

A New Technique for Measuring Local Electric Field Fluctuations in High Temperature Plasmas

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Understanding Turbulence in Tokamaks is a Fundamental Challenge for Fusion Energy

- Plasma turbulence in tokamaks results in anomalous transport
 - Cross-field transport $\gg$ neoclassical predictions
- Present plasma diagnostics measure key fluctuating parameters $\tilde{n}$, $\tilde{T}_i$, $\tilde{T}_e$, $\tilde{v}$
- Measurement of electrostatic field or potential turbulence, $\tilde{\phi}$ or $\tilde{E}$, remains a challenge
 - $\tilde{E}_\theta \times B_\phi \cong \tilde{v}_r$: turbulent cross-field transport
 - $\tilde{E}_r \times B_\phi \cong \tilde{v}_\theta$: shear-flow and zonal flow dynamics
- Other topics of interest:
 - Nonlinear turbulence dynamics, energy cascades, mode energy transfer, Reynolds Stress: $d\langle \tilde{v}_r \tilde{v}_\theta \rangle / dr$, turbulent particle flux,...
 - Validation of turbulence codes: GYRO, GENE,...

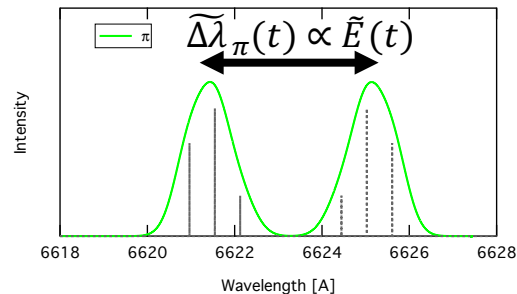
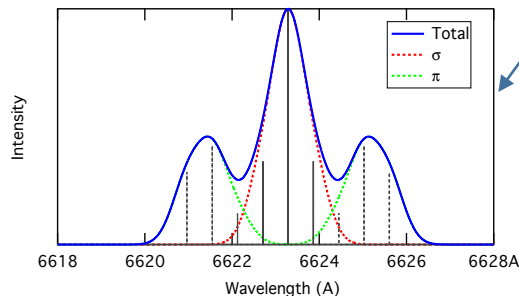
Motional Stark Effect Field Used as Carrier Signal for $\tilde{E}$

- Motional Stark Effect spectrum provides carrier line broadening for $\tilde{E}$:

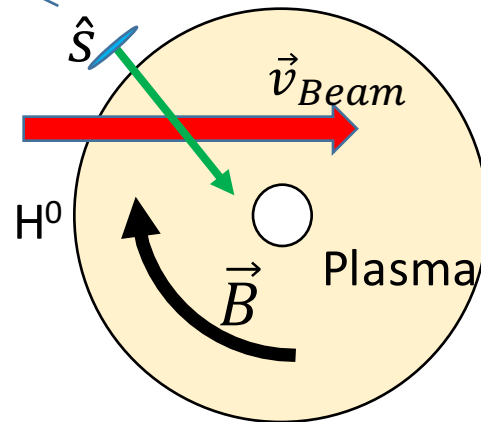
$$\vec{E}_{total} = \vec{v}_b \times \vec{B} + \vec{E}_{plasma}$$

- Measure high-speed variations in π/σ line intensity ratio or in π -components linewidth to derive $\tilde{E}$
- Spatial Heterodyne Spectrometer (SHS) provides flexible analyzer of multiplet spectrum
- New CMOS imaging systems provide detection and DAQ

Model H α Stark Spectrum: 80 keV, 0.5 T



Diagnostic layout:



Tokamak Top Down View

Analysis of Stark Multiplet Allows Measurement of $\vec{E}_{plasma}(t)$

- Midplane beam, sightline: linewidth changes

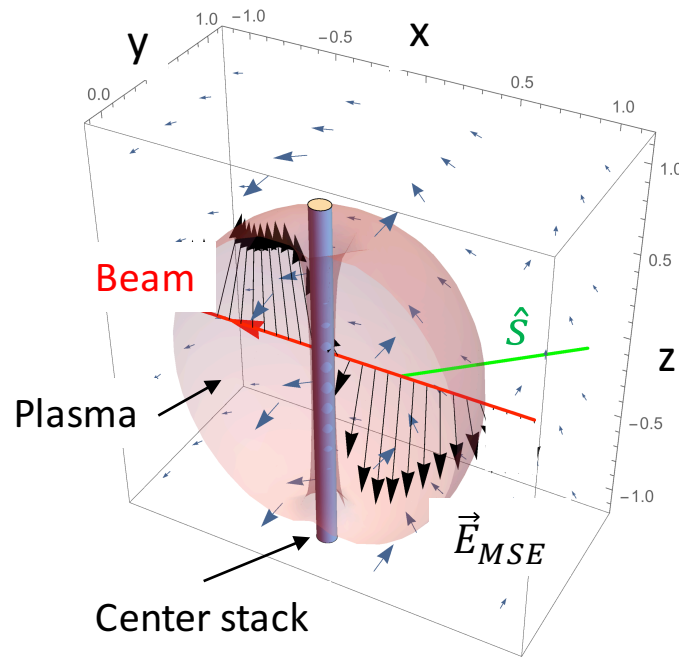
$$\widetilde{\Delta\lambda}_{stark} \propto \tilde{E}_z$$

- Midplane beam, off-midplane sightline:
Intensity ratio change

$$R = \frac{\sum I_\pi}{\sum I_\sigma} \propto \tilde{E}_R F(\tilde{n})$$

- First emphasis on line width measurement:
insensitive to density fluctuations

Example: ST Geometry



$\tilde{E}$ Estimated for Tokamaks Using Drift Wave Scaling

- Drift wave turbulence:

$$\frac{\tilde{n}}{n} \approx \frac{e\tilde{\phi}}{T_e}$$

- Long wavelength turbulence peaks at $k_{\perp}\rho_s \sim \alpha$, $\alpha=0.1-1$
 - From BES and other measurements
- $\tilde{E} \sim k_{\perp}\tilde{\phi}$ and $\tilde{n}/n \sim 1/k_{\perp}L_n$ where $L_n \sim a$ (worst case)

$$\tilde{E} \approx \frac{\tilde{n}}{n} \frac{T_e}{e\rho_s} \approx \frac{T_e}{ea}$$

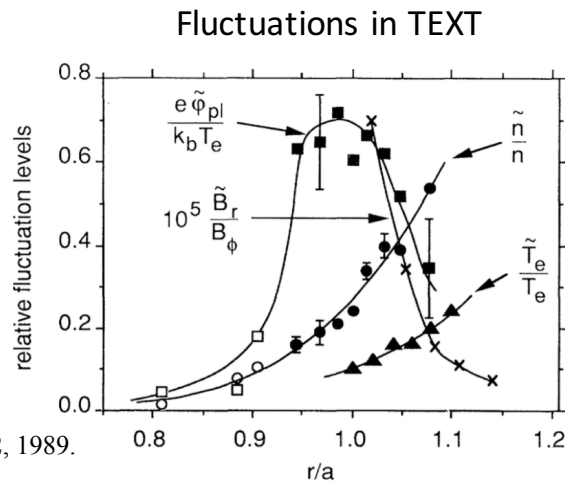


$\tilde{E}/\vec{E}_{MSE}$ in Fusion Grade Plasmas is $\sim 10^{-3}$

- Tokamak drift wave turbulence scaling gives $\tilde{E} \approx T_e/ea$

Experiment	$T_{e,0}$ (keV)	B (T)	a (m)	$\tilde{E}/E_{MSE}$
NSTX-U	$\sim 2-4$ (?)	1	0.6	$1 - 2 \times 10^{-3}$
DIII-D	2-5	2	0.7	$0.5 - 1 \times 10^{-3}$

- $\tilde{E}$, $\tilde{n}$ rise from core to edge
- Comparable to typical photon noise floor for BES



C. P. Ritz, et. al., Phys. Rev. Lett., **62**, 1989.

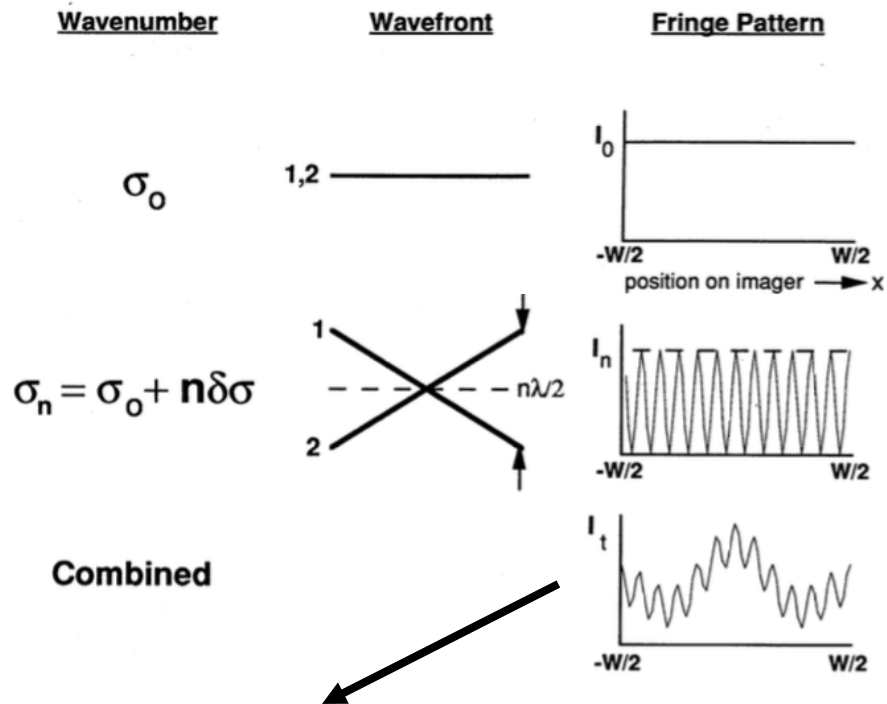
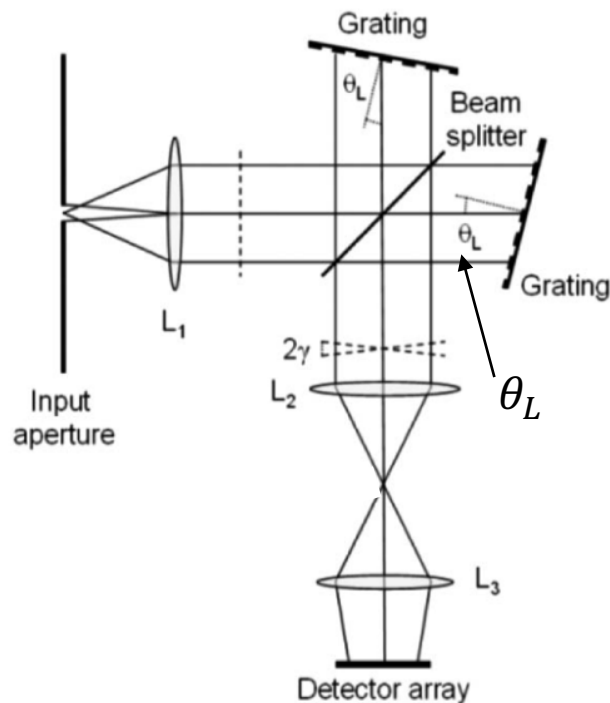


$\Delta\tilde{\lambda}_\pi$ Spectrometer Requirements are Formidable

- Resolution:
 - Need ~ 8 spectral bins to resolve 2 gaussian-like π components
 - $\Delta\lambda_{H\alpha}^\pi \sim 4 \text{ \AA}$ giving a spectral resolution of $0.5 \text{ \AA}$, $R = \frac{\lambda}{\delta\lambda} \sim 1.3 \times 10^4$
- Throughput:
 - Matched to collection optics, port availability, $U = 0.05 - 0.1 \text{ cm}^2\text{-str}$
 - 2 spatial points desired
- Compatible detector system:
 - $\sim 250 \text{ kHz}$ time response
- Mitigation of sightline-DNB geometric broadening

Spatial Heterodyne Spectroscopy Meets $\tilde{E}$ Spectrometer Requirements

- Self scanned, 2 beam interferometer
- Input wavelengths heterodyned around Littrow wavelength

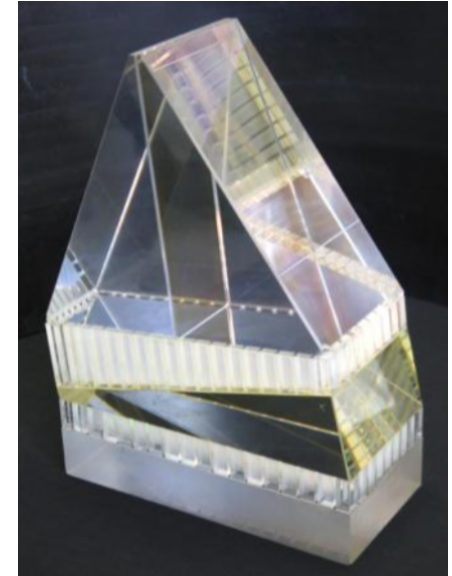


$$I(x) = \int_0^{\sigma} B(\sigma) (1 + \cos[2\pi(4|\sigma - \sigma_0|x \tan \theta_L)]) d\sigma$$

Spatial Heterodyne Spectroscopy Achieves High Resolution and Throughput

- SHS theoretical resolving power:
 - $R = \sigma / \delta\sigma \approx 2W/d$
 - For $\tilde{E}$: Need $R \sim 1 \times 10^4$
 - For $W = 50$ mm only requires $d = 1/100$ lines/mm
 - Resolution readily achievable with simple coarse gratings, compact size
- SHS throughput comparable to field widened Fourier Transform spectrometer
 - For $\tilde{E}$: need throughput of $0.05\text{--}0.1 \text{ cm}^2\text{str}$
 - $U = 2\pi\eta A/R = 0.0015\eta \text{ cm}^2\text{str}$; $\eta \sim 1$ (no field widening)
– 100 (field widening)
 - Required throughput readily achievable in SHS

DASH Interferometer

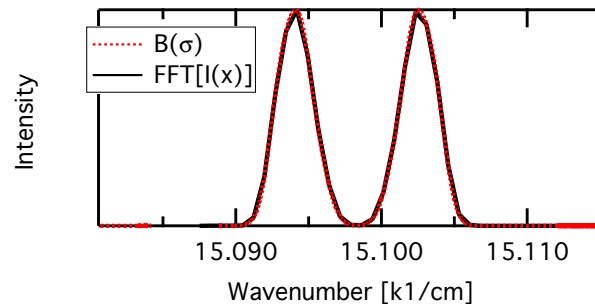
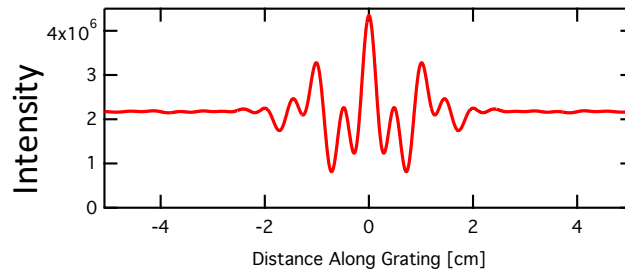
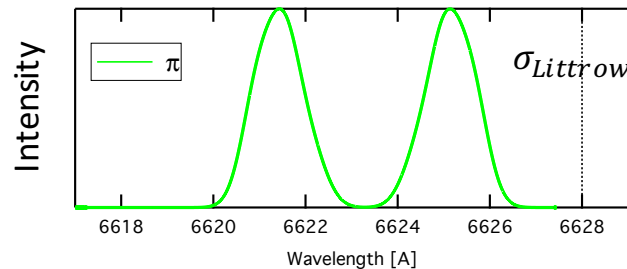


$R \approx 5 \times 10^4$, $U \approx 0.15 \text{ cm}^2\text{str}$

Modeling of Interferogram Used to Explore Spectrometer Design

- Synthetic interferograms generated via modeled π components
- Fourier transform of interferogram $I(x)$ gives $B(\sigma)$
- High speed recording and inversion of $I(x)$ is similar to gaussian fit analysis of $\tilde{T}_i$ and $\tilde{\nu}$ measurements

$$I(x) = \int_0^{\sigma} B(\sigma) (1 + \cos[2\pi(4|\sigma - \sigma_0|x \tan \theta_L)]) d\sigma$$



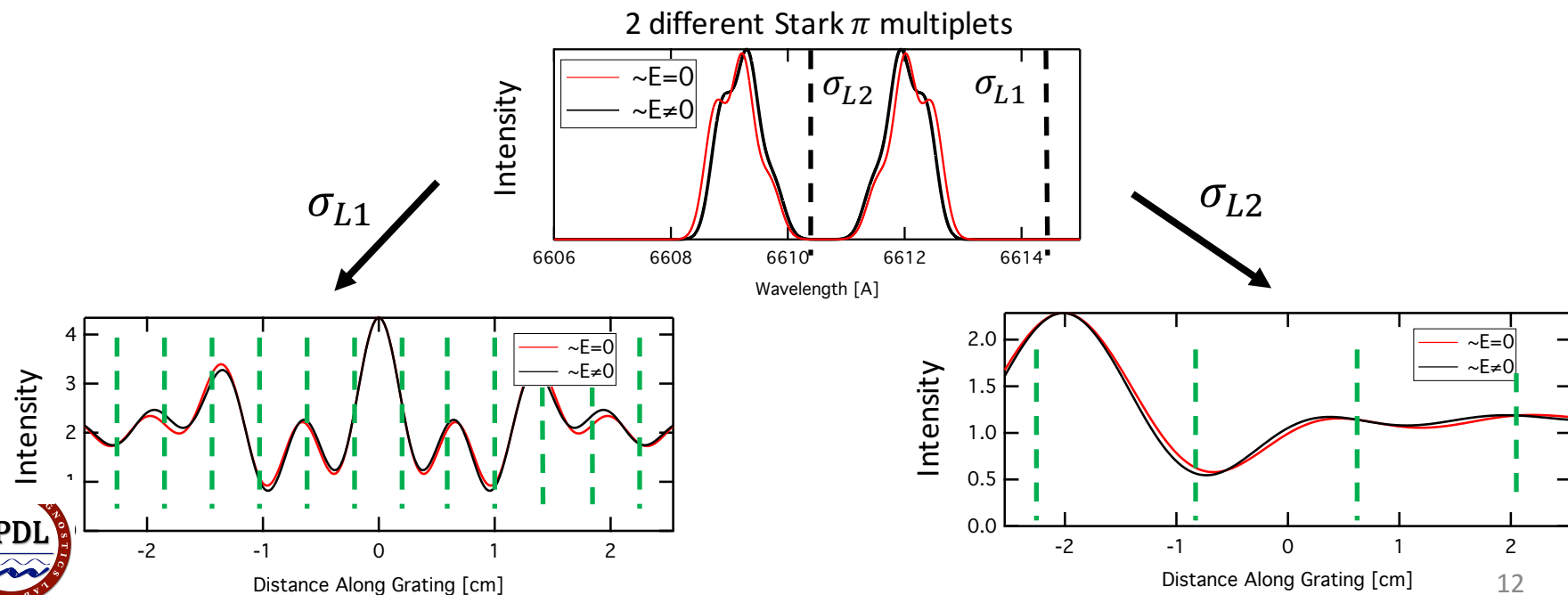
New CMOS Imaging Technology Provides Turbulence Timescale Measurement

- Flexible, high speed recording of full interferogram at photon noise limit
- Example: Phantom v2512 FAST by Vision Research
 - 500 kHz @ 256 x 80 pixels or 110 x 110 pixels
 - QE ~ 50% over visible range
 - Integrated DAQ
- Potential for 2 spatial measurements



Extracting $\widetilde{\Delta\lambda}$ From Central Fringe Analysis Could Reduce the Number of Detectors

- Full interferogram recording may not be necessary
- Can optimize spectrometer to give fringe pattern of interest without losing light
- $\widetilde{\Delta\lambda}(t)$ then recorded using 3-4 detectors

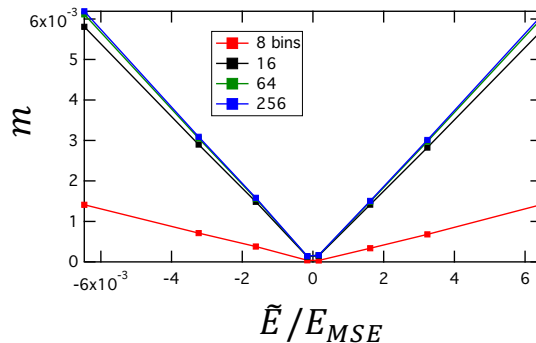
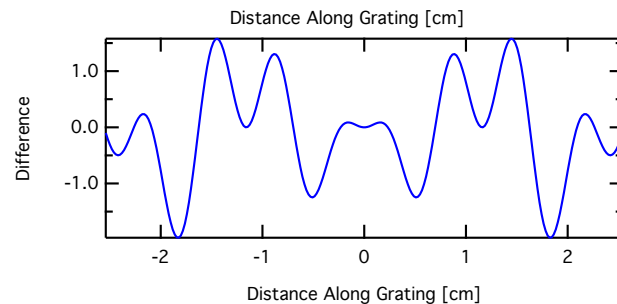
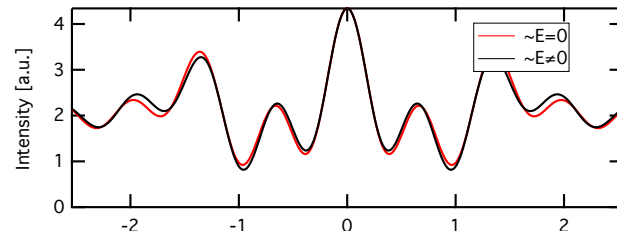


Metric from Simplified Interferogram Scales Linearly with $\tilde{E}$, Requires Less Detector Channels

- Want a metric (m) that is proportional to $\tilde{E}$
- Approach: finite number of bins around central fringe region measured to get $\tilde{E}$
- Example metric (m) based on differences in interferogram area from time average area:

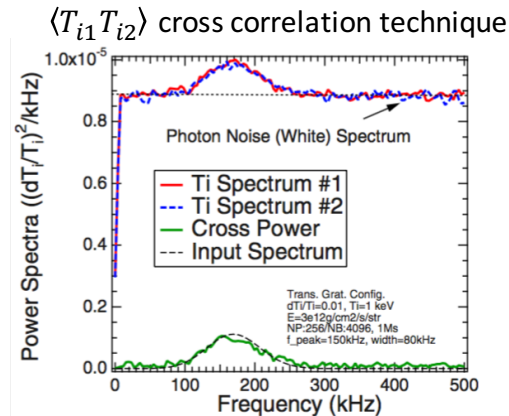
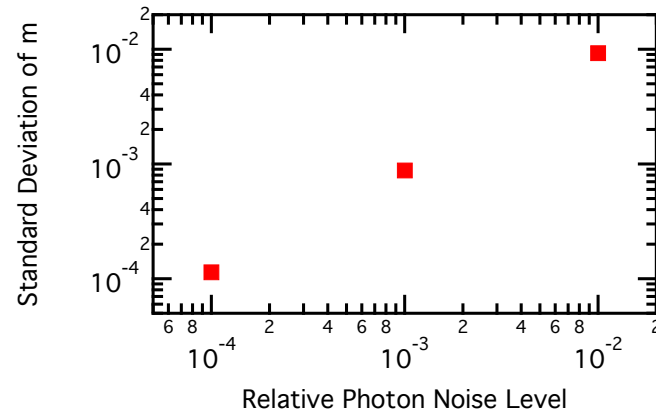
$$m = \sqrt{\frac{\sum_j^{N_{bins}} (I_{j, \tilde{E} \neq 0} - I_{j, \tilde{E} = 0})^2}{\sum_j^{N_{bins}} (I_{j, \tilde{E} = 0})^2}}$$

- $m = \tilde{E}/E_{MSE}$
- For given case 16 bins are adequate
- Design optimization ongoing, ideally reduce to 3-4 detectors for single spatial point

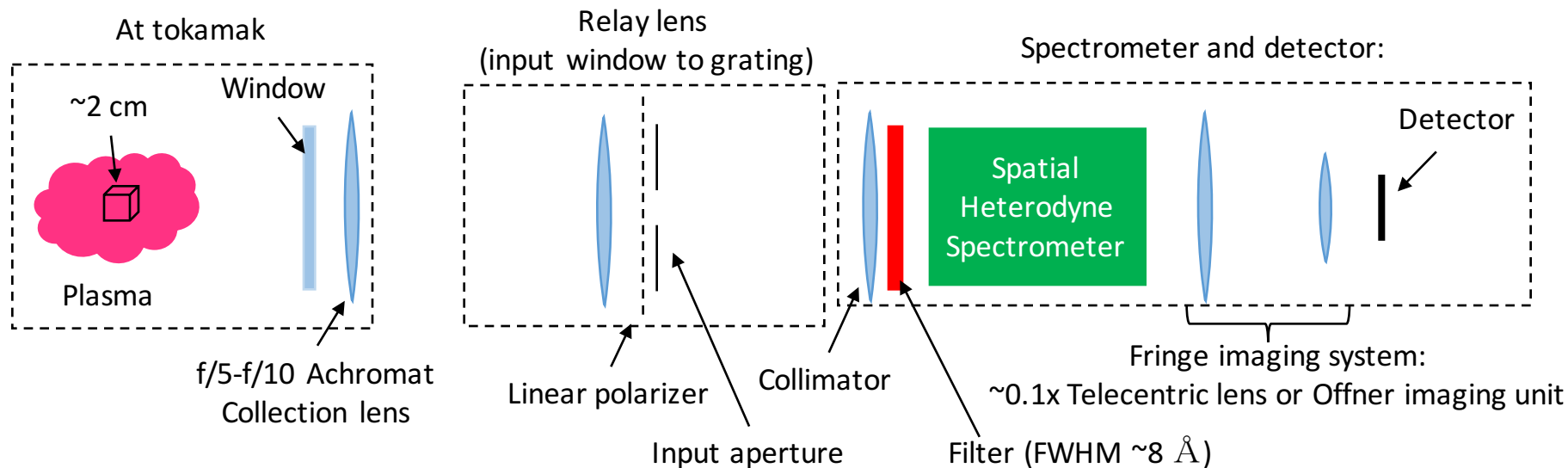


Noise Floor for Multi-bin Metric Equal to Relative Photon Noise Level

- Simulated variation in metric due to photon noise shows relative noise in metric = photon noise level
- Measured photon flux is standard BES signal
 - BES photon noise level $\sim 10^{-3}$
- Random photon noise can be suppressed by standard cross correlation techniques
 - Two independent but spatially correlated measurements made simultaneously
 - Example: $\langle \tilde{E}_1 \tilde{E}_2 \rangle$ and $\langle \tilde{E} \tilde{n} \rangle$
- Depending on data record length, can reduce residual noise floor by 10-100x

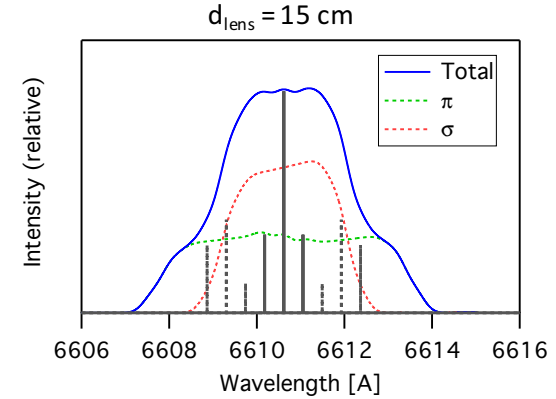
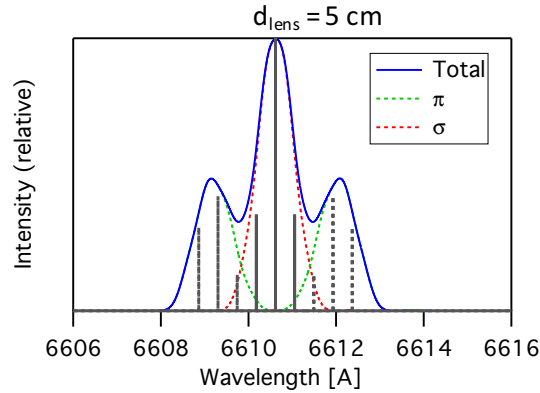
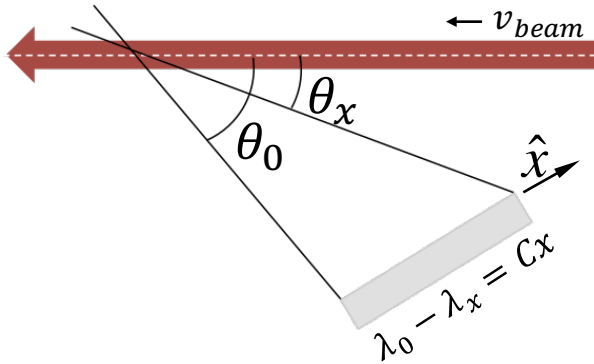


Optics Require Conjugate Imaging, High Throughput



- Fringe image detection requires large depth of field, high throughput, no aberrations
 - Set by maximum path difference between wavefronts and/or coherence length of wavefronts
- Realized with telecentric lens or Offner imaging system

Geometric Broadening Compensated in SHS, Allows Large Collection Optic



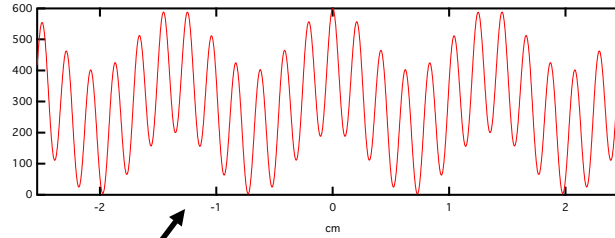
- SHS Fizeau fringe pattern is optically conjugate to input optic
- λ (phase) shift due to window geometry $\sim$ linear across grating

$$\phi_w = 2\pi cx \rightarrow \phi_{Total} = \phi_G + \phi_w = 8\pi(\sigma - \sigma_L)\tan\theta x + \phi_w(x)$$

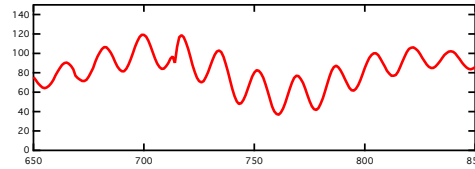
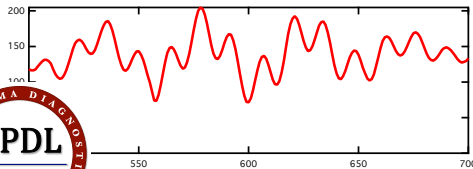
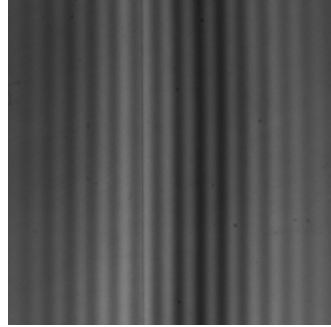
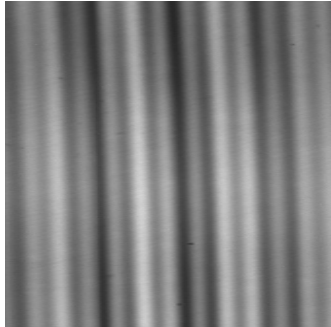
- Convolve $I(x)$ with $\mathcal{F}[\exp(-i\phi_w)]$ in the spectral domain to remove geometric broadening
- Chirped gratings, $d(x)$, could actively remove geometric broadening inside spectrometer

Flexible Modular SHS System Developed for First Tests

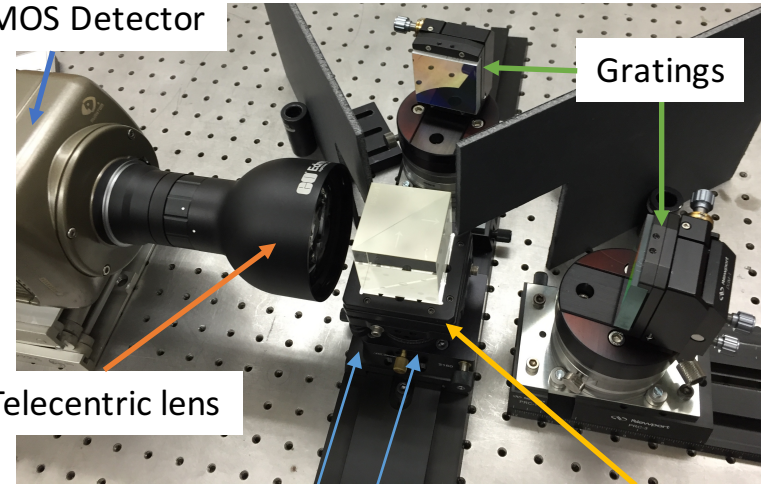
Sodium Doublet: $\Delta\lambda \sim 6 \text{ \AA}$
Interferogram model:



Change θ_L



Fast CMOS Detector



Telecentric lens

Gratings

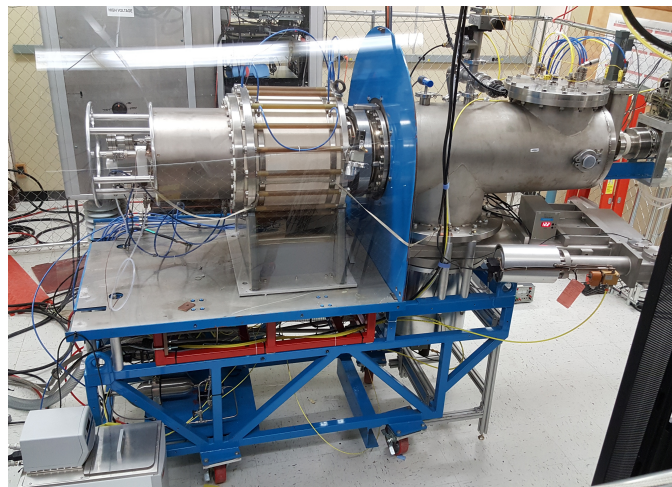
Beam Splitter

Collimated input

$\tilde{E}$ Diagnostic Requires Low Divergence, High Full Energy Fraction DNB

- H^0 DNB on loan from PPPL
 - Full-energy J at focus: $3\text{-}6\text{ mA/cm}^2$ *
 - Diameter $\sim 9\text{ cm}$
- Features favorable for measurement
 - Low divergence: $\leq 0.47^\circ$
 - Mitigates Divergence line broadening
 - High $E_b \sim 60 - 80\text{ keV}$
 - Maximizes MSE broadening
 - 90-95% ionization at full beam energy
 - Ensures maximum signal for diagnostic

Low divergence , high energy DNB

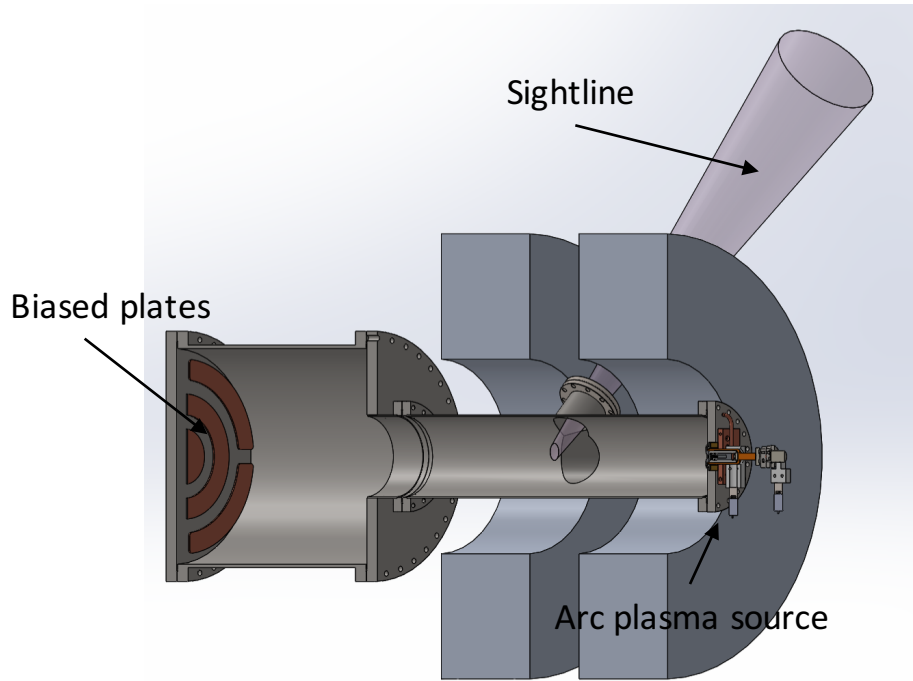


See M. Bakkens Poster #1

Summary: Moving Towards Diagnostic For $\tilde{E}$ in High Temperature Magnetically Confined Plasmas

- $\tilde{E}$ measurements appear feasible using high speed measurements of motional stark multiplet
 - Horizontal view gives $\tilde{E}_Z$, Off midplane gives $\tilde{E}_R$
- SHS provides flexible, compact, spectrometer concept
 - Full spectrum measurement available
 - Subsampling interferogram may support multiple spatial channels with simple discrete detectors like BES
- Next steps:
 - Commission low divergence, 80 keV DNB
 - Deploy plasma target station to emulate edge tokamak plasma conditions, $n_e > 1 \times 10^{19} \text{ m}^{-3}$
 - Validate diagnostic using imposed electric field fluctuations on target plasma

Validation Test Stand



$\tilde{E}$ Test Stand:

