

# A New Technique for Measuring Local Electric Field Fluctuations in High Temperature Plasmas

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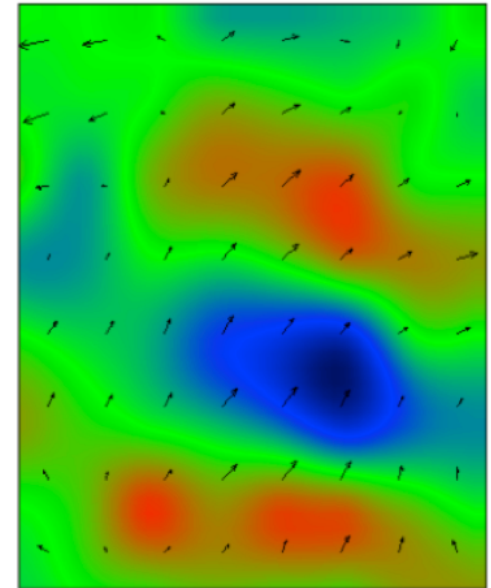


# Introduction

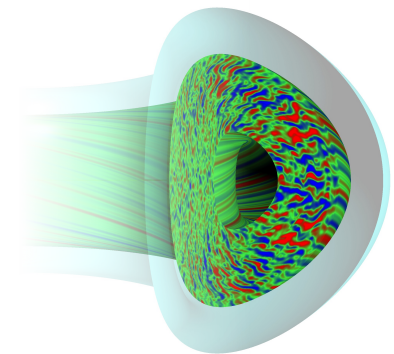


# Understanding Turbulence in Tokamaks is a Fundamental Challenge for Fusion Energy

- Plasma turbulence in tokamaks results in anomalous transport
  - Cross-field transport  $\gg$  neoclassical predictions
- Present plasma diagnostics measure key fluctuating parameters  $\tilde{n}$ ,  $\tilde{T}_i$ ,  $\tilde{T}_e$ ,  $\tilde{v}$
- Measurement of electrostatic field turbulence ( $\tilde{E} \sim k_{\perp} \tilde{\phi}$ ) remains a challenge, gives  $\tilde{v}$ 
  - $\tilde{E}_{\theta} \times B_{\phi} \cong \tilde{v}_r$ : turbulent cross-field transport
  - $\tilde{E}_r \times B_{\phi} \cong \tilde{v}_{\theta}$ : shear-flow and zonal flow dynamics
- Other topics of interest:
  - Nonlinear turbulence dynamics, energy cascades, mode energy transfer, Reynolds Stress:  $d\langle \tilde{v}_r \tilde{v}_{\theta} \rangle / dr$ , turbulent particle flux,...
  - Validation of turbulence codes: GYRO, GENE,...



Density perturbations and calculated velocimetry in DIII-D plasma



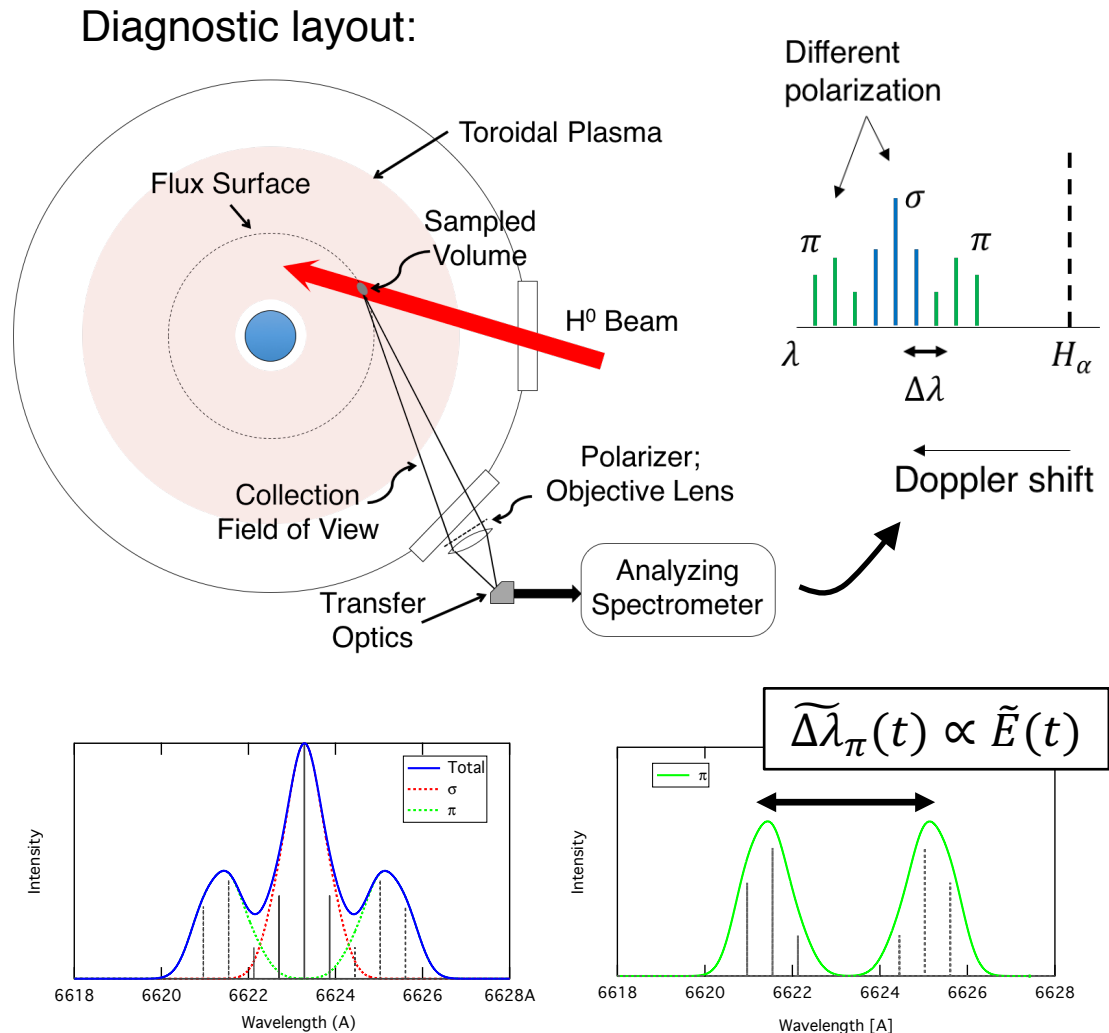
GYRO turbulence simulation

# Motional Stark Effect Field Used as Carrier Signal for $\tilde{E}$

- Motional Stark Effect spectrum provides carrier line broadening for  $\tilde{E}$ :

$$\vec{E}_{total} = \vec{v}_b \times \vec{B} + \vec{E}_{plasma}$$

- Measure high-speed variations in  $\pi$ /s line intensity ratio or in  $\pi$ -components linewidth to derive  $\tilde{E}$
- Spatial Heterodyne Spectrometer (SHS) provides flexible analyzer of multiplet spectrum
- New CMOS imaging systems provide detection and DAQ

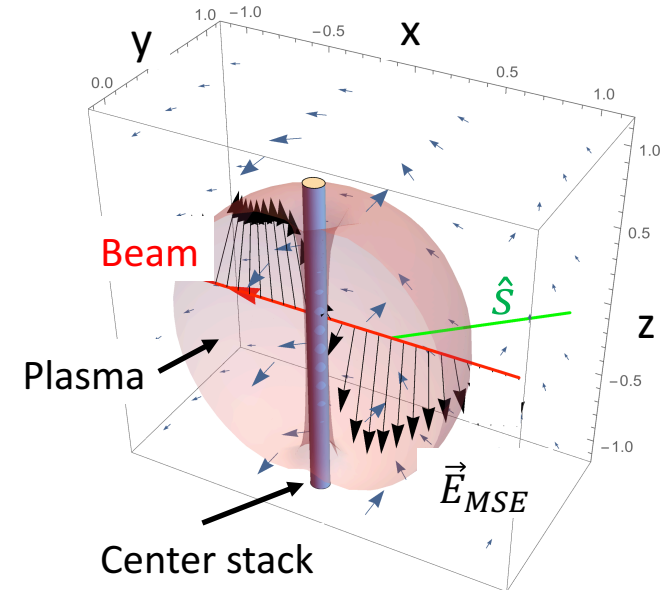
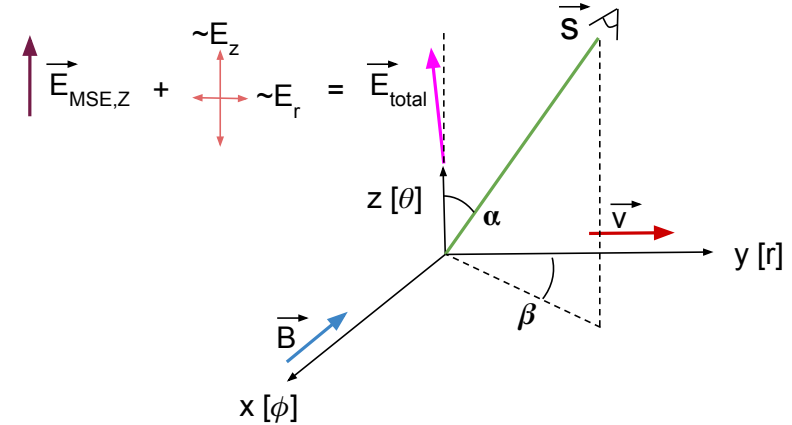


Model  $H^\alpha$  Stark Spectrum: 80 keV, 0.5 T



# Multiple Techniques Used to Extract Components of $\vec{E}_{plasma}(t)$

- Midplane beam, sightline: linewidth changes
  - Radial beam:  $\vec{E}_{MSE}\hat{z}$ ,  $\tilde{E}_z$  doesn't change  $\alpha$
  - $\tilde{\Delta\lambda}_{Stark} \propto \tilde{E}_z \rightarrow \tilde{v}_r$
- Midplane beam, off-midplane sightline: Intensity ratio change
  - $R = \frac{\sum I_\pi}{\sum I_\sigma} = \frac{\sin^2 \alpha}{1 + \cos^2 \alpha} (I_\pi / I_\sigma) (n_e) \equiv \frac{\sin^2 \alpha}{1 + \cos^2 \alpha} F$
  - $\tilde{R} = R \left[ \frac{\partial \ln F}{\partial \ln n_e} \frac{\tilde{n}_e}{n_e} + \frac{4 \cos \alpha}{(1 + \cos^2 \alpha) \sin \alpha} \tilde{\alpha} \right]$
  - $\tilde{E}_r \sim \tilde{\alpha} E_{MSE} \rightarrow \tilde{v}_z$
- First emphasis on line width measurement: insensitive to density fluctuations, midplane view



Example: ST Geometry

# Local Magnetic Field Fluctuations May be Measurable via Stark Multiplet

- Measurement of local magnetic field fluctuations ( $\tilde{B}$ ) in high temperature plasmas is challenging
  - Provides information on: fast particle modes, island structures, plasma response to 3D RMP for ELM control, high- $\beta$  turbulence
- Again use MSE field as carrier
- For midplane sightline and radial beam:
  - $\vec{v}_r \times \tilde{B}_\phi = \tilde{E}_z$ ,  $\vec{E}_{MSE}$  is mostly in the  $\hat{z}$  direction  $\rightarrow \Delta\lambda_{Stark} \propto \tilde{B}_\phi$
  - $\vec{v}_r \times \tilde{B}_z = \tilde{E}_r$ , changes angle of  $\vec{E}_{MSE} \rightarrow$  measure polarization intensity
- Typically for tokamaks  $\tilde{B}/B \sim 10^{-5}$ , 100x smaller than broadband  $\tilde{E}/E$
- However, for 3D RMP in plasma edge,  $\tilde{B}/B$  has narrow frequency bandwidth
- $\tilde{B}/B$  and  $\tilde{E}/E$  distinguishable using different beam energy components

# Estimate of $\tilde{E}/E$ in Tokamaks



# $\tilde{E}$ Estimated for Tokamaks Using Drift Wave Scaling

- Drift wave turbulence:

$$\frac{\tilde{n}}{n} \approx \frac{e\tilde{\phi}}{T_e}$$

- Long wavelength turbulence peaks at  $k_{\perp}\rho_s \sim \alpha$ ,  $\alpha=0.1-1$

- From BES and other measurements

- $\tilde{E} \sim k_{\perp}\tilde{\phi}$  and  $\tilde{n}/n \sim 1/k_{\perp}L_n$  where  $L_n \sim a$  (worst case)

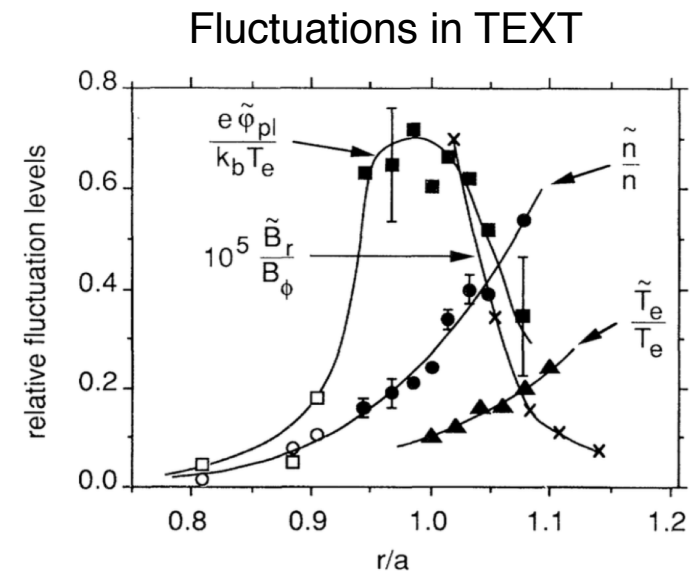
$$\tilde{E} \approx \frac{\tilde{n}}{n} \frac{T_e}{e\rho_s} \approx \frac{T_e}{ea}$$

# $\tilde{E}/\vec{E}_{MSE}$ in Fusion Grade Plasmas is $\sim 10^{-3}$

- Tokamak drift wave turbulence scaling gives  $\tilde{E} \approx T_e/ea$

Experiment	$T_{e,0}$ (keV)	B (T)	a (m)	$\tilde{E}/E_{MSE}$
NSTX-U	$\sim 2-4$ (?)	1	0.6	$1 - 2 \times 10^{-3}$
DIII-D	2-5	2	0.7	$0.5 - 1 \times 10^{-3}$
Pegasus	$\sim 0.3$	0.3	0.35	$0.7 - 1 \times 10^{-3}$

- $\tilde{E}$  turbulence broadband, majority of fluctuation power < 300 kHz
- $\tilde{E}$ ,  $\tilde{n}$  rise from core to edge
- $\tilde{E}/E_{MSE}$  comparable to typical photon noise floor for BES



# Spectrometer Requirements

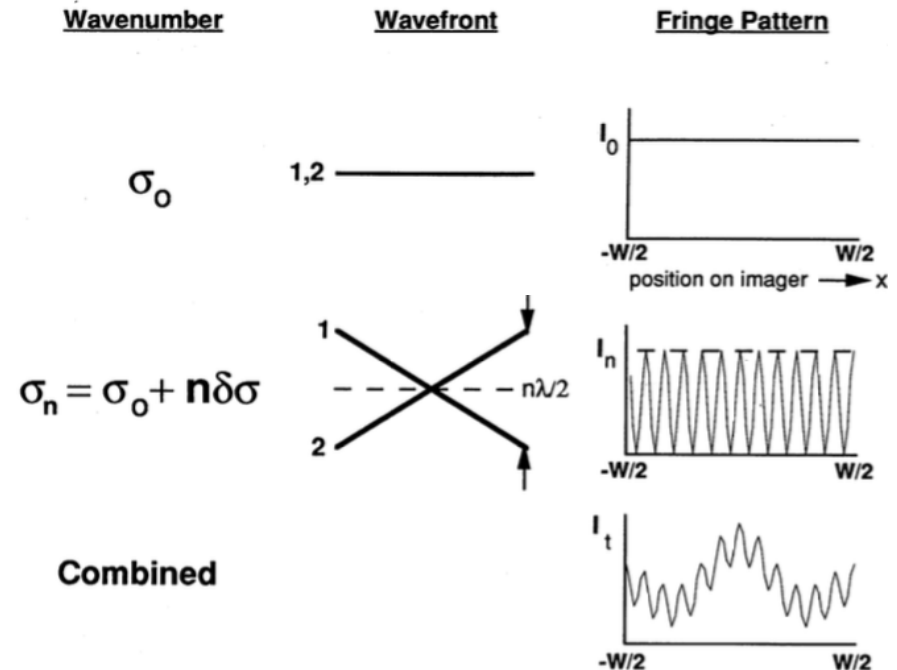
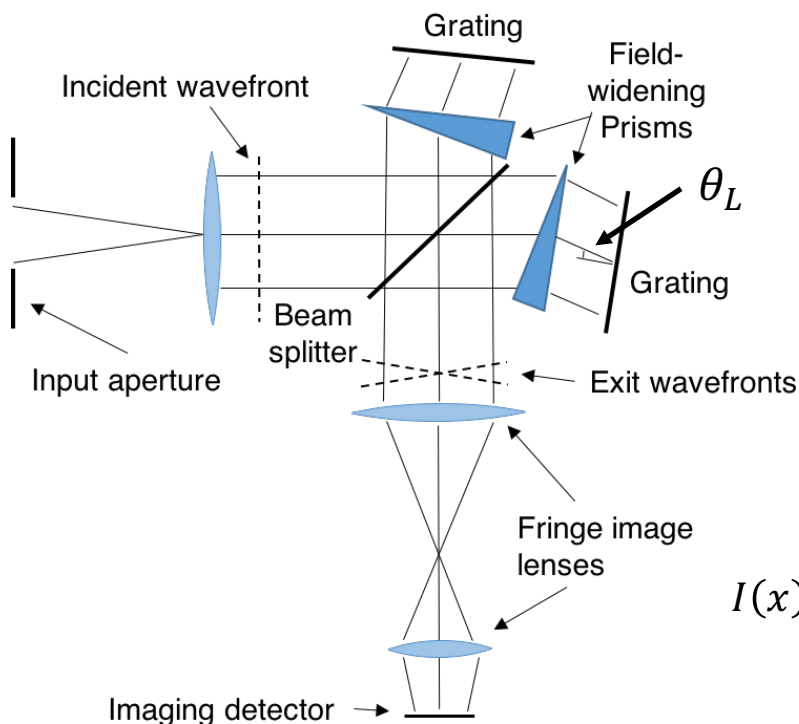


# $\Delta\tilde{\lambda}_\pi$ Spectrometer Requirements are Formidable

- Resolution:
  - Need  $\sim 8$  spectral bins to resolve 2 gaussian-like  $\pi$  components
  - $\Delta\lambda_{H\alpha}^\pi \sim 4 \text{ \AA}$  giving a spectral resolution of  $0.5 \text{ \AA}$ ,  $R = \frac{\lambda}{\delta\lambda} \sim 1.3 \times 10^4$
- Throughput:
  - Matched to collection optics, port availability,  $U = 0.01 - 0.1 \text{ cm}^2\text{-str}$
  - 2 spatial points desired
- Compatible detector system:
  - $\sim 250 \text{ kHz}$  time response
- Mitigation of sightline-DNB geometric broadening

# Spatial Heterodyne Spectroscopy Meets $\tilde{E}$ Spectrometer Requirements

- Self scanned, 2 beam interferometer
- Input wavelengths heterodyned around Littrow wavelength
- Field widening prisms increase throughput



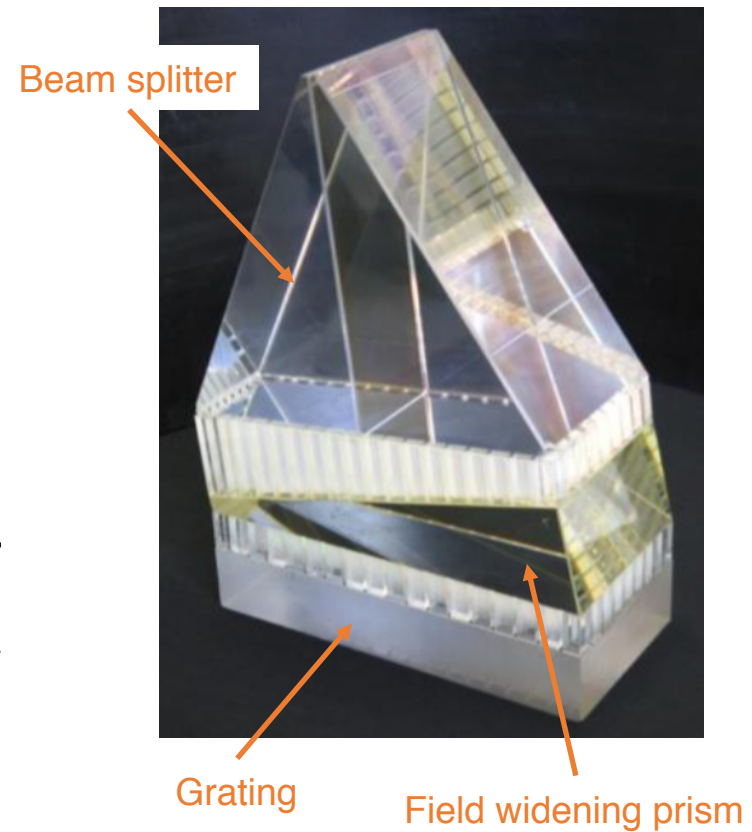
$$I(x) = \int_0^{\sigma} B(\sigma) (1 + \cos[2\pi(4|\sigma - \sigma_0|x \tan \theta_L)]) d\sigma$$



# Spatial Heterodyne Spectroscopy Achieves High Resolution and Throughput

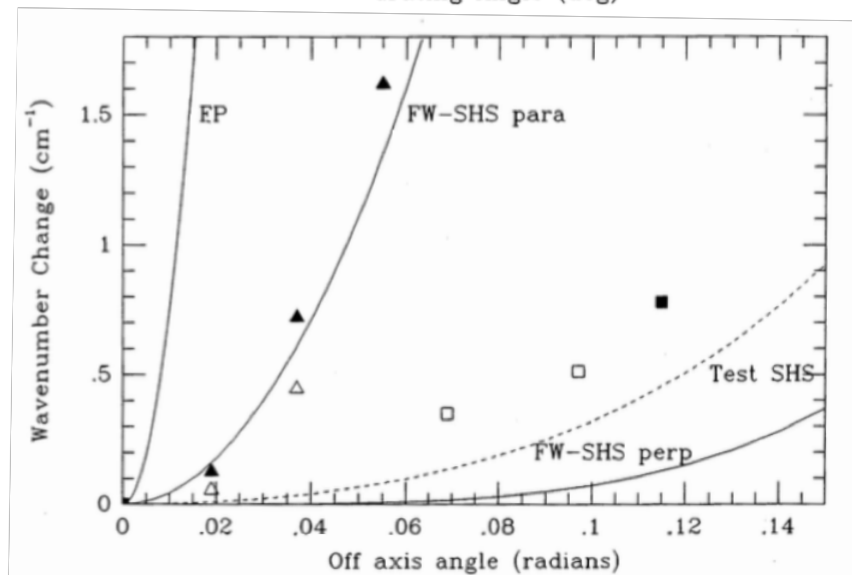
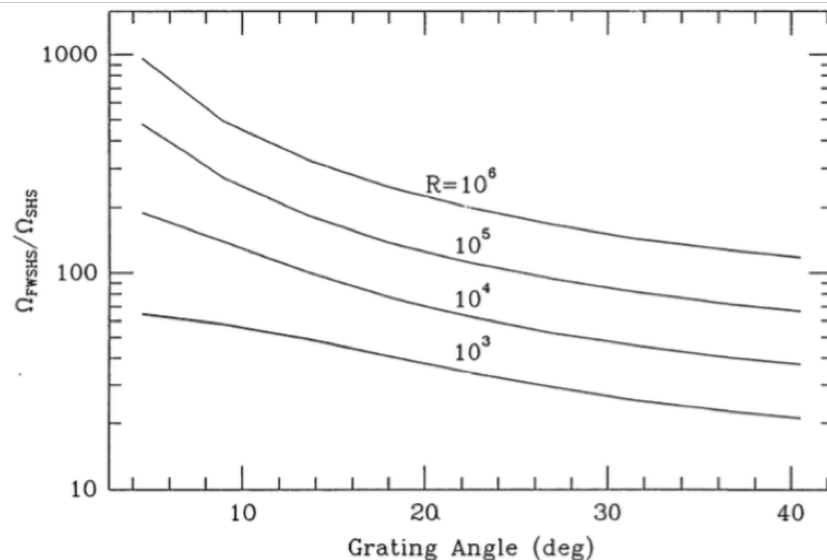
- SHS theoretical resolving power:
  - $R = \sigma / \delta\sigma \approx 2W / d$
  - For  $\tilde{E}$ : Need  $R \sim 1 \times 10^4$
  - For  $W = 50$  mm only requires  $d = 1/100$  lines/mm
  - Resolution readily achievable with simple coarse gratings, compact size
- SHS throughput comparable to field widened Fourier Transform spectrometer
  - For  $\tilde{E}$ : need throughput of  $0.01 - 0.1 \text{ cm}^2 \text{str}$
  - $U = 2\pi\eta A / R = 0.0015\eta \text{ cm}^2 \text{str}$ ;  $\eta \sim 1$  (no field widening) – 100 (field widening)

Example SHS:  
Monolithic DASH Interferometer  
 $R \approx 5 \times 10^4$ ,  $U \approx 0.15 \text{ cm}^2 \text{str}$



# Field Widening in SHS Increases Throughput, No Moving Parts

- Field widening prisms greatly reduce the path length difference dependence of off-axis ray angle
- Allows for large input angle  $\Omega$
- Required throughput ( $0.1 \text{ cm}^2\text{-str}$ ) readily achievable using prisms in SHS
- Prism angle definition:



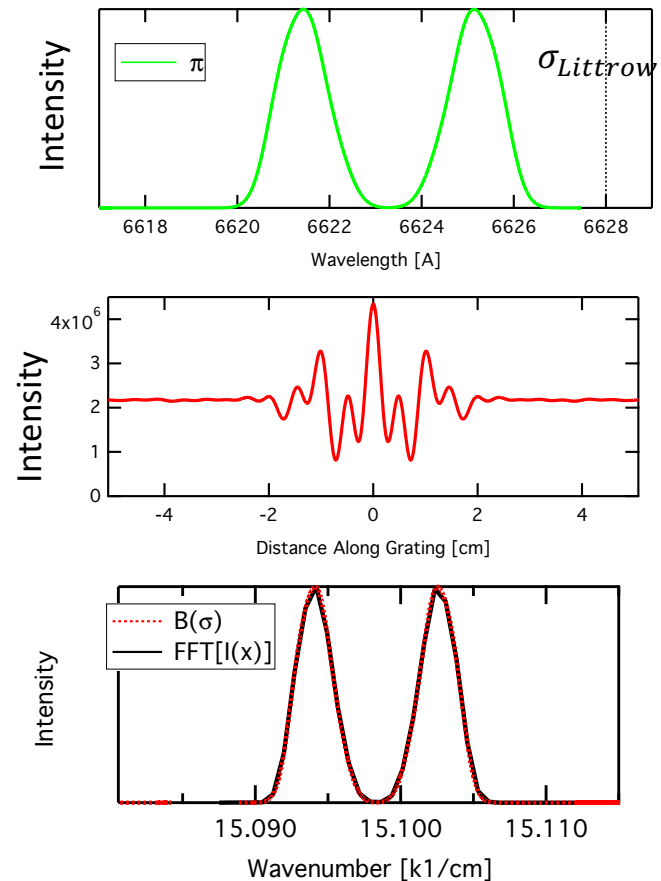
# Interferometer Modeling



# Modeling of Interferogram Used to Explore Spectrometer Design

- Synthetic interferograms generated via modeled  $\pi$  components
- Fourier transform of interferogram  $I(x)$  gives  $B(\sigma)$
- High speed recording and inversion of  $I(x)$  is similar to gaussian fit analysis of  $\tilde{T}_i$  and  $\tilde{v}$  measurements

$$I(x) = \int_0^{\sigma} B(\sigma)(1 + \cos[2\pi(4|\sigma - \sigma_0|x \tan \theta_L)])d\sigma$$



# New CMOS Imaging Technology Provides Turbulence Timescale Measurement

- Flexible, high speed recording of full interferogram at photon noise limit
- Example: Phantom v2512 FAST by Vision Research
  - 500 kHz @ 256 x 80 pixels or 110 x 110 pixels
  - f/1 optics gives  $U \sim 0.1 \text{ cm}^2\text{str}$
  - QE  $\sim 50\%$  over visible range
  - Integrated DAQ
- Potential for 2 spatial measurements

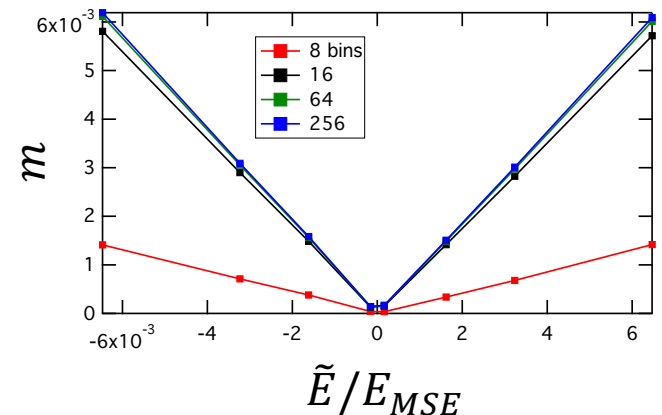
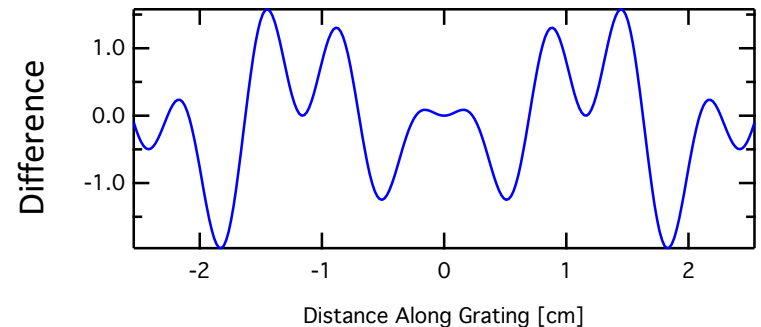
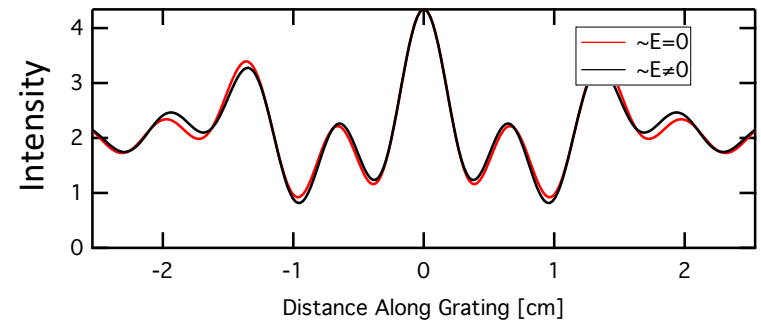


# Metric from Simplified Interferogram Scales Linearly with $\tilde{E}$ , Requires Less Detector Channels

- Want a metric that is proportional to  $\tilde{E}$
- Approach: finite number of bins around central fringe region measured to get  $\tilde{E}$
- Example metric ( $m$ ) based on differences in interferogram area from time average area:

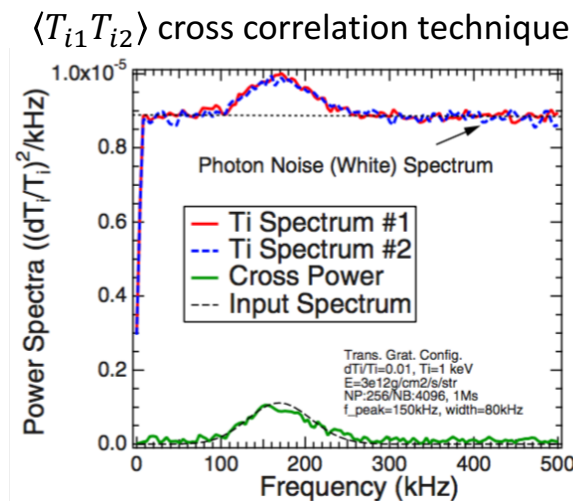
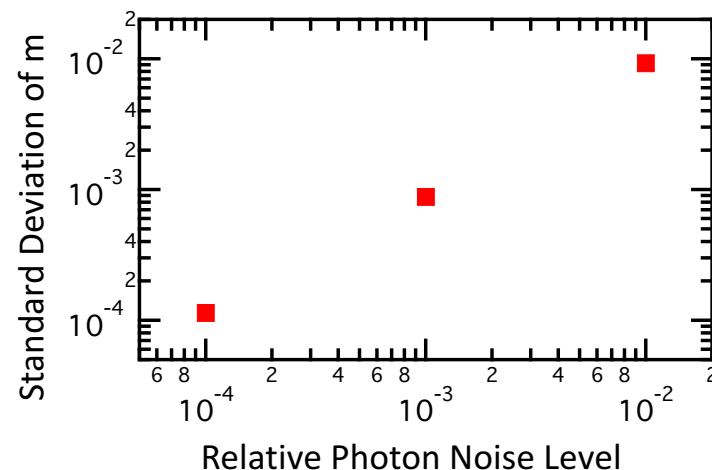
$$m = \sqrt{\frac{\sum_j^{N_{bins}} (I_{j,\tilde{E} \neq 0} - I_{j,\tilde{E} = 0})^2}{\sum_j^{N_{bins}} (I_{j,\tilde{E} = 0})^2}}$$

- $m = \tilde{E} / E_{MSE}$
- For given case 16 bins are adequate
- Design optimization ongoing, ideally reduce to 3-4 detectors for single spatial point



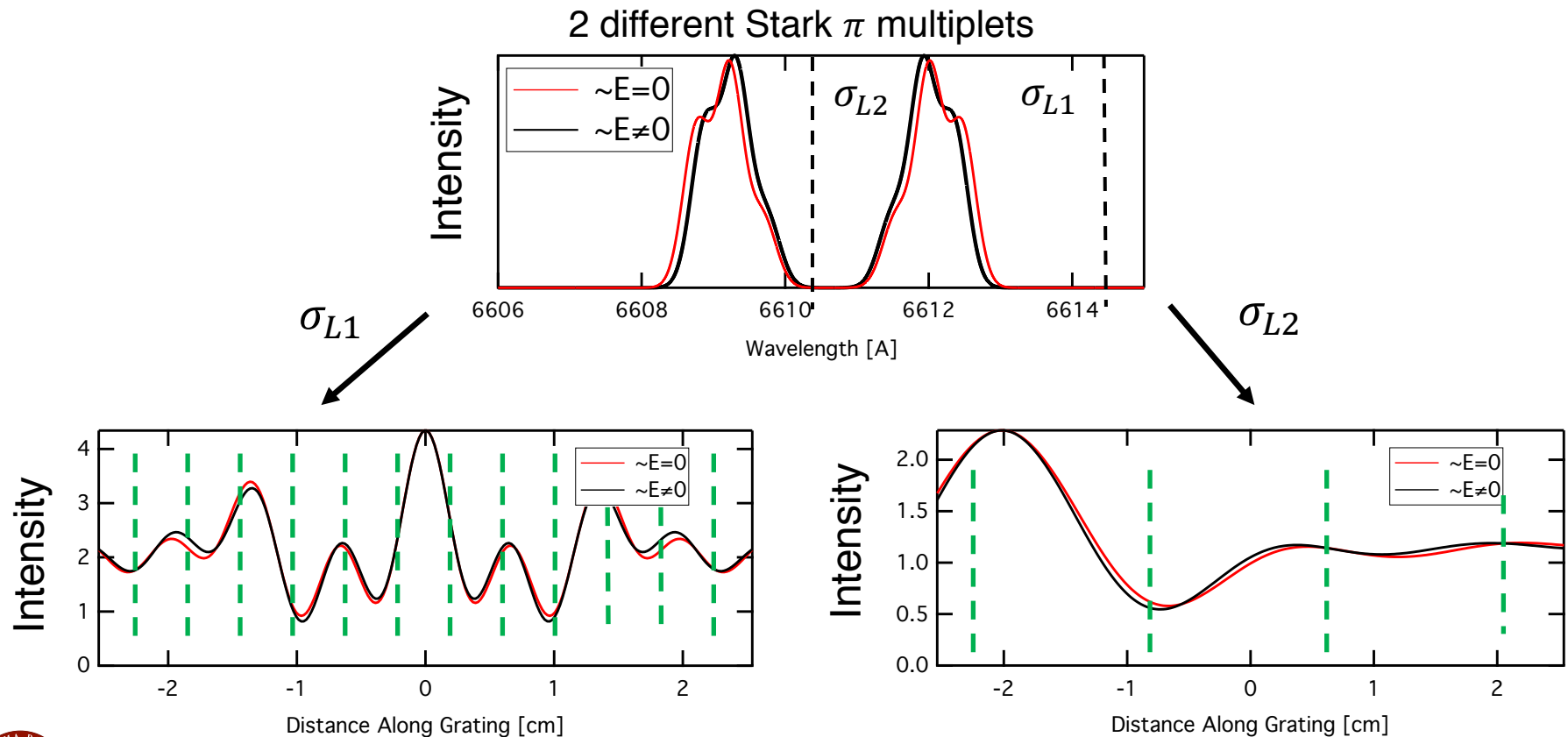
# Noise Floor for Multi-bin Metric Equal to Relative Photon Noise Level

- Simulated variation in metric due to photon noise shows relative noise in metric = photon noise level
- Measured photon flux is standard BES signal
  - BES photon noise level  $\sim 10^{-3}$
- Random photon noise can be suppressed by standard cross correlation techniques
  - Two independent but spatially correlated measurements made simultaneously
  - Example:  $\langle \tilde{E}_1 \tilde{E}_2 \rangle$  and  $\langle \tilde{E} \tilde{n} \rangle$
- Depending on data record length, can reduce residual noise floor by 10-100x



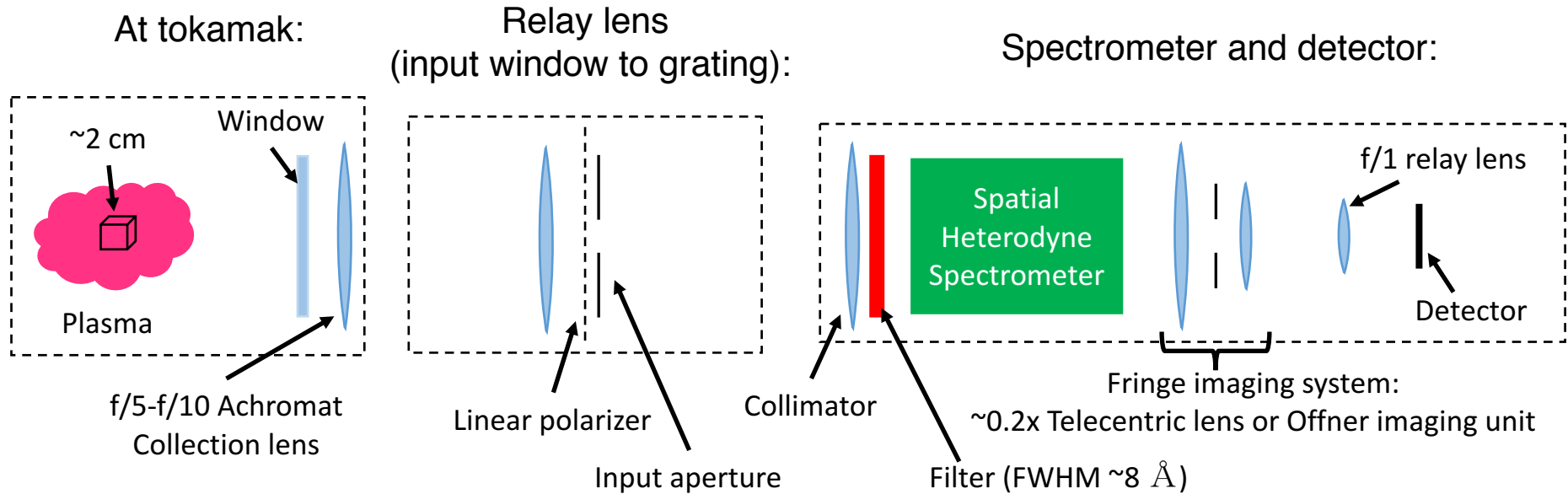
# Extracting $\widetilde{\Delta\lambda}$ From Central Fringe Analysis Could Reduce the Number of Detectors

- Full interferogram recording may not be necessary
- Can optimize spectrometer to give fringe pattern of interest without losing light
- $\widetilde{\Delta\lambda}(t)$  then recorded using 3-4 detectors



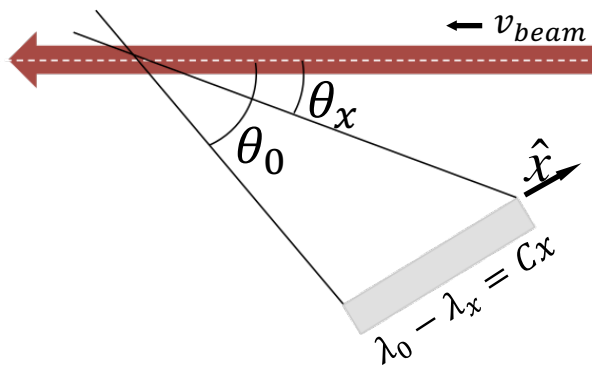


# Optics Require Conjugate Imaging, High Throughput

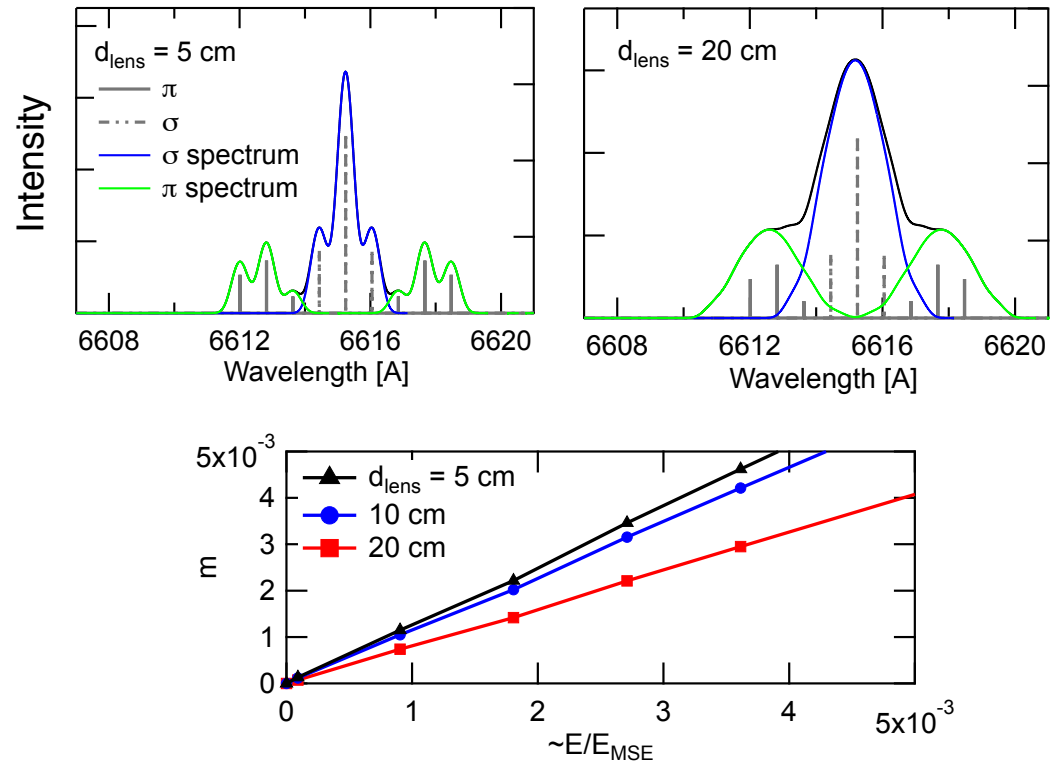


- Fringe image detection requires large depth of field, high throughput, no aberrations
  - Set by maximum path difference between wavefronts and/or coherence length of wavefronts
- Realized with telecentric lens or Offner imaging system and high throughput coupling lens to detector

# Geometric Broadening Compensated in SHS, Allows Large Collection Optic



Geometric broadening on DIII-D:



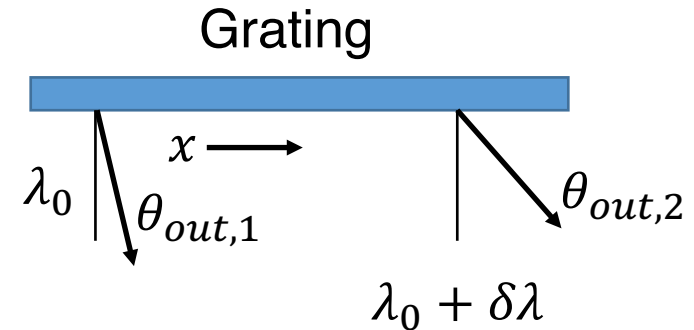
- SHS Fizeau fringe pattern is optically conjugate to input optic
- $\lambda$  (phase) shift due to window geometry  $\sim$ linear across grating

$$\phi_w = 2\pi cx \rightarrow \phi_{Total} = \phi_G + \phi_w = (8\pi(\sigma - \sigma_L)\tan\theta + \phi_w(x))x$$

- Convolve  $I(x)$  with  $\mathcal{F}[\exp(-i\phi_w)]$  in the spectral domain to remove geometric broadening

# Geometric Broadening can be Actively Compensated For Inside Spectrometer

- Doppler shift across window means that the output angle from the grating is changing across the grating face
- In principle,  $\theta_{out}$  can be kept constant by varying the grating groove constant in direct opposition to the change in  $\sigma$  due to geometric broadening
- Window effect becomes known linear phase shift across image plane, can be removed
- Similar to Doppler shift compensation in Fabry-Perot spectrometers used to measure planetary wind velocity<sup>1</sup>

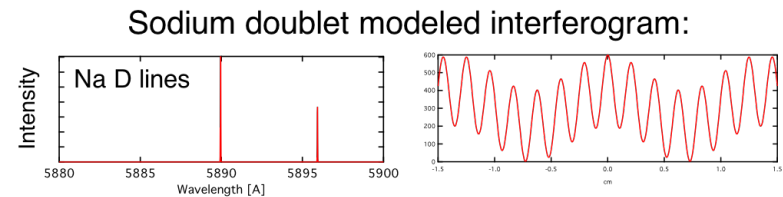
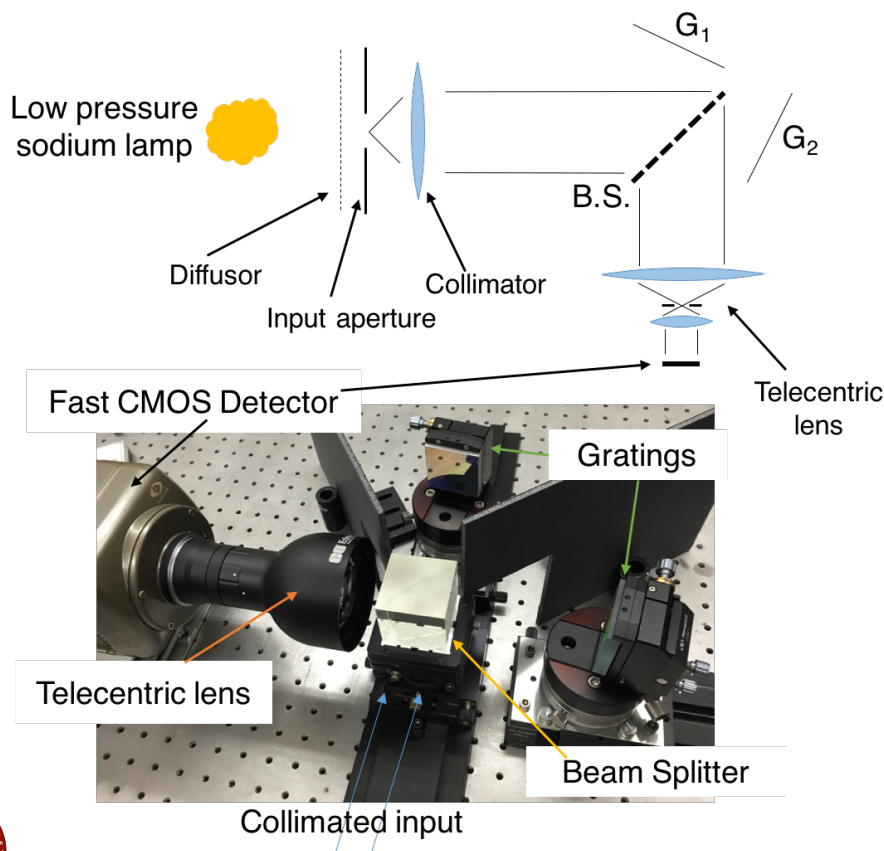


$$\sin(\theta_{out}(x)) = \frac{md}{\sigma(x)} - \sin \theta_L$$

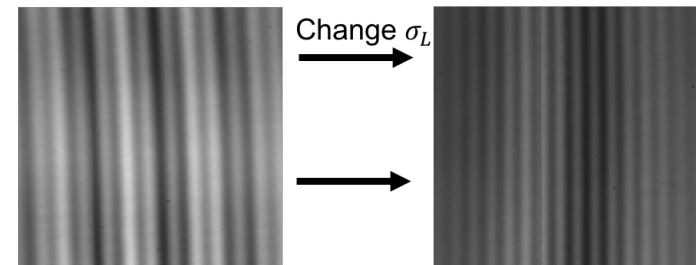
$$\sin(\theta_{out}(x)) = \frac{md(x)}{\sigma(x)} - \sin(\theta_L(x))$$

# Flexible Modular SHS System Developed for First Tests

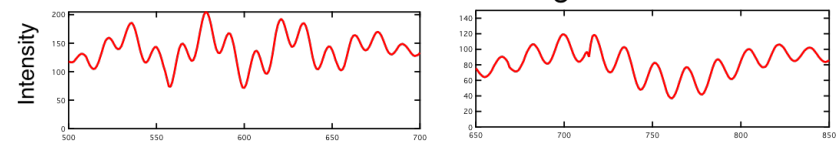
- Initial testing done using Na doublet, manipulation of interferogram explored
- Fabrication and testing of second SHS underway, to be deployed on Pegasus for initial validation using large amplitude, low frequency,  $\vec{B}$  and  $\vec{E}$  generated by helicity injectors



Sodium doublet in prototype SHS:



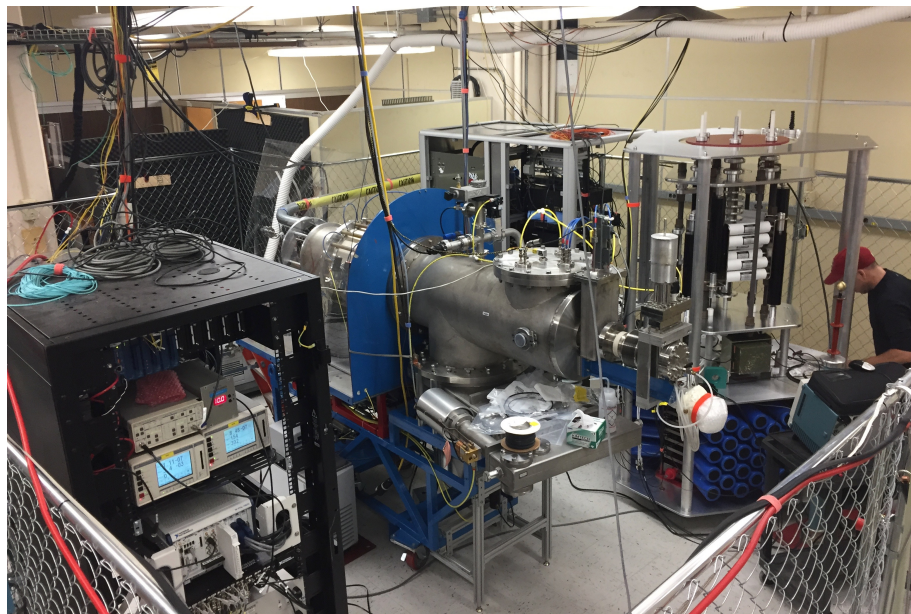
Measured interferograms:



# $\tilde{E}$ Diagnostic Requires Low Divergence, High Full Energy Fraction DNB

- $H^0$  DNB on loan from PPPL
  - Full-energy  $J$  at focus: 3-6 mA/cm<sup>2\*</sup>
  - Diameter  $\sim 9$ cm
- Features favorable for measurement
  - Low divergence:  $\leq 0.47^\circ$ 
    - Mitigates Divergence line broadening
  - High  $E_b \sim 60 - 80$  keV
    - Maximizes MSE broadening
  - 90-95% ionization at full beam energy
    - Ensures maximum signal for diagnostic

DNB refurbishment lab



See M. Bakkens Poster

# Summary: Moving Towards Diagnostic For $\tilde{E}$ and $\tilde{B}$ in High Temperature Magnetically Confined Plasmas

- $\tilde{E}$  measurements appear feasible using high speed measurements of motional stark multiplet
  - Horizontal view gives  $\tilde{E}_z$ , off midplane gives  $\tilde{E}_R$
  - $\tilde{B}$  measurement also possible using Stark multiplet
- SHS provides flexible, compact, spectrometer concept
  - Full spectrum measurement available
  - Subsampling interferogram may support multiple spatial channels with simple discrete detectors like BES
- Next steps:
  - Commission low divergence, 80 keV/amu DNB
  - Deploy beam to Pegasus for preliminary measurements of large amplitude, low frequency  $\tilde{B}$  and  $\tilde{E}$