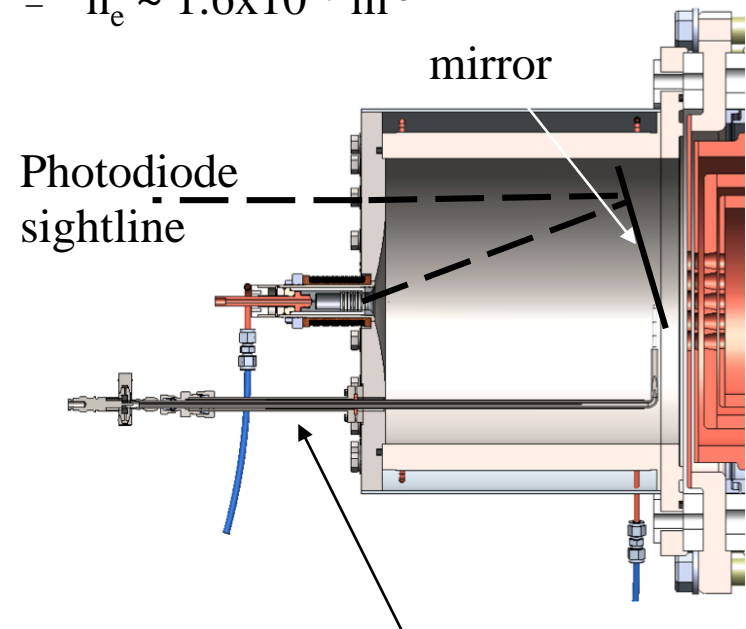
$$n_e = \frac{I_e^*}{eA} \sqrt{\frac{2\rho m_e^{(*)}}{T_e}} \quad v_B = \sqrt{T_e / m_i}$$

- Swept Langmuir probe deployed to characterize plasma parameters

\* N. Hershkowitz. "How Langmuir Probes Work."  
Plasma Diagnostics, 113-183. Academic Press, 1989.

- Source Requirements to meet  $j_{\text{ext}}$  at the grids:

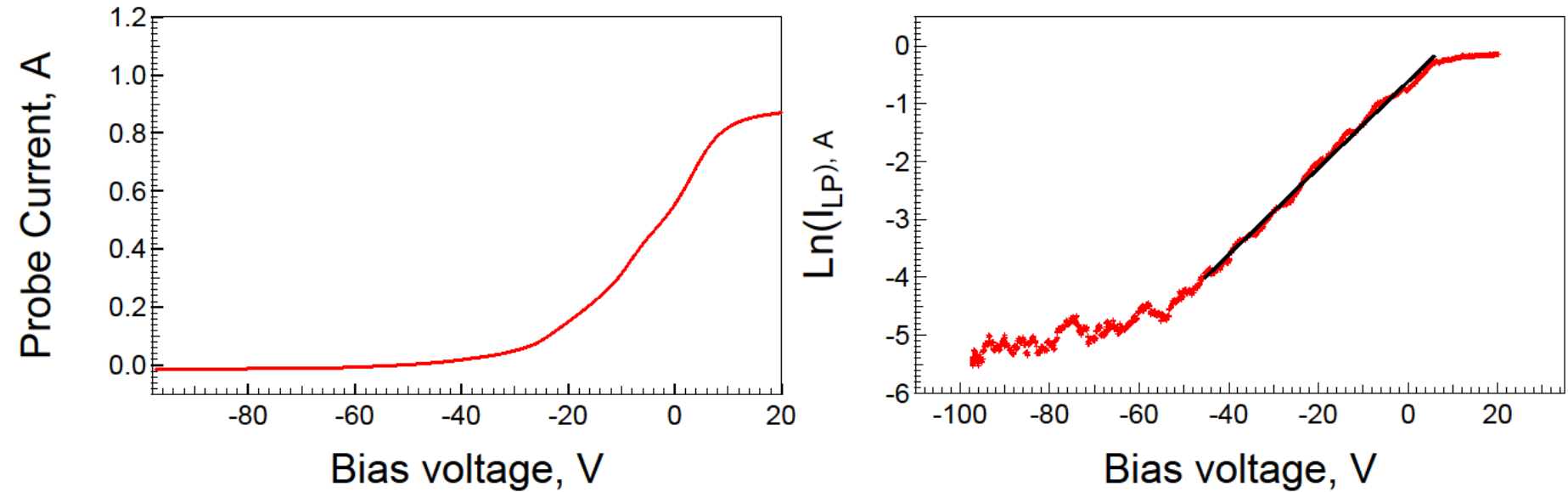
- $T_e \sim 15 \text{ eV}$
- $n_e \sim 1.6 \times 10^{17} \text{ m}^{-3}$



- Retractable and rotatable probe designed for complete characterization of source plasma



# Single Swept Langmuir Probe Traces Provide $T_e$ and $n_e$ Information

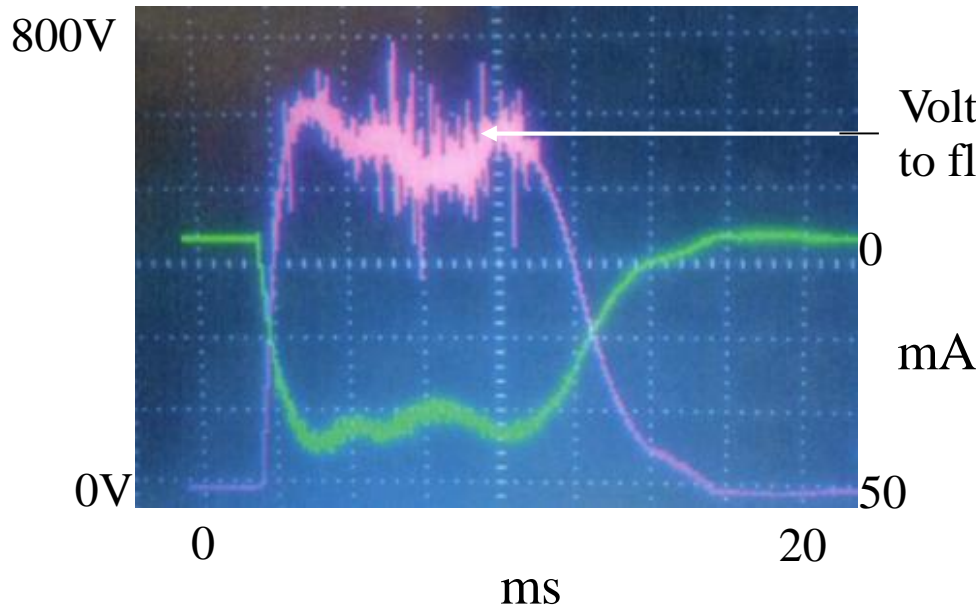


- $T_e \geq 14\text{eV}$  allows for greater ionization and high species fraction
- $n_e \approx 6 \times 10^{17} \text{ m}^{-3}$  densities (above those required) achieved easily
  - $j_{\text{ext}} \sim 350 \text{ mA/cm}^2$ , high but can be reduced with a grid if needed

# Desired Arc Operation Space Achieved

- Realized Arc Parameters
  - $T_e \sim 15 \text{ eV}$
  - $n_e \sim 2 \times 10^{17} \text{ m}^{-3}$
- Shot Parameters:
  - Potential drop across the arc: 700 V
    - $\sim 1.5 \text{ kA}$  arc current
  - Cathode plenum flow rate:  $300 \text{ Torr-L s}^{-1}$
  - $B_{GF}$ : 0.6 kGauss

**$V_{\text{arc}}$  (pink) and Langmuir Probe  $I_{\text{sat}}$  (green) in 10ms arc discharge**



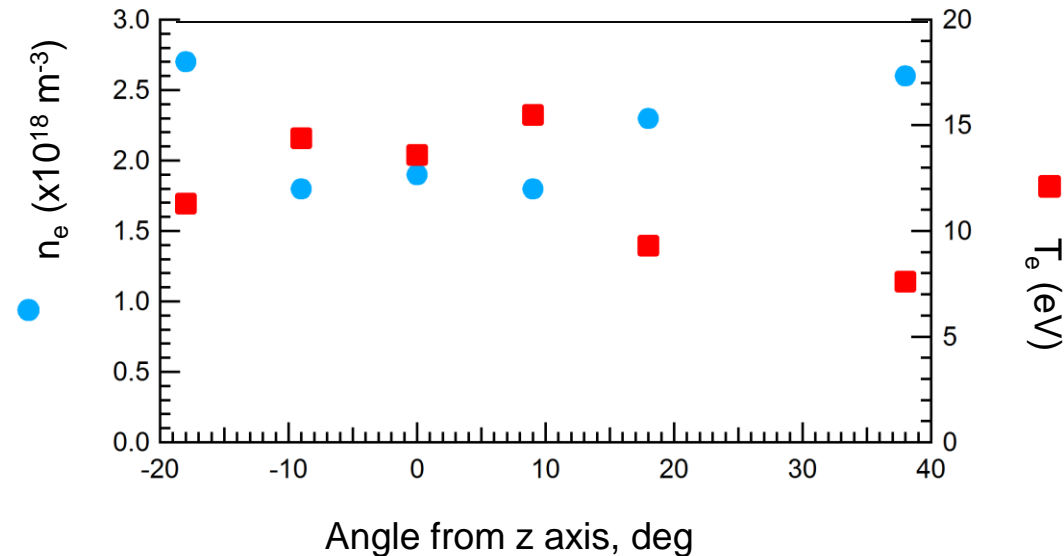
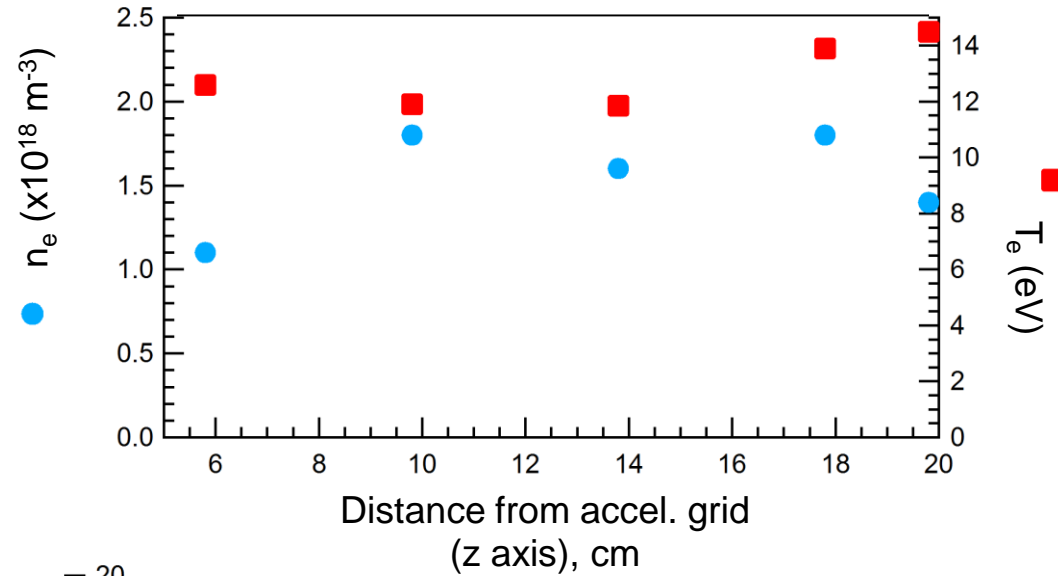
Voltage fluctuations on the arc do not correspond to fluctuations in ion saturation current

# Measured $T_e/n_e$ Profiles At Extraction Grid Spatially Uniform as Required

- Temperature spikes near the source, but remains stable in the bucket
- Density decreases near the grid

↘

→



- Temperature decreases at the edge
- Density increases at the edge

←



# Arc Performance



# 100kV Testing of Arc Diagnostics Successful

- High voltage conditioning is still required for beam accelerator grids
- Integration of new 80kV power supply after grid conditioning





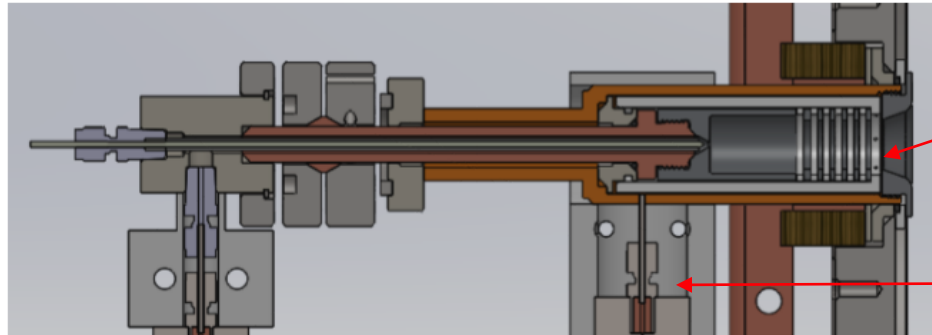


# Additional Optimization of Arc Discharge May Be Needed for Diagnostic Performance

- Arc stability may affect beam divergence
  - $\widetilde{n}_e$  at the extraction plane may translate to beam divergence
  - Effect will be characterized when power supply is online
- Recent work has improved arc discharge stability
- Two major contributors:
  - Additional hydrogen fueling at anode
  - Magnetic guide field strength

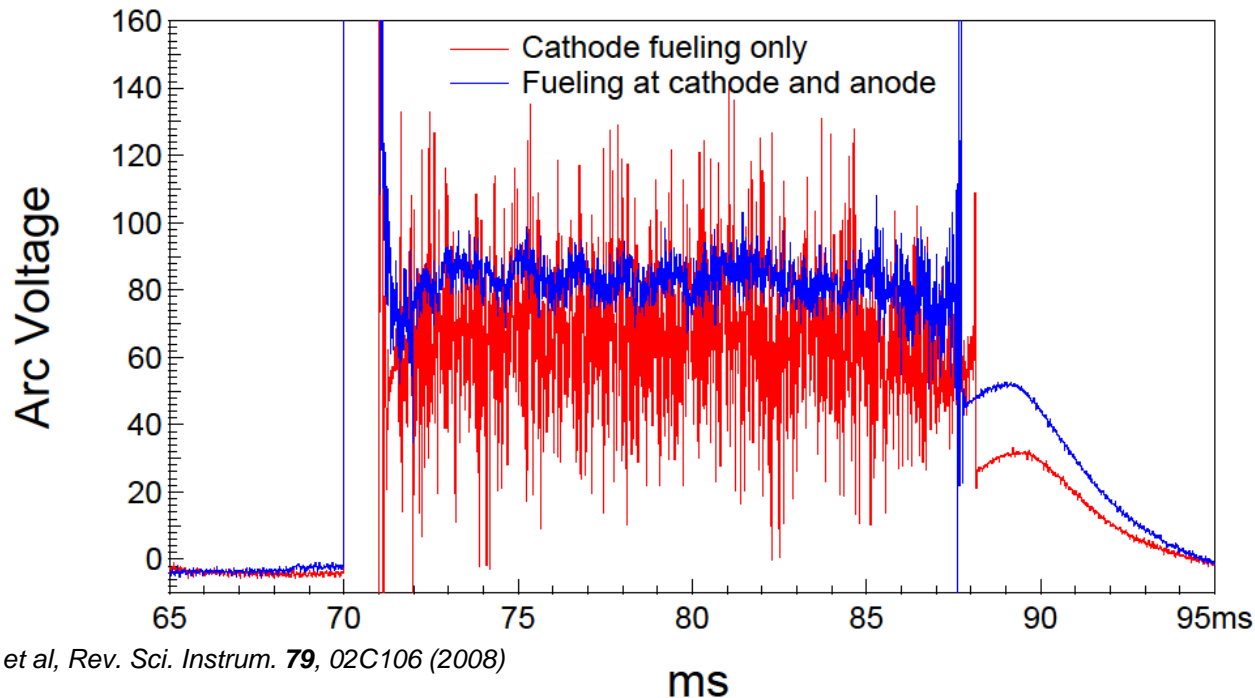
# Arc Stability Increased by Hydrogen Fueling at Anode

- Hydrogen gas at anode reduces voltage fluctuations in the arc



Gas introduced radially via small holes in the last ceramic washer

Anode gas valve

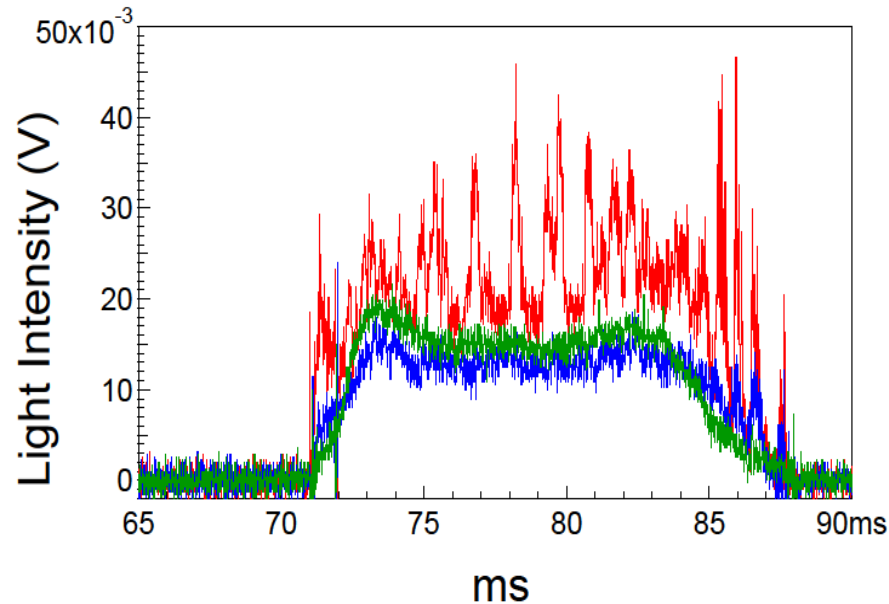


<sup>1</sup> Deichuli et al, Rev. Sci. Instrum. **79**, 02C106 (2008)

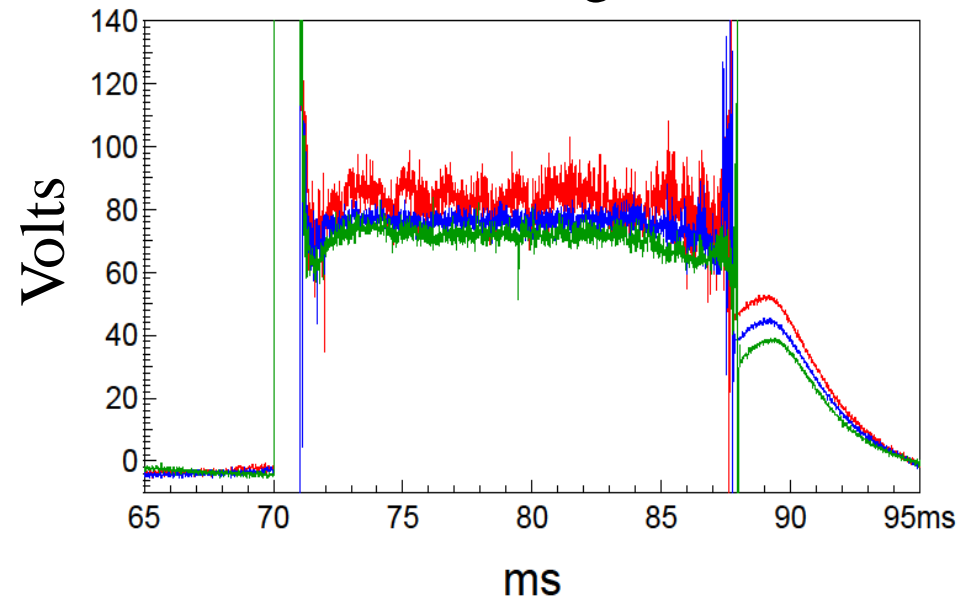
# Arc Stability Modified by Strong Guide Field

- Increasing guide field induces voltage fluctuations in the arc

## Photodiode Detector

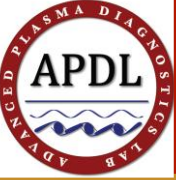


## Arc Voltage



## Guide Field Strength

- 1.2kGauss
- 0.6kGauss
- 0.24kGauss



# Measurements of Electric Field Fluctuation Possible with Novel Diagnostic

- $\tilde{E}$  measurements at 500 kHz possible via new Spatial Heterodyne Spectrometer and high speed 2D detector, providing a powerful, high resolution, high throughput, compact spectrometer concept
- A low-divergence, high energy diagnostic neutral beam (from PPPL) with new ion source being deployed to develop measurement
- A novel three-phase resonant converter power supply has been designed and built for low ripple, constant voltage output
- After conditioning, ion species mix measurements will determine necessity of quiet arc discharges.

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