

Predictive Modelling and Helicity Dissipation Scaling Studies for Local Helicity Injection Non-Solenoidal ST Startup

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PEGASUS
Toroidal Experiment



Layout Slide (Include for Posters)

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Predictive Modelling and Helicity Dissipation Scaling Studies for Local Helicity Injection Non-Solenoidal ST Startup

LHI Path to High I_p
Startup

LHI is a Promising
Non-Solenoidal
Startup Technique

Hierarchy of Physics
Models Contribute to
the Understanding
of LHI Startup

Path to High I_p
Depends on Choice of
LHI Injector
Geometry

LFS LHI is the
Focus of Present
PEGASUS
Operations

0-D Power Balance
Model Insights

0-D Power Balance
Model Incorporates
Analytic Plasma
Inductance (ψ_{Le} , ψ_{PF})
Formulae

LFS LHI Dominated
by V_{IND} , V_{LHI} Drops
as Plasma Grows

0-D Model
Reproduces $I_p(t)$,
Taylor Limited in
Early Phase

Model Insights
Provides Strategy
Towards Scaling to
Higher I_p

Validating URANIA
Operational Scenario
on PEGASUS

Taylor Limit Increase
Early in LFS
Discharges: Access to
Higher I_p

Experiment Tests
Early Taylor Limit
Scaling Through I_{TF}
Scan

Early Phase $I_p(t)$
Exhibits I_{TF} Scaling

Early Phase I_p
Scales with $\sqrt{I_{TF}}$ as
Expected from
Taylor Limit

Dissipation in LFS
LHI

Inductive Reactance
is the Dominant
Contribution to Net
Plasma Impedance

Similar T_e Profiles at
Different I_{TF} Levels

Peaked T_e Profiles
when Coupled to
Injectors

Scaling LHI toward
NSTX-U Startup

Model Applied to
NSTX-U Geometry
for Initial $I_p \sim 0.8$ MA
Scenario

URANIA Experiments
will Test NSTX-U
Startup Scenario

Near Term PEGASUS
Experiments to
Establish URANIA
Operation

LFS LHI Provides a
Path Toward
Scalable, non-
inductive, high I_p
Startup





LHI Path to High I_p Startup

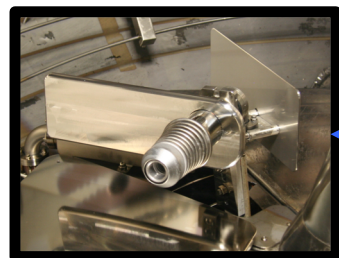


LHI is a Promising Non-Solenoidal Startup Technique



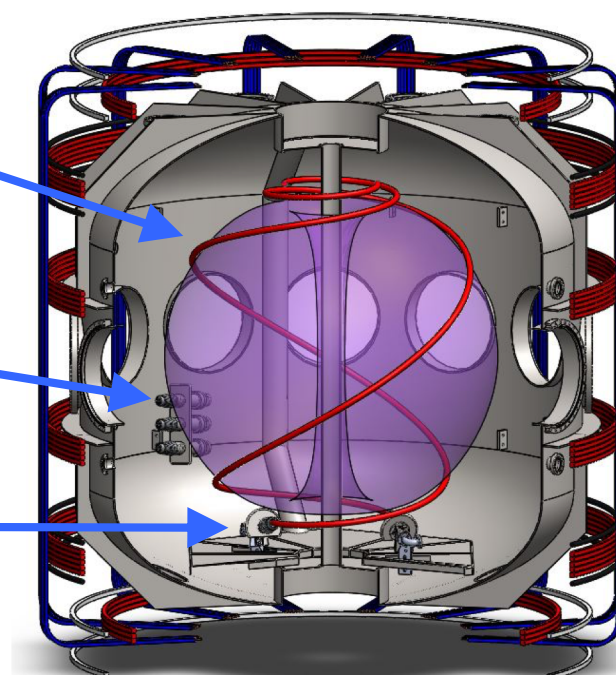
LFS System

HFS System



Injected
Current Stream

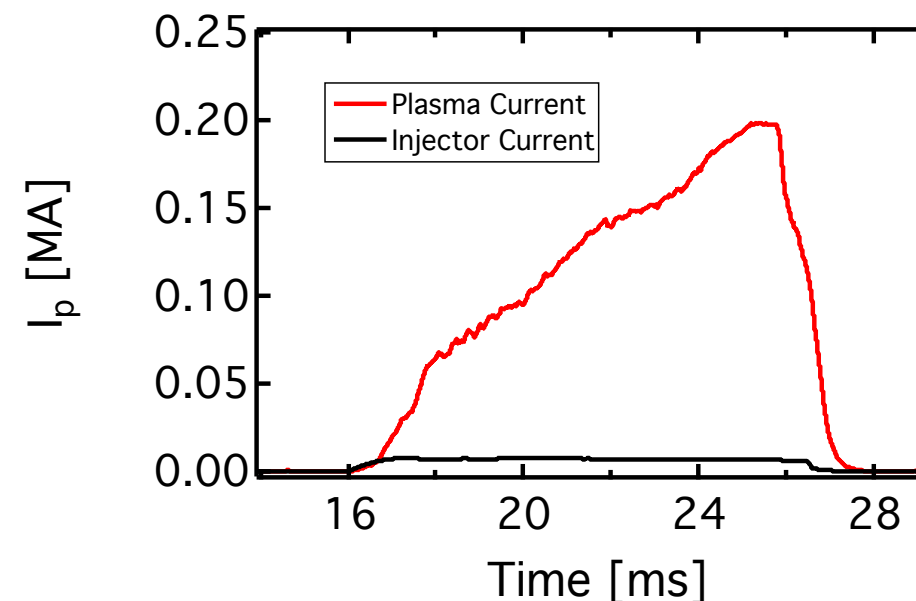
Local
Helicity
Injectors



PEGASUS Parameters

A	1.15 – 1.3
R [m]	0.2 – 0.45
I_p [MA]	≤ 0.25
B_T [T]	< 0.15
Δt_{shot} [s]	≤ 0.025

Non-Solenoidal, High $I_p \leq 0.2$ MA ($I_{inj} \leq 8$ kA)



- Edge current extracted from injectors
- Relaxation to tokamak-like state via helicity-conserving instabilities
- Used routinely for startup on PEGASUS



Hierarchy of Physics Models Contribute to the Understanding of LHI Startup

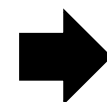
1. Taylor relaxation, helicity conservation

- Steady-state maximum I_p limits

Taylor Relaxation

$$\nabla \times B = \mu_0 J = \lambda B$$

$$\lambda_p \leq \lambda_{edge}$$



$$I_p \leq \sqrt{\frac{1}{B_{\theta+v,inj}/I_p} \frac{\Psi_T I_{inj}}{2\pi R_{inj} w_{inj}}}$$

2. 0-D power-balance $I_p(t)$

- V_{LHI} is effective LHI current drive
- V_{IND} is net drive from PF, shape, I_p and L changes

Helicity Conservation

$$I_p R_p \leq V_{LHI} \approx \frac{A_{inj} B_{t,inj}}{\Psi_T} V_{inj}$$

3. 3D Resistive MHD (NIMROD)

- Physics of LHI current drive mechanisms

J.L. Barr, et al. Nucl. Fusion Nuclear Fusion **58**, 076011 (2018)

D.J. Battaglia, et al. Nucl. Fusion **51** 073029 (2011)

N.W. Eidietis, Ph.D. Thesis, UW-Madison (2007)

J. O'Bryan, C.R. Sovinec, Plasma Phys. Control. Fusion **56** 064005 (2014)

Taylor Limit Constrained Power Balance

$$I_p [V_{LHI} + V_{IND} + V_{IR}] = 0 ; I_p \leq I_{TL}$$



Path to High I_p Depends on Choice of LHI Injector Geometry

LFS

- Pros:

- More physical access $\rightarrow$ retractable helicity sources
- Added poloidal field induction
- Geometry allows for large A_{inj}
- Less prone to PMI
- Simpler null formation

- Cons:

- Less V_{LHI} for same injector system (V_{inj} , A_{inj})
- Passively unstable radial position

HFS

- Pros:

- Increased V_{LHI} for same injector system (V_{inj} , A_{inj})
- Passively stable radial position

- Cons:

- Reduced physical access
- Space restriction in lower divertor region
- More PMI prone
- More difficult null formation

PRESENT APPROACH: LFS LHI provides more attractive path to high I_p startup



LFS LHI is the Focus of Present PEGASUS Operations

- PEGASUS Operations to develop URANIA scenarios
 - Validate LFS I_p scaling
 - Increase early phase Taylor Limit
 - Non-circular, high A_{inj} injector design testing
 - Electron confinement and impurity studies
- Moving to high I_p LHI development in URANIA Experiment
 - URANIA: upgraded PEGASUS for general non-inductive startup development
- Developing NSTX-U Startup in URANIA
 - High $B_{TF} \rightarrow I_p$, confinement scaling, and injector technology
 - Shape and V_{LHI} control
 - Expanded diagnostic capability
 - Advanced (large scale relevant) injector design



0-D Power Balance Model Insights



0-D Power Balance Model Incorporates Analytic Plasma Inductance (ψ_{Le} , ψ_{PF}) Formulae

$$I_p \left[\underbrace{V_{PF} + V_{Le} - V_{Wm}}_{V_{IND}} - \underbrace{V_{IR}}_{\text{Resistive}} + \underbrace{V_{NICD}}_{\text{LHI}} \right] = 0$$

- $I_p(t)$ determined via numerically solving initial value problem
- Inputs: shape(t), $\langle \eta_p \rangle$, $l_i(t)$, $\beta_p(t)$
- Analytic, finite-A descriptions calculate ψ_{Le} , ψ_{PF} assuming radial force balance

Inductive Drive from Poloidal Fields

$$V_{PF} = -\frac{\partial}{\partial t} \psi_{PF} \approx -\frac{\partial}{\partial t} \left[I_p M_V \pi R_0^2 \left(\frac{B_V}{I_p} \right) \right]$$

$$\frac{1}{\mu_0} \frac{B_V}{I_p} = -\frac{1}{4\pi R_0} \left\{ \frac{1}{\mu_0} \frac{\partial L_e}{\partial R_0} + \left(\beta_p + \frac{l_i}{2} \right) - \frac{1}{2} \right\}$$

$$\frac{1}{\mu_0} M_V = R_0 \frac{(1 - \epsilon)^2}{(1 - \epsilon)^2 f_c + f_d \sqrt{\kappa}}$$

Plasma Magnetic Energy Change

$$V_{Wm} = \frac{1}{I_p} \frac{\partial}{\partial t} \left[\frac{1}{2} L_i I_p^2 \right] - V_{RTT} \quad L_i = \mu_0 l_i \frac{V_P}{\ell_P^2}$$

$$V_{RTT} = \frac{I_p}{2\mu_0} \oint \oint_{S_P} \left(\frac{B_p}{I_p} \right)^2 \vec{v}_b(\theta) \cdot \hat{n} dS$$

$\left(\frac{B_p}{I_p} \right)$ from Miller local equilibrium model
Shape, B_t , q_{edge} dependencies

Inductive Drive from Shape Evolution

$$V_{Le} = -\frac{\partial}{\partial t} [L_e I_p]$$

$$\frac{1}{\mu_0} L_e = R_0 \frac{f_a(1 - \epsilon)}{(1 - \epsilon) + \kappa f_b} \quad \begin{matrix} f_a = \text{fitting} \\ \text{function} \end{matrix}$$

Resistive Dissipation

$$V_{IR} = I_p R_p = I_p \left(\frac{\langle \eta_p \rangle 2\pi R_0}{A_p} \right)$$

LHI Drive

$$V_{LHI} = \frac{A_{inj} B_{\phi, inj}}{\psi_T} V_{inj}$$

J.L. Barr et al., Nucl. Fusion Nuclear Fusion **58**, 076011 (2018)





LFS LHI Dominated by V_{IND} , V_{LHI} Drops as Plasma Grows

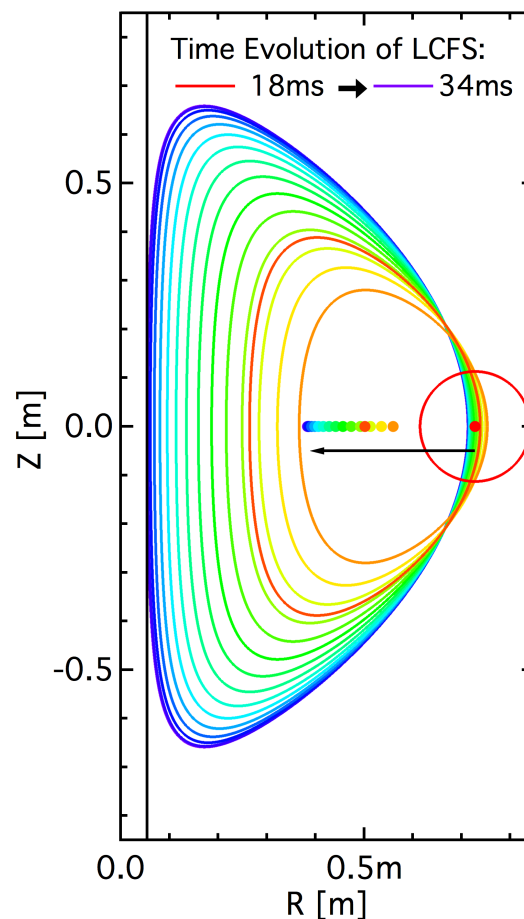
Taylor Limited Phase

- Small, outboard limited plasma
 - Low Taylor Limit
 - Ample Drive

Drive Limited Phase

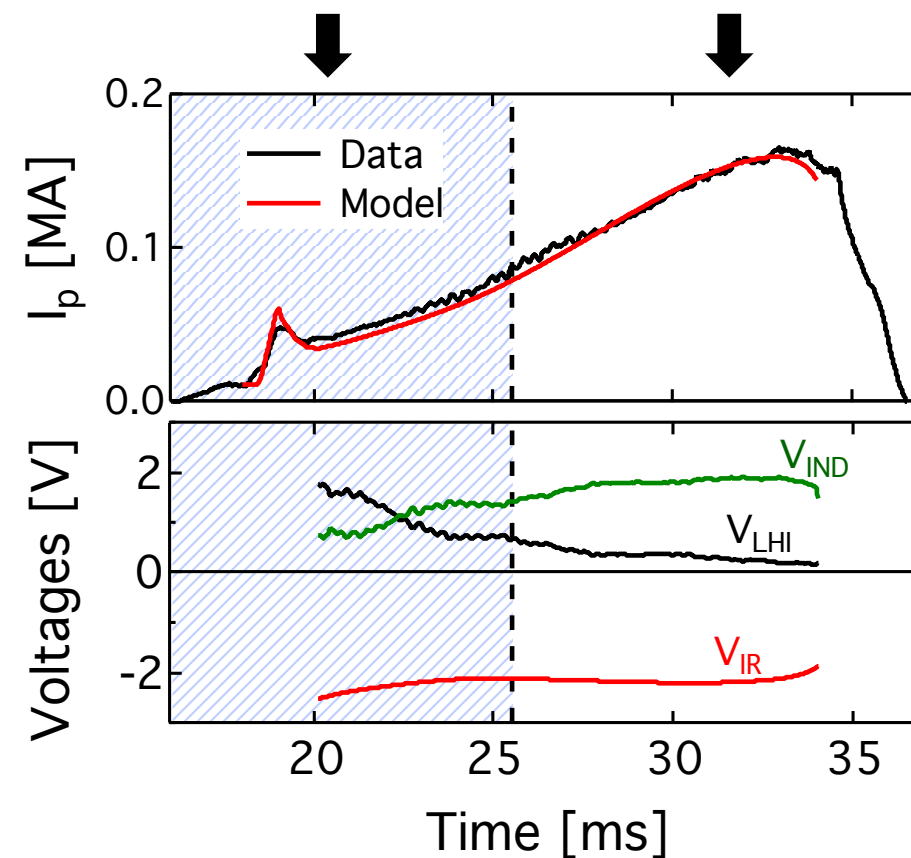
- Plasma expands inward
 - Taylor Limit increases
 - V_{LHI} decreases
 - V_{IND} dominates

Typical LFS Geometry Evolution



Taylor Limited Phase

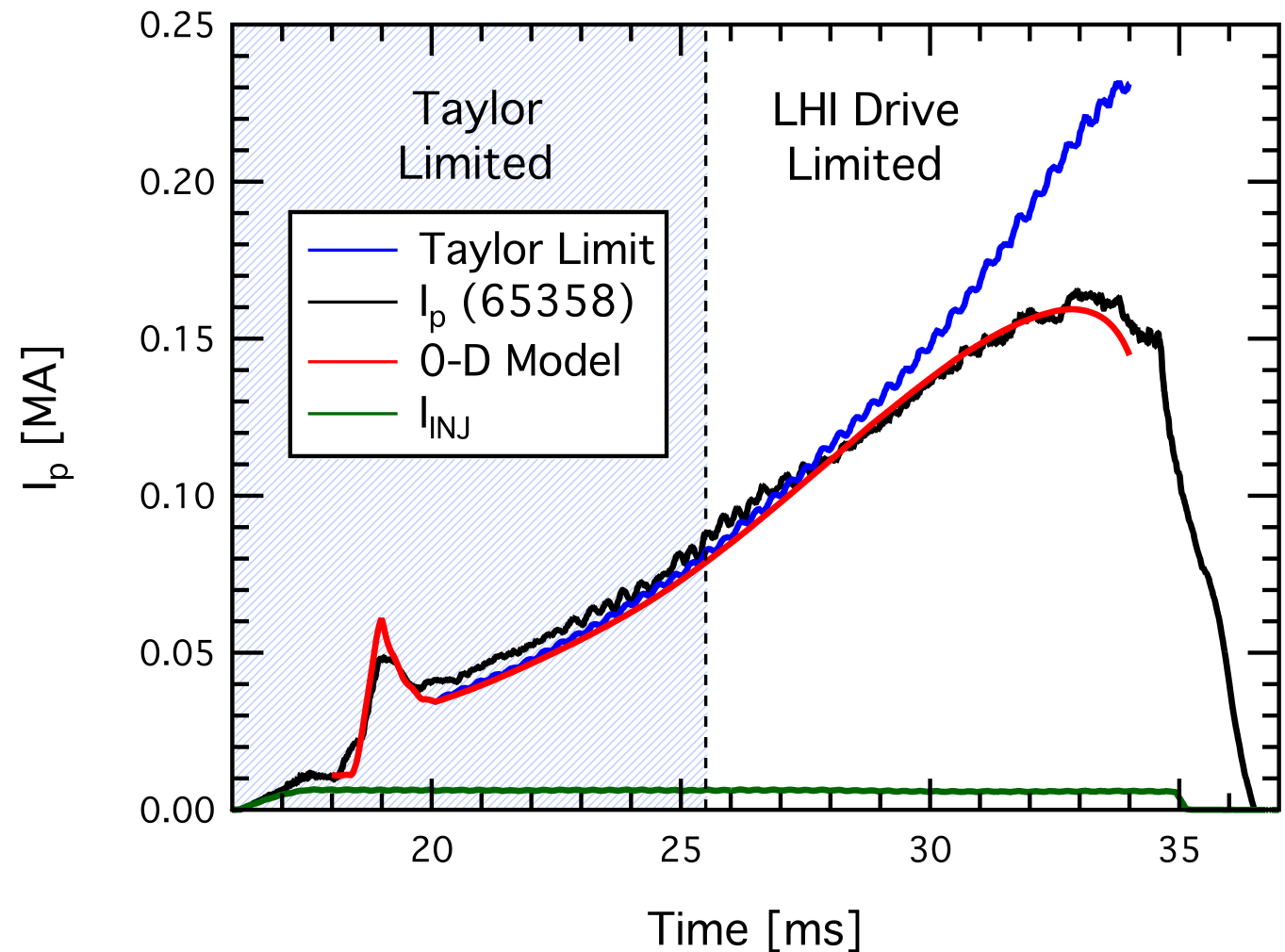
LHI Drive Limited Phase





0-D Model Reproduces $I_p(t)$, Taylor Limited in Early Phase

- Model reproduces experiment
 - Assumed constant $\langle \eta_p \rangle$
 - Constrained shape evolution
 - Experimental injector parameters
- Two-phase $I_p(t)$ evolution
 - Early: Taylor Limited
 - Late: Drive Limited





Model Insights Provides Strategy Towards Scaling to Higher I_p

- Increase net poloidal flux in early phase to provide more V-sec during shape evolution
- Increase Taylor limit in the early phase of the discharge
- Provide sufficient V_{LHI} to drive system up to early phase Taylor limit



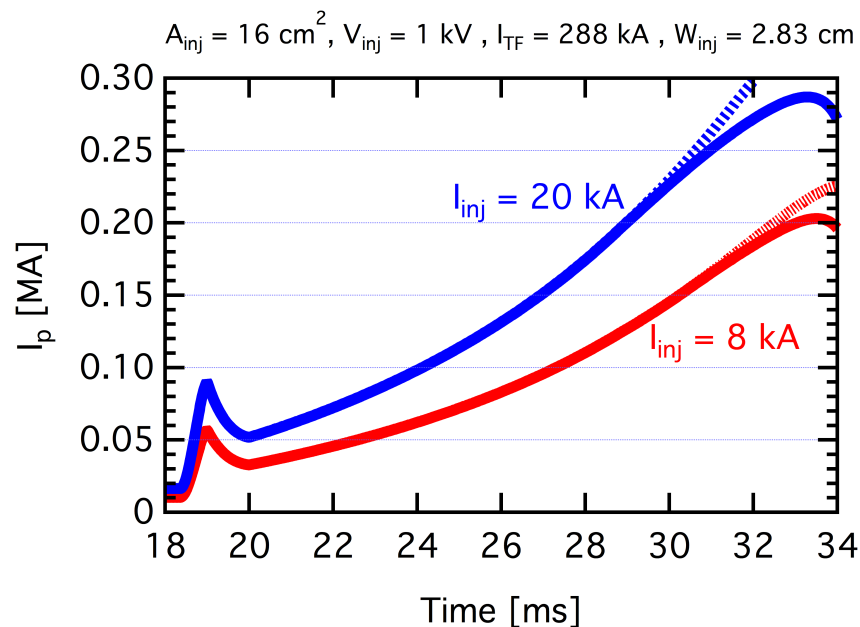
Validating URANIA Operational Scenario on PEGASUS



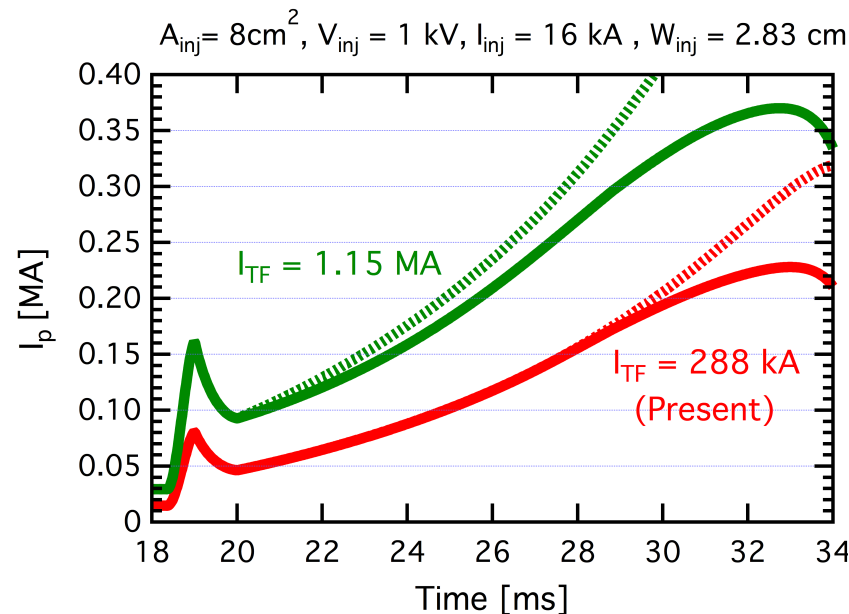
Taylor Limit Increase Early in LFS Discharges: Access to Higher I_p

- LFS discharges experience an extended Taylor-limited I_p phase
- Increase Taylor limit through injector design or facility modifications $I_{TL} \sim \sqrt{\frac{I_{TF} I_{INJ}}{W_{INJ}}}$

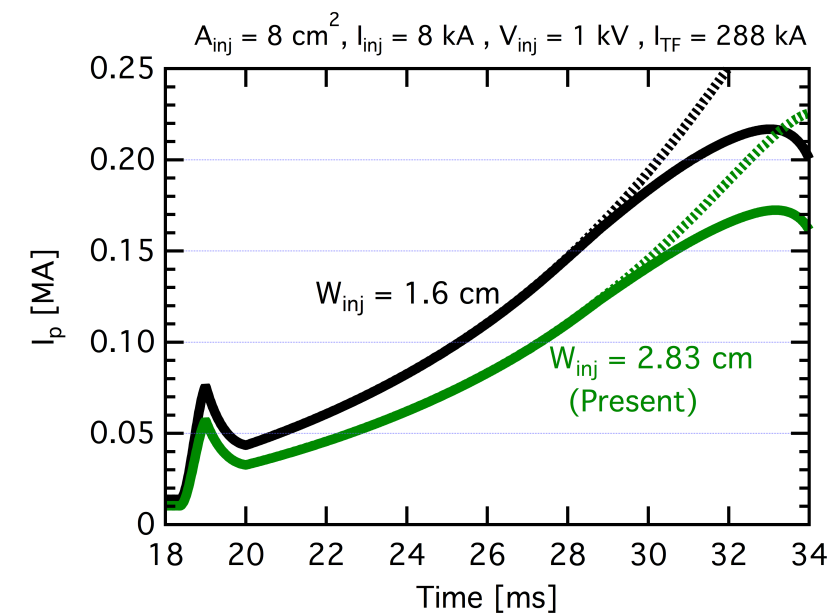
Increase I_{inj}



Increase I_{TF}



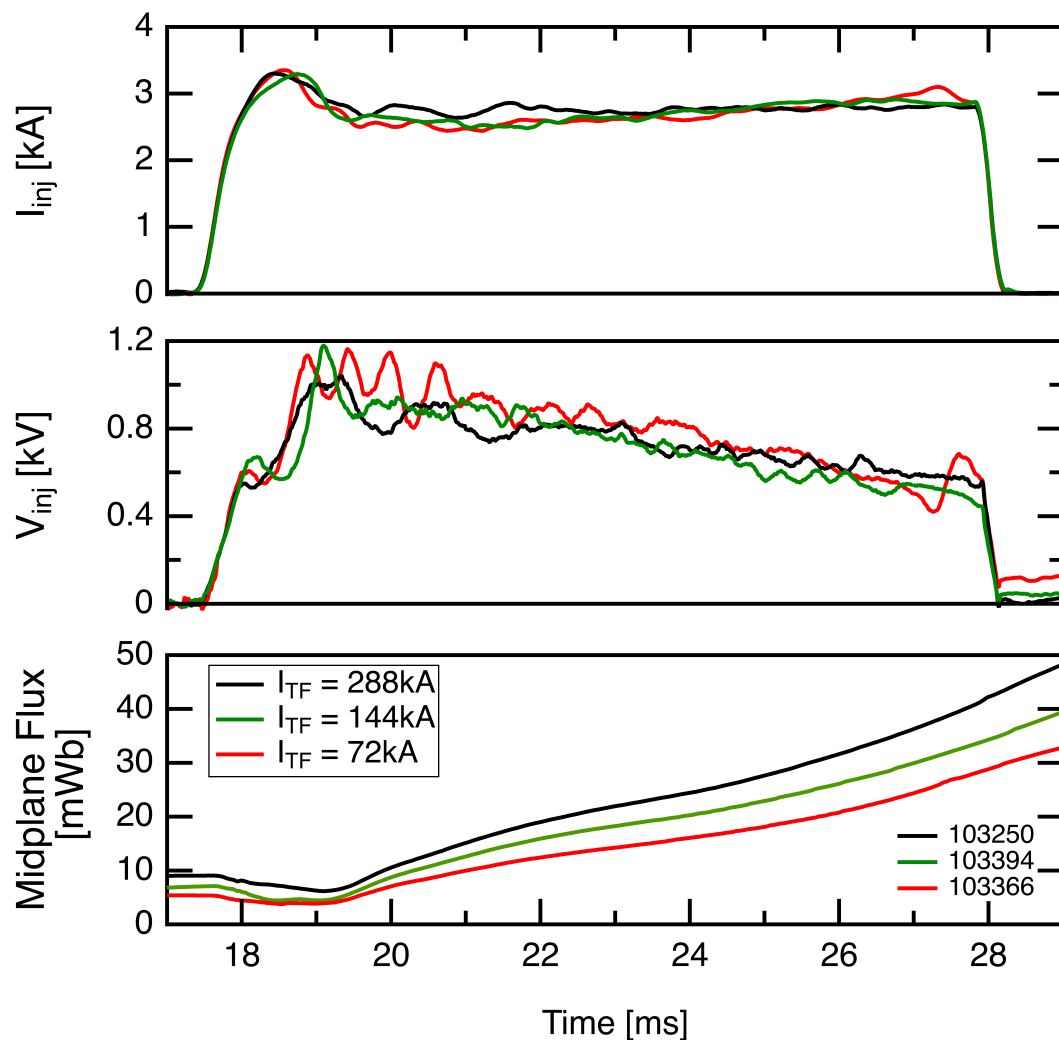
Decrease W_{inj}



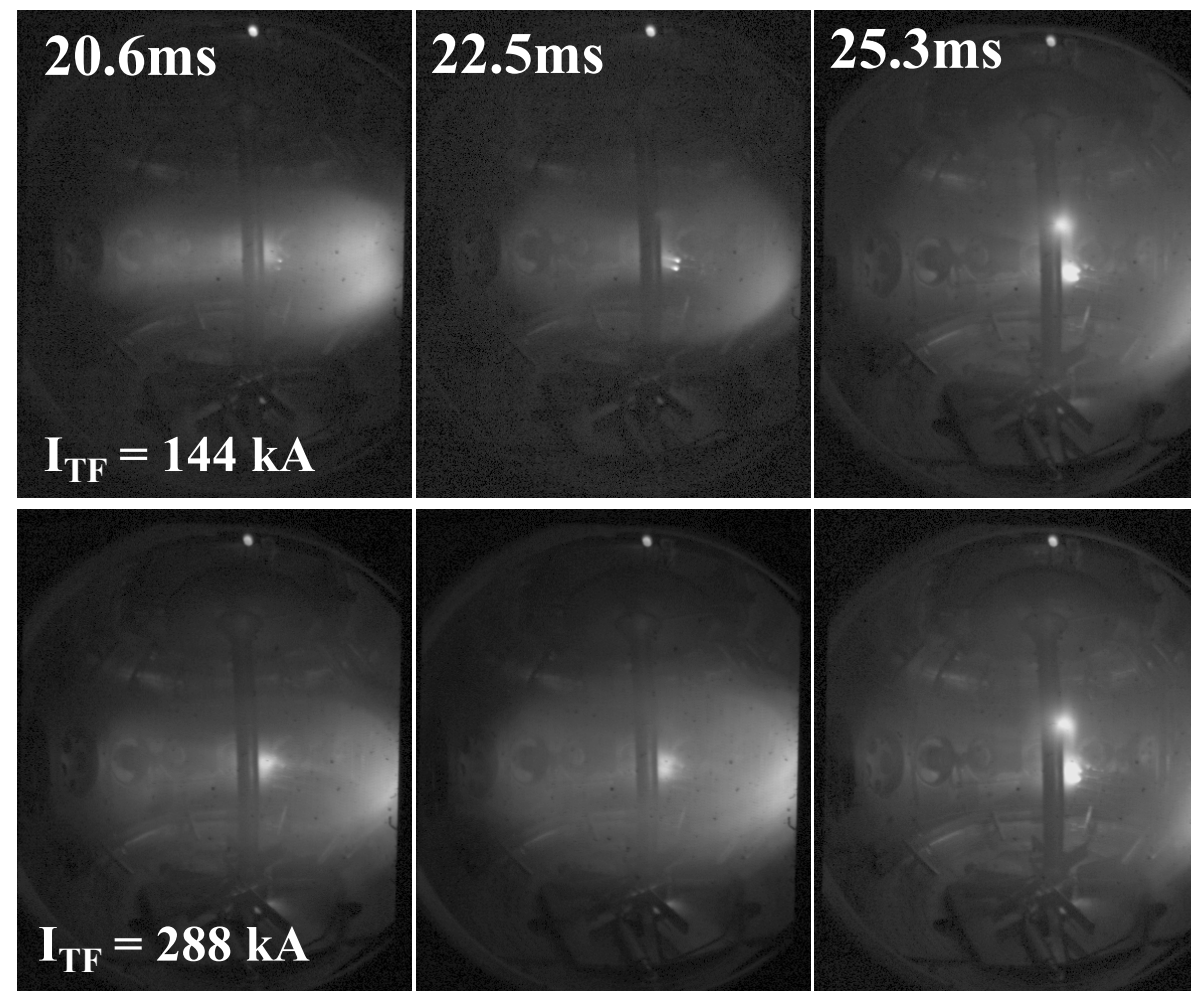


Experiment Tests Early Taylor Limit Scaling Through I_{TF} Scan

- Injector parameters matched



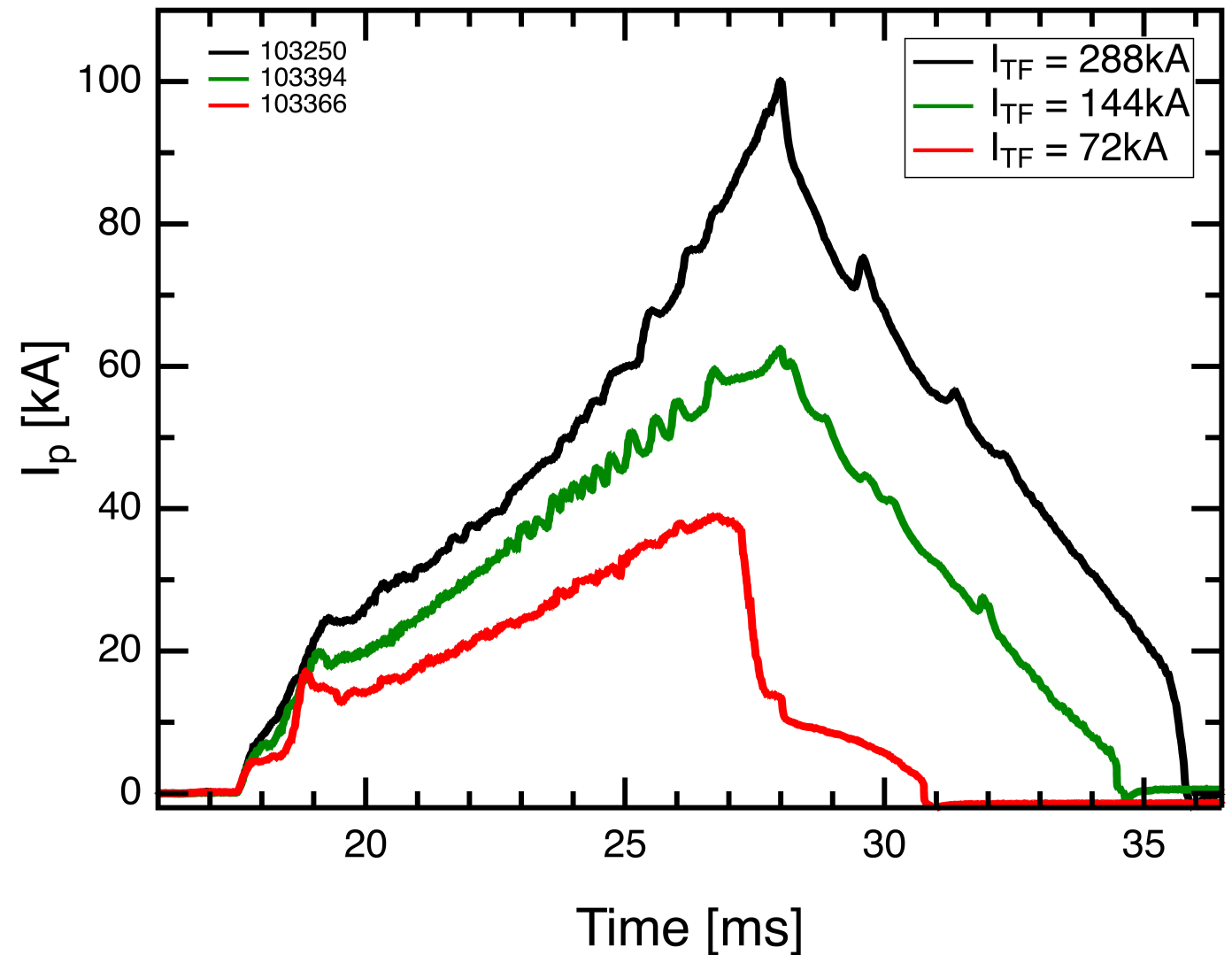
- Comparable Shape Evolution





Early Phase $I_p(t)$ Exhibits I_{TF} Scaling

- Higher performance achieved as I_{TF} increased
- Behavior similar to model expectations
 - Modify early phase I_p via I_{TF}
 - Higher performance at end of discharge



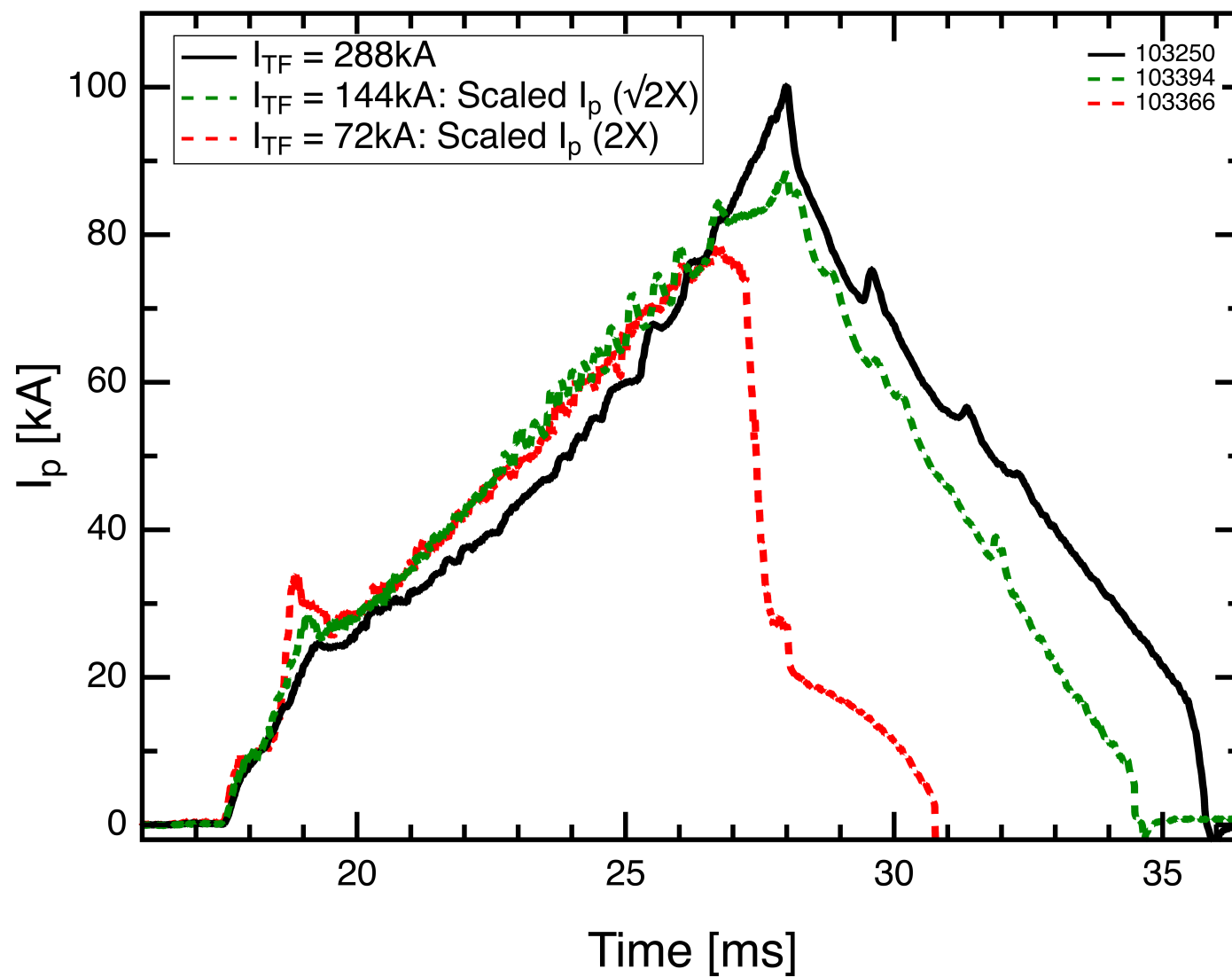


Early Phase I_p Scales with $\sqrt{I_{TF}}$ as Expected from Taylor Limit

- Consistent with comparable plasma shape evolution

$$- I_{TL} \sim \sqrt{A_p}$$

- URANIA scenario utilizes this scaling to achieve higher I_p performance

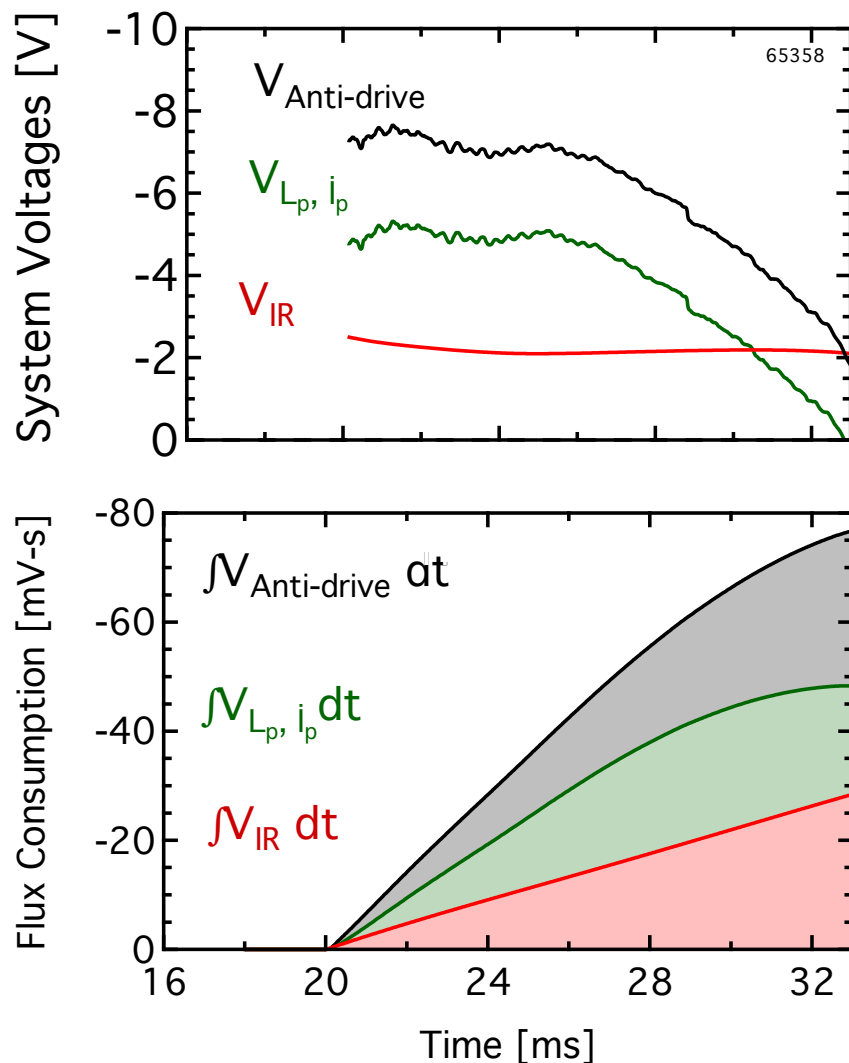




Dissipation in LFS LHI



Inductive Reactance is the Dominant Contribution to Net Plasma Impedance



$$V_{Anti-drive} = V_{IR} + V_{L_p, i_p}$$

- Resistive dissipation**

- V_{IR} : $\sim 1-2$ V
- $\sim 40\%$ of V-s
- Assumed $\langle T_e \rangle = 70$ eV
- Assumed $Z_{eff} M_{neo} = 2.85$

$$V_{IR} = I_p \left(\frac{\langle \eta_p \rangle 2\pi R_0}{A_p} \right)$$

- Inductive reactance**

- V_{L_p, i_p} : $\sim 4-6$ V
- $\sim 60\%$ of V-s

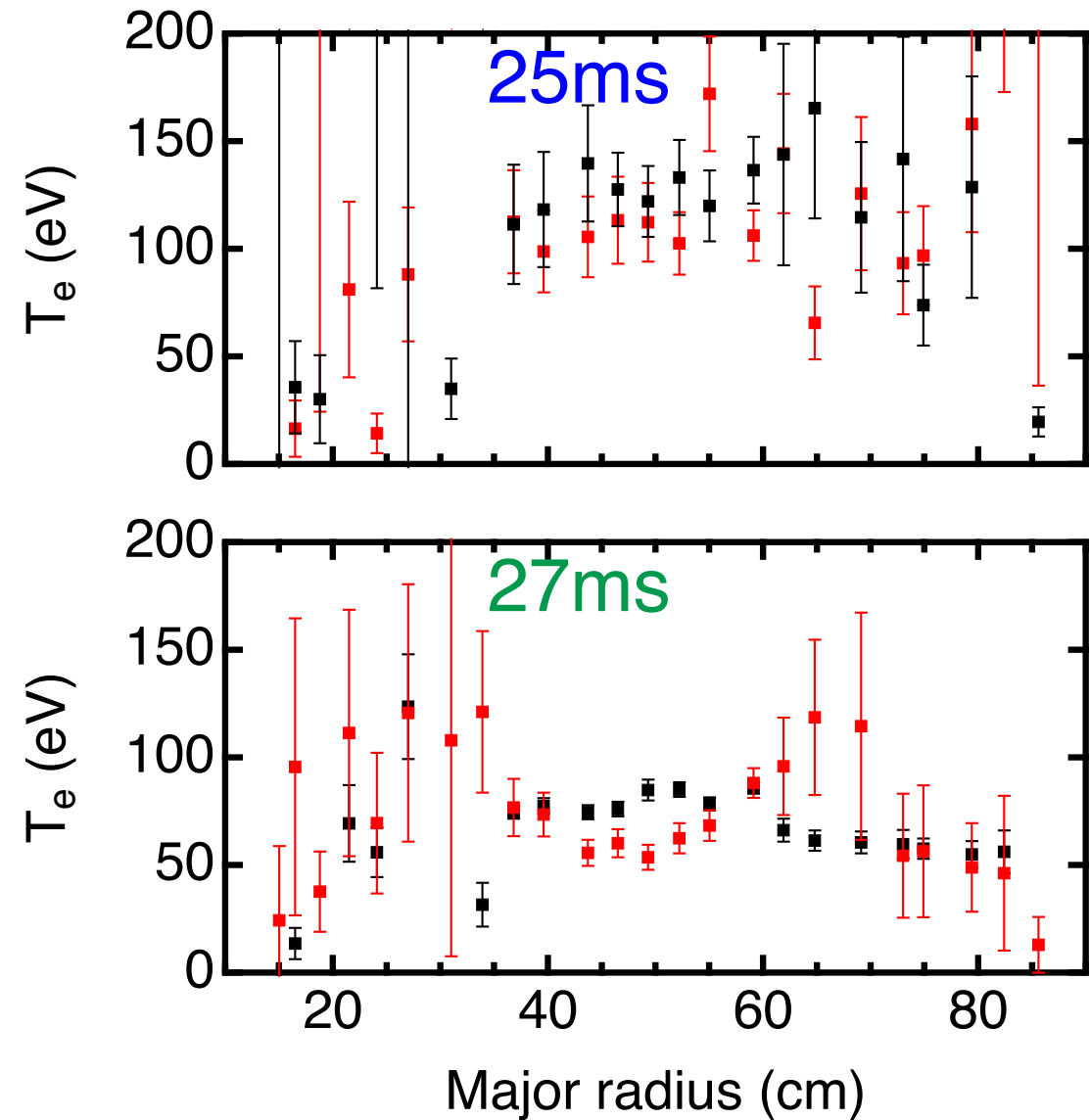
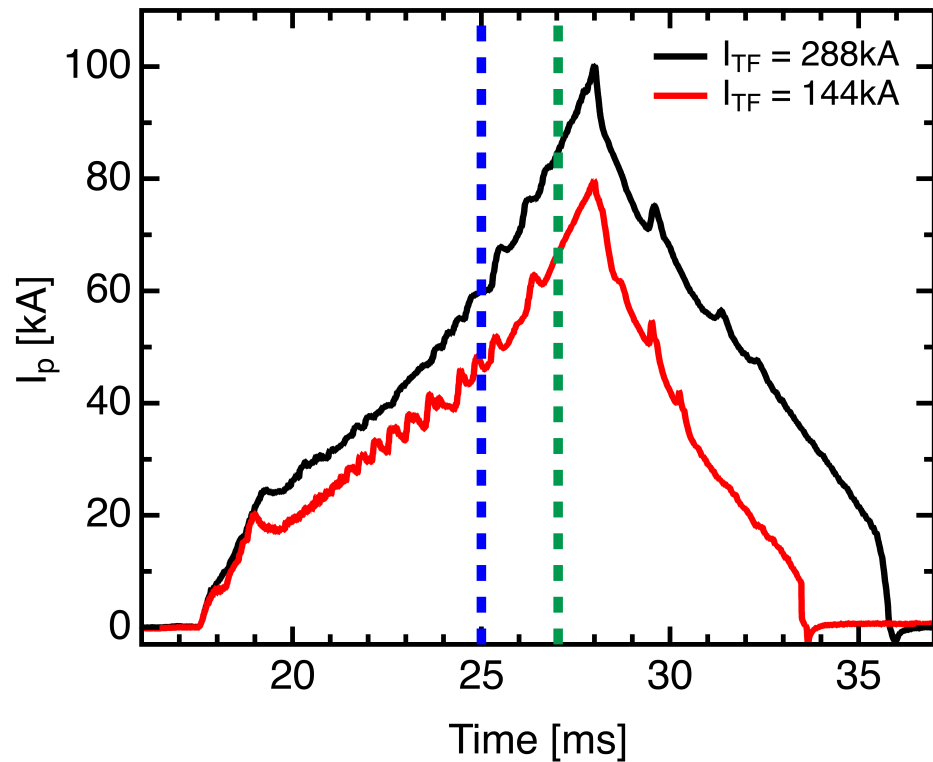
$$V_{L_p, i_p} = -L_e \frac{dI_p}{dt}$$





Similar T_e Profiles at Different I_{TF} Levels

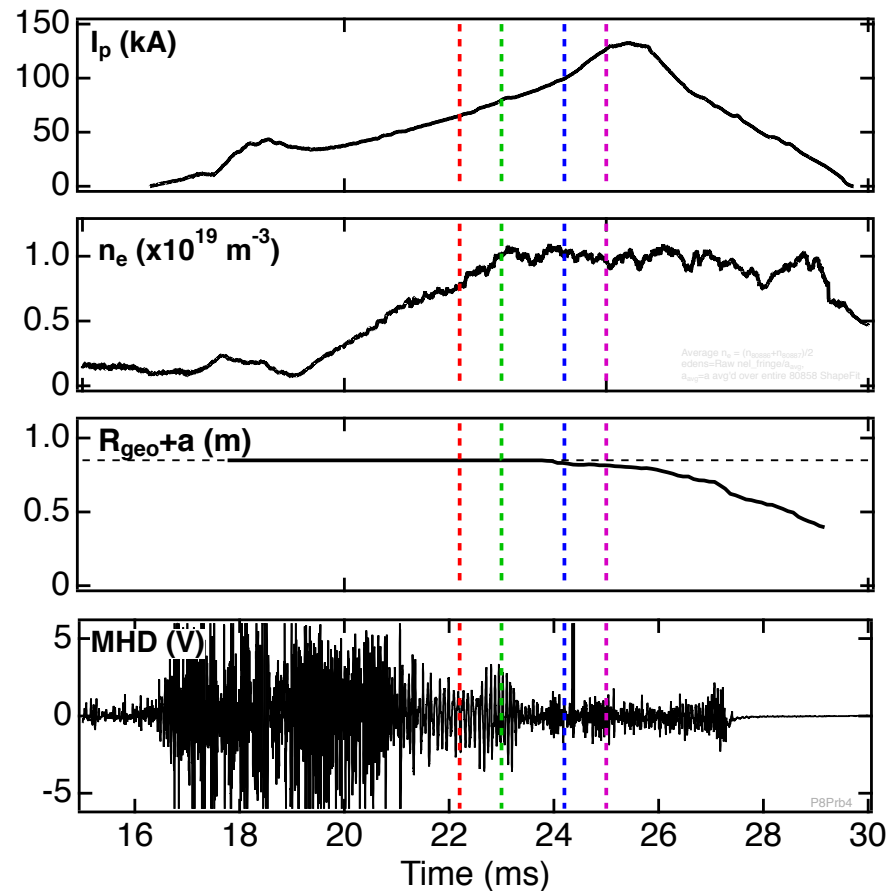
- Similar $\langle T_e \rangle \rightarrow$ similar $\langle \eta_{spitzer} \rangle$
 - Assumed constant Z_{eff}





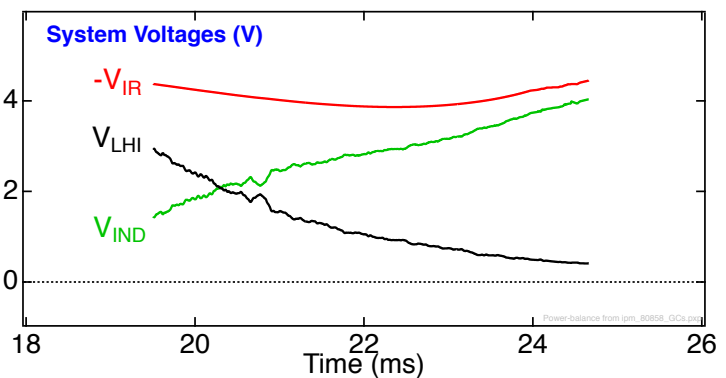
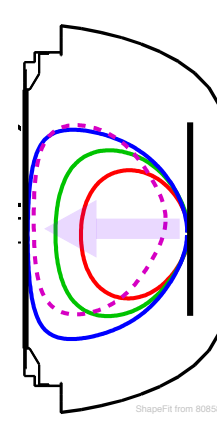
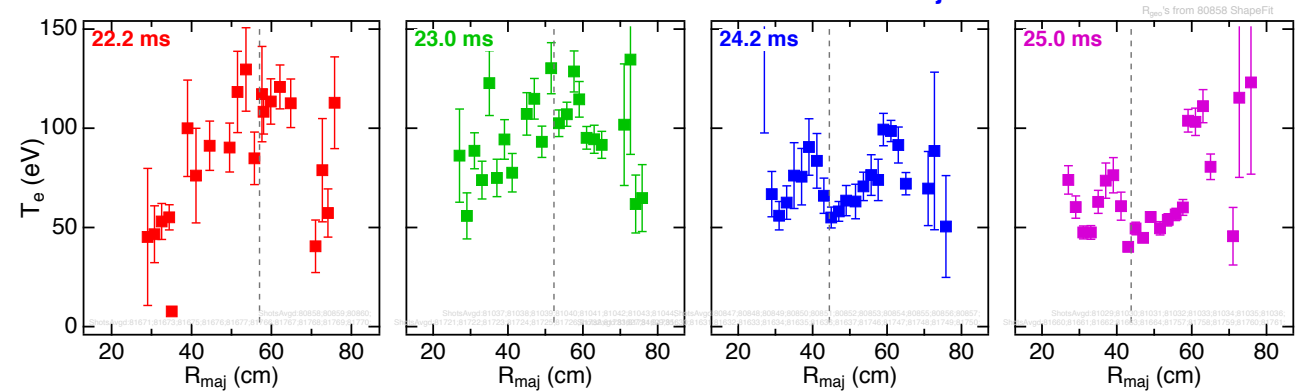
Peaked T_e Profiles when Coupled to Injectors

Majority Inductive Drive in Later Half of Discharge



$I_{TF} \sim 288$ kA

Inductive-Drive Dominant $T_e(R_{maj}, t)$



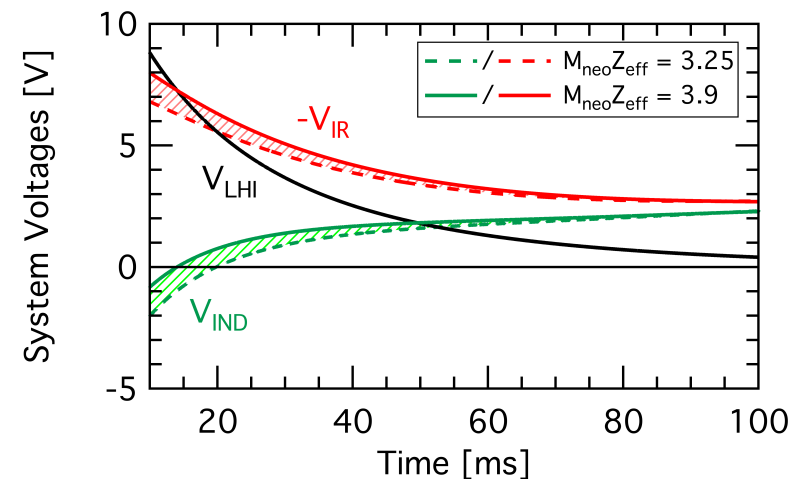
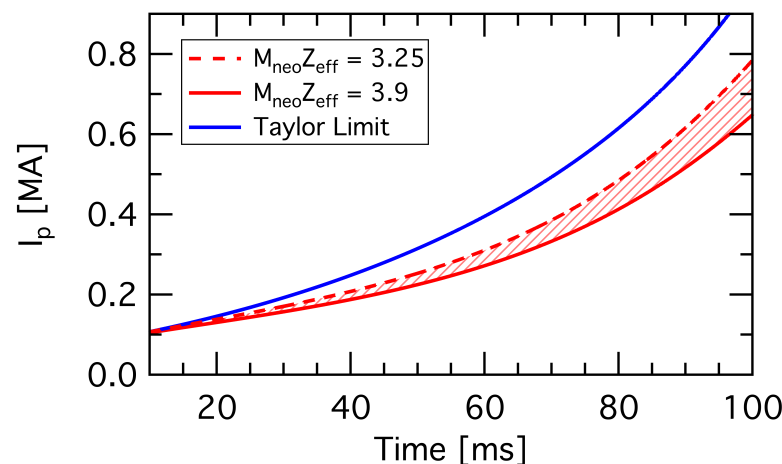
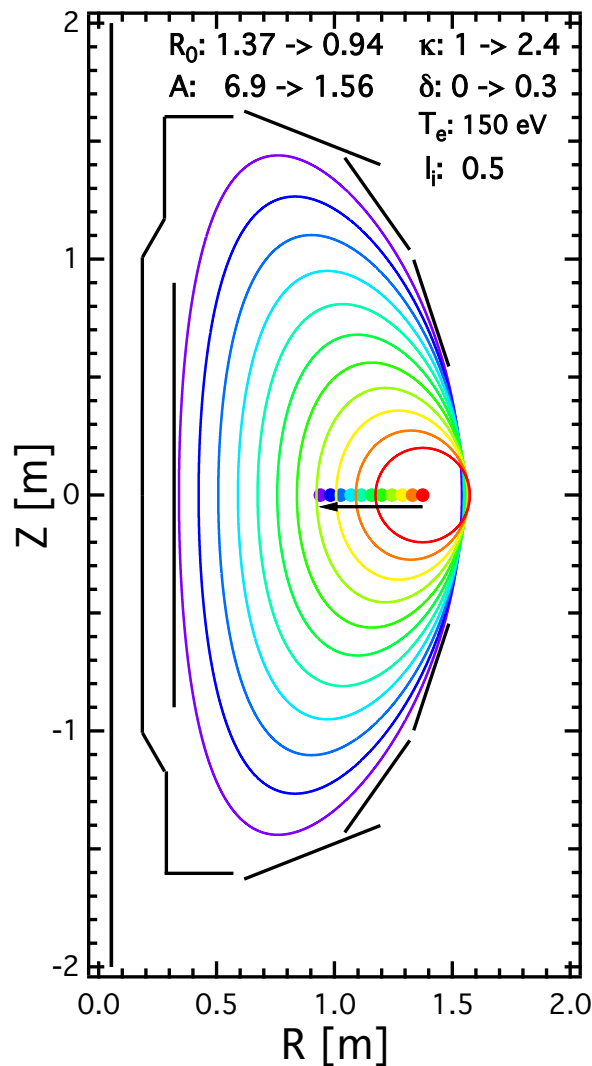
- Model $\langle \eta_p \rangle$ consistent with measured $\langle T_e \rangle$ and typical $M_{neo} \approx 2$ and $Z_{eff} \approx 3$ for PEGASUS
 - Z_{eff} and helicity dissipation are under active investigation



Scaling LHI toward NSTX-U Startup



Model Applied to NSTX-U Geometry for Initial $I_p \sim 0.8$ MA Scenario



- $I_p \sim 0.8$ MA achievable with reasonable LHI system
 - $B_{TF,0}$ @ full size (100ms) = 1 T
 - $\langle T_e \rangle \sim 150$ eV assumed; $M_{neo} = 1.3$; $Z_{eff} = 2.5-3$
 - $A_{inj} V_{inj} = 20 \text{ kVcm}^2$; $I_{inj} = 20 \text{ kA}$
- Important physics and technology questions remain for projection:
 - Confinement and current drive efficiency scaling to large size, high B_{TF}
 - Low V_{inj} at high V_{LHI} for PMI control

*C. Neumeyer et al (2009) 23rd IEEE/NPSS Symposium on Fusion Engineering





URANIA Experiments will Test NSTX-U Startup Scenario

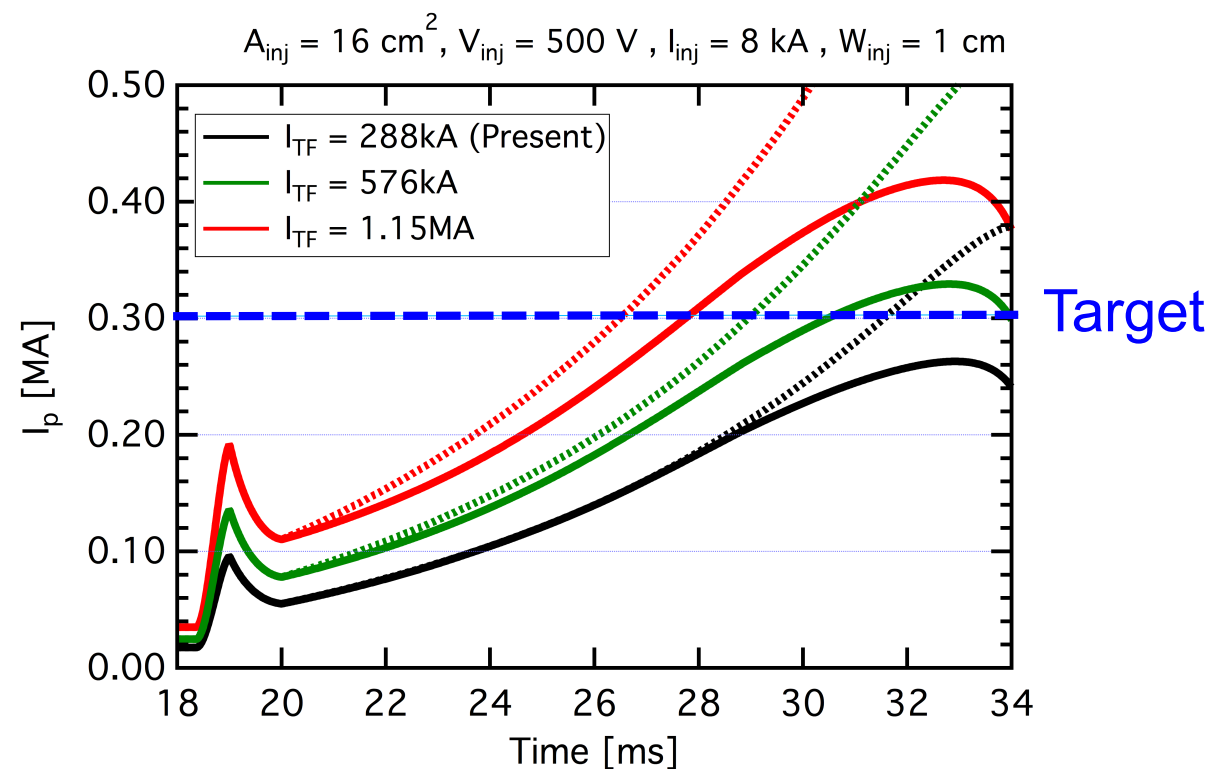
- Physics Tests

- Scaling to $I_p \sim 0.3$ MA
- Increase $B_{TF} \sim 0.6$ T
- Validate high I_p through early Taylor Limit increase
- Demonstrate high V_{LHI} at low V_{inj}

- Technology Tests

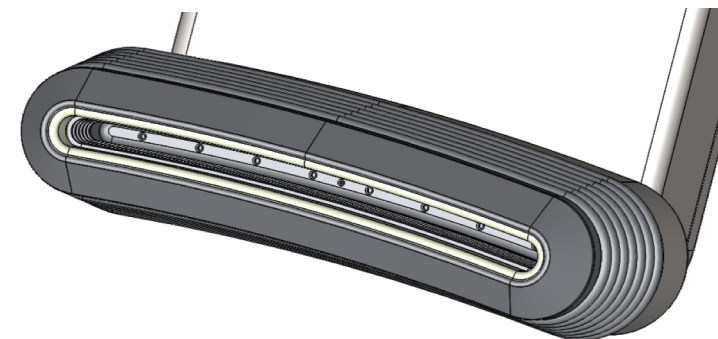
- Low $V_{INJ} \rightarrow$ Avoid PMI
- “Slit” injector design on LFS
- Removable single port injector access
- $V_{inj}(t)$ control
- Active injector gas control
- Long pulse operation

Model projection for next gen. LHI system



*Non-circular, High- A_{inj} Helicity
Injector Rendering*

*High $A_{inj} = 16 \text{ cm}^2$
Low $W_{inj} = 1 \text{ cm}$ aperture*

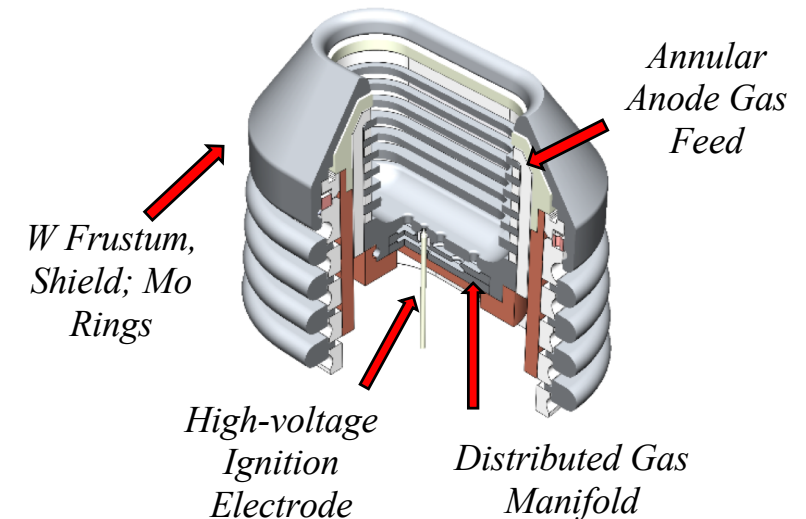




Near Term PEGASUS Experiments to Establish URANIA Operation

- Push injector current density limit
 - $J_{inj} > 1 \text{ kA} * \text{cm}^{-2}$
 - Control neutral particle density $\rightarrow$ maintain V_{inj}
- Test non-circular, high A_{inj} LFS system
- Thomson scattering documentation of typical LFS LHI scenario
 - Investigate electron confinement behavior
- Ohmic operations
 - Taylor limit scaling
 - LHI $\rightarrow$ ohmic handoff

Non-Circular, High- A_{inj} Helicity Injector Renderings



*High $A_{inj} = 6 \text{ cm}^2$,
Low $w_{inj} = 1.6 \text{ cm}$
Aperture*





LFS LHI Provides a Path Toward Scalable, Non-Inductive, High I_p Startup

- Path to high I_p depends on increasing Taylor limit early in discharge
- I_{TF} scans demonstrate higher I_p with increased early Taylor limit
 - Controlled shape evolution, injector parameters, and resistive dissipation
- URANIA Experiments will test NSTX-U Startup Scenario
 - Scaling LHI to higher I_p , B_{TF}
- Planned Experiments on PEGASUS to develop URANIA operation scenarios
 - Testing non-circular injector design, high J_{inj} , confinement studies
- Work Supported by US DOE grants DE-FG02-96ER54375 and DE-SC0006928





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